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Balance of the Waste Tank Farm Radioisotope Inventory Report

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List of Acronyms

A&PC	Analytical & Process Chemistry
CFMT	Concentrator Feed Makeup Tank
CMP	Characterization Management Plan for the Facility Characterization Project (WVDP-403)
CPC	Chemical Process Cell
HEPA	High-Efficiency Particulate Air
HLW	High-Level Waste
MDA	Minimum Detectable Activity
NFS	Nuclear Fuel Services
PNNL	Pacific Northwest National Laboratory
PUREX	Plutonium Uranium Extraction Process
PVS	Permanent Ventilation System
STS	Supernatant Treatment System
THOREX	Thorium Uranium Extraction Process
WVDP	West Valley Demonstration Project
WVNSCO	West Valley Nuclear Services Company

1.0 Introduction

This report provides a conservative curie inventory for the balance of the Waste Tank Farm for use with performance assessment modeling. Evaluation and characterization activities were conducted in accordance with WVDP-403, "Characterization Management Plan for the Facility Characterization Project" (CMP)⁽¹⁾.

The approach used to evaluate the balance of the Waste Tank Farm and generate the inventory estimate involved the following steps:

- Collection and evaluation of existing/historical information and data;
- Determination that additional data was needed to be collected to construct the inventory estimate;
- Collection of additional data;
- Preparation of dose-to-curie computer models; and
- Application of a conservative set of scaling factors to the modeling results yielding a conservative radioisotopic inventory for the units.

2.0 Balance of the Waste Tank Farm Description

The balance of the Waste Tank Farm refers to the equipment, piping, and structures, located within the fenced-in area known as the Waste Tank Farm not previously characterized as part of the Supernatant Treatment System (STS) Valve Aisle and Waste Storage Tanks 8D-1, 8D-2, 8D-3 and 8D-4. The balance of the Waste Tank Farm would therefore include the Sludge Mobilization System, High-Level Waste (HLW) Transfer System, the STS Support Building, the Waste Tank Farm legacy pipelines, the permanent ventilation system, equipment shelter, the Con-Ed Building, and the Tank 8D-2 M-8 Riser Pump Pit. Reference drawings are provided in Appendix A.

The Waste Tank Farm is located approximately 300 feet north of the Nuclear Fuel Services (NFS) Process Building. The Waste Tank Farm facilities were constructed in the 1960's for storage of aqueous wastes generated as a by-product of spent nuclear fuel reprocessing operations. These aqueous waste streams were principally generated from the solvent extraction process performed in the extraction cells where dissolved nuclear fuel, an aqueous waste stream containing uranium, plutonium, and fission products, was contacted with a mixture of tributyl phosphate and n-dodecane to separate the uranium and plutonium from the fission products. The fission products in the aqueous waste stream were transferred to Tanks 8D-2 and 8D-4 in the Waste Tank Farm for storage.

2.1 HLW Transfer System (Transfer Trench and Pits 8Q-1, 8Q-2, 8Q-3, and 8Q-5)

The HLW Transfer System is composed of three pump pits, a diversion pit, and the Waste Transfer Trench (see Figure 1). The HLW Transfer System directly supported HLW processing activities associated with the transfer of HLW waste from the Waste Tank Farm to the Vitrification Facility.

Pump Pits 8Q-1, 8Q-2, and 8Q-4 located at the respective storage tank on top of the tank vaults, and Diversion Pit 8Q-5 accommodates the piping, valves, and upper section of the waste removal pumps along with other equipment required for waste transfer. Piping to equipment connections within the pits is made through remote connectors called jumpers. Equipment access is gained through removable one foot six inch thick pre-cast concrete pit covers. The pits are reinforced concrete structures internally lined with stainless steel. All pits are approximately six feet deep and vary in size from 6 feet by 7 feet to 13.5 feet by 12 feet. Pit walls and floors are nominally one to two feet thick. The tank access riser for each of the respective waste removal pumps penetrates the pump pit floor. The liner slopes to a low point drain connected to the removal pump access riser. Each pit accommodates the equipment required to process the waste out of

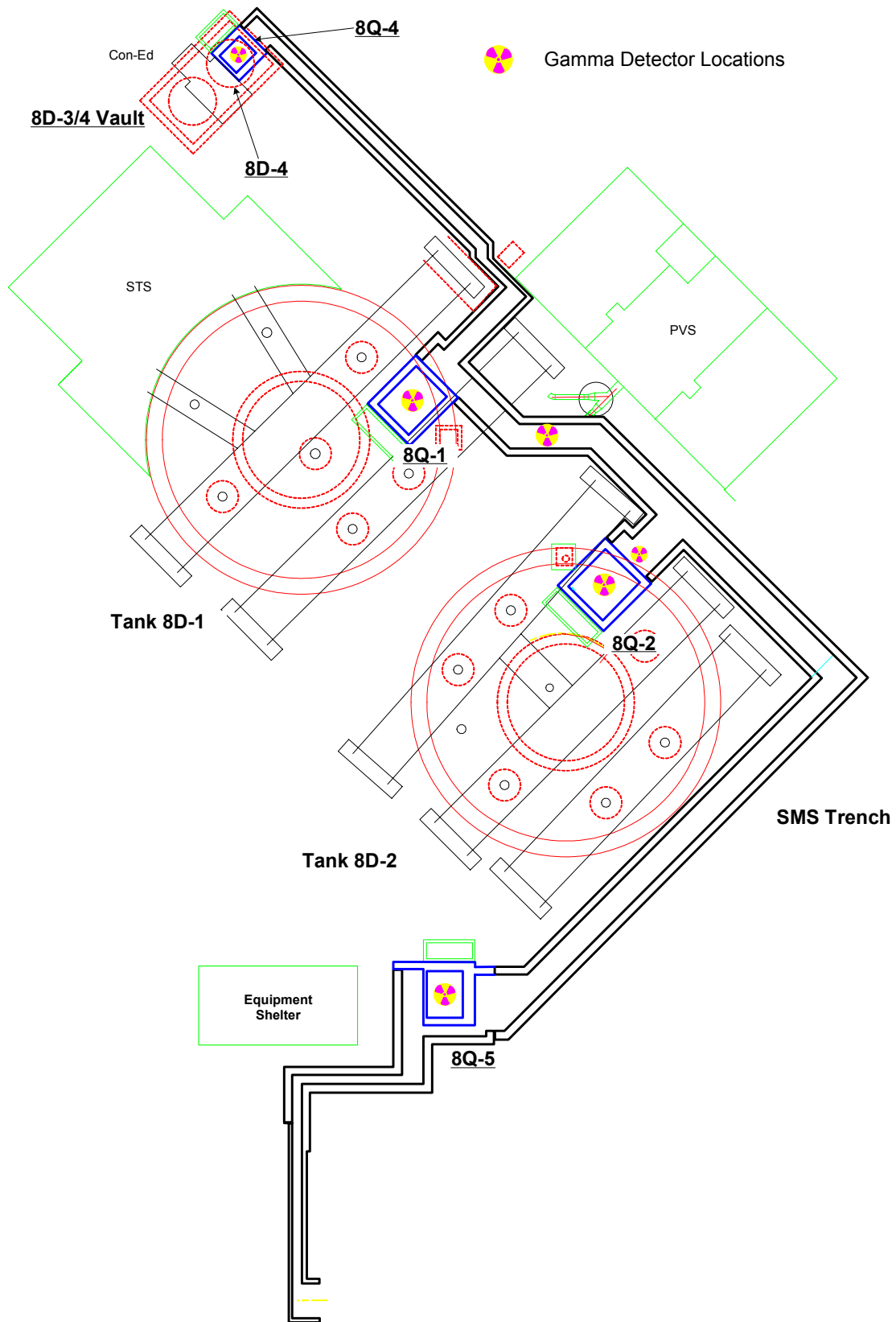


Figure 1

High-Level Waste Transfer System

the respective tank (i.e., removal pump, discharge piping, and flow monitoring equipment for controlling waste transfer operations). Unique to the 8Q-2 Pump Pit is particle size reduction equipment for size reducing the zeolite transferred from Tank 8D-1 to 8D-2. Zeolite is an ion sieve used to remove Cs-137 from Tank Farm liquids.

The HLW Transfer Trench is a long concrete vault containing double-walled piping that was designed to convey waste between the Waste Tank Farm and the Vitrification Facility. The HLW Transfer Trench is approximately 500 feet long, extending from the Tank 8D-3/Tank 8D-4 Vault along the north side of Tanks 8D-1 and 8D-2, before turning to the southwest and entering the north side of the Vitrification Facility. The trench is 6 to 20 feet wide and its height ranges from six to nine feet. The HLW Transfer Trench was constructed of reinforced concrete walls and pre-cast concrete covers. The walls of the trench are 18 to 24 inches thick and the pre-cast covers are two feet thick. The floor slab of the trench is one foot thick concrete. Wastes are conveyed through approximately 3,000 feet of two- and three-inch double-walled, butt welded, Schedule 40 stainless steel transfer piping contained within the transfer trench. No leaks of radioactive liquids from the transfer piping contaminating the transfer trench are known to have occurred based on routine sampling of the Transfer Trench Sump.

The HLW Transfer System was constructed by the West Valley Demonstration Project (WVDP) in the early 1990's to support the waste handling needs for the HLW Vitrification Project. There were three distinct phases of operation that the HLW Transfer System supported: zeolite transfers from Tank 8D-1 to Tank 8D-2, thorium uranium extraction process (THOREX) transfer and neutralization from Tank 8D-4 to Tank 8D-2, and HLW sludge transfer from Tank 8D-2 to the Vitrification Facility. During vitrification operations, the HLW System transfer piping and pit jumpers were routinely flushed with at least one line volume of water after each transfer. At the conclusion of vitrification operations more aggressive flushing was completed with one molar nitric acid followed by a utility water flush.

There was no historical radiological survey data located for the HLW Transfer System with the exception of the 8Q-2 Pit. Dose rate surveys of the 8Q-2 Pit taken on February 21, 1998 ranged from 80 mR/hr to 5 R/hr⁽²⁾. The radionuclide distribution for the HLW Transfer System can be conservatively bounded by the Batch 10 HLW radionuclide distribution which was derived from a sample of the first HLW transfer to the Vitrification Facility from Tank 8D-2. Data from later HLW transfers indicate that the ratio of alpha-transuranics to Cs-137 steadily decreased over time.

2.2 Permanent Ventilation System Building

The Permanent Ventilation System (PVS) Building is located at the north perimeter of Tank 8D-2 and measures 75 feet long, 40 feet wide, and 16 feet tall (see Figure 1). The PVS Building contains four rooms which include the PVS Room, the Electrical Room, the Mechanical Room, and the Control Room. The steel structure is attached to the concrete floor of the building. The concrete floor is one foot thick and the entire structure is supported by concrete footings. The PVS Building has a sheet metal roof which supports the PVS Discharge Stack. The PVS is designed to provide ventilation to the STS Support Building, STS Valve Aisle, STS Pipeway, and the HLW Tanks during radioactive operations. Air flow from these facilities is directed to the PVS where it passes through a mist eliminator, heater, roughing filter, and two sets of High-Efficiency Particulate Air (HEPA) filters before being discharged through the PVS Stack to the atmosphere. Residual radioactivity is expected to be associated with the ventilation equipment.

A small, recently built, skid-mounted PVS Stack Monitoring Building is located near the east end of the PVS Building. Insulated samples lines lead from and back to the PVS Stack.

A routine radiation and contamination survey is performed weekly in the PVS Building during which dose rate measurements and contamination level information is collected. Dose rate measurements of the PVS Building taken in December 2003⁽³⁾ ranged from 1 mR/hr to 60 mR/hr. The highest dose rates, as seen in the weekly surveys, are associated with the HEPA filter bank in the PVS Room. Based on the dose rate measurements collected, significant contamination would not be expected to remain in the PVS Room or in the ventilation system subsurface piping. Therefore, the PVS Building is not a key curie contributor in the balance of the Waste Tank Farm.

2.3 Equipment Shelter

The Equipment Shelter is a one-story concrete block building located immediately north of the Vitrification Facility (see Figure 1). The Equipment Shelter measures approximately 40 feet long, 18 feet wide, and 12 feet high and has a concrete floor six inches thick. A small extension on the west side of the Equipment Shelter is approximately nine feet long, seven feet wide, and five feet high, with a one foot thick concrete floor. The roof decking covering this structure is four inches thick. This structure houses the Waste Tank Farm Ventilation System that formerly ventilated the HLW tanks and the STS process vessels in Tank 8D-1. The ventilation system draws air through a condenser, a knockout drum, a heater, and two sets of HEPA filters and blowers before being discharged through the main stack of the Process Building.

A routine radiation and contamination survey is performed weekly in the Equipment Shelter during which dose rate measurements and contamination level information is collected. Dose rate measurements⁽⁴⁾ from four locations in the Equipment Shelter taken in December 2003 ranged from 0.1 mR/hr to 2.8 mR/hr. Most of the radiological inventory in the Equipment Shelter is expected to be removed with the ventilation system equipment during facility decommissioning. Based on the dose rate measurements collected, significant contamination would not be expected to remain in the Equipment Shelter or in the ventilation system subsurface piping and associated condensate piping. Therefore, the Equipment Shelter is not a key curie contributor in the balance of the Waste Tank Farm and is not considered further in this report.

2.4 Con-Ed Building

The Con-Ed Building is a concrete block building constructed on top of the underground concrete vault containing Tanks 8D-3 and 8D-4. This building, which is 10 feet wide, 13 feet long, and 11 feet high, houses the instrumentation and valves used to monitor and control the operation of Tanks 8D-3 and 8D-4. As stated in WVDP-EIS-017⁽⁵⁾, the Con-Ed Building is reported to be radiologically contaminated. The majority of the radiological inventory is believed to be contained within the piping and equipment inside the building.

A routine radiation and contamination survey is performed weekly in the Con-Ed building during which dose rate measurements and contamination level information is collected. Dose rate measurements⁽⁴⁾ of the Con-Ed Building taken in December 2003 were 0.1 mR/hr. Based on the dose rate measurements collected, significant contamination would not be expected to remain in the Con-Ed Building. Therefore, the Con-Ed Building is not a key curie contributor in the balance of the Waste Tank Farm and is not considered further in this report.

2.5 STS Support Building

The STS Support Building is located adjacent to and on top of the Tank 8D-1 vault. The STS Support Building is a two-story structure that contains equipment and auxiliary support systems needed to operate the STS which was designed for the pretreatment of the HLW plutonium uranium extraction process (PUREX) supernatant and sludge wash solutions. The upper level of the STS Support Building, extending from a site reference elevation of 107 feet to the roof peak at

129 feet, is a steel framework structure covered with steel siding. The upper level is a radiologically clean structure that contains a control room, heating, ventilation and air conditioning equipment, utilities, and storage tanks for fresh water and fresh zeolite to support STS operations. The lower level of the STS Building, extending from 92 to 107 feet, was constructed with reinforced concrete walls, floor, and ceiling and contains an airlock, the shielded valve aisle, and an operating aisle. See Appendix A for drawings.

The STS Support Building was built on 68 55-foot long cast-in-place piles. Each pile was installed to a minimum depth of 15 feet into the Lavery Till unit. These piles were installed to provide additional structural support to the STS Support Building because the backfill soil around HLW Tanks 8D-1 and 8D-2 was not compacted after the tanks were built⁽⁶⁾.

The shielded valve aisle is located on the first floor of the support building, adjacent to Tank 8D-1. This valve aisle contains remotely operated valves and instrumentation used to control operation of the STS. The shield walls of the valve aisle were constructed of 12-inch thick carbon steel and the ceiling was made from 14-inch thick carbon steel. The shield walls and ceiling are composed of three individual steel plates that are bolted together. The valve aisle is radiologically contaminated from valve and piping leaks⁽⁶⁾. Removable hatches are above the valve aisle that provide access to the aisle for removal of large items.

The STS Pipeway/Shield Structure is located on top of the Tank 8D-1 vault adjacent to the first floor of the support building. This concrete and steel structure contains numerous piping runs and structural members that support the STS equipment in Tank 8D-1. Additionally, STS decontaminated supernatant piping and Low-Level Waste Treatment System concentrate return piping runs between the Process Building and the STS Pipeway. Significant contamination is not expected to remain in this piping.

Flushing of the STS equipment and piping was conducted in late 2000 and again in early 2002. Six flushing paths were identified to effectively flush residual solids from the STS process equipment and piping back into Tank 8D-2. Radiation probes were deployed in key locations for each flush to monitor flush effectiveness. Flushing was performed using dilute nitric acid and demineralized water⁽⁷⁾.

The majority of the STS Support Building is not radiologically contaminated. Only the STS Valve Aisle and the piping within the Pipeway/Shield Structure is radiologically contaminated. The STS Valve Aisle radioisotope inventory has been determined and is reported in RIR-403-007⁽⁸⁾. There was no historical radiological survey data located for the STS Pipeway/Shield Structure. However, jumpers in the valve aisle have been surveyed which would be radiologically similar to the Pipeway/Shield Structure piping. Dose rate measurements of a valve aisle jumper taken in May 1998 was 1,700 mR/hr⁽⁹⁾. The radionuclide distribution for the STS Support Building would be the same as that derived for the STS Valve Aisle.

2.6 Waste Tank Farm HLW Legacy Piping

The Waste Tank Farm HLW legacy piping refers to the originally installed underground piping employed by NFS to manage the HLW wastes produced during spent nuclear fuel reprocessing operations. During NFS reprocessing operations, the HLW process piping was used to transfer the aqueous waste streams generated from the solvent extraction process and collected in the Chemical Process Cell (CPC) to the Waste Tank Farm. Since the end of reprocessing operations primarily laboratory wastes and to a lesser extent liquid accumulations from cell sumps have been transferred. These lines, which originate at the floor connections in the CPC, are approximately 500 to 700 feet long and are constructed of three-inch Schedule 40 stainless steel which gravity drain to storage tanks in the Waste Tank Farm. All reprocessing wastes, with the exception of the

THOREX waste, was transferred to the Waste Tank Farm via Line 7P-113 during NFS reprocessing operations. Subsequent to reprocessing, this pipeline has been flushed by the process plant decontamination solutions⁽¹⁰⁾ and other miscellaneous wastes that were collected in Tank 7D-2 such as cell sumps and laboratory wastes.

For the transfer of THOREX waste to Tank 8D-4, Line 7P-120 was used. The other HLW pipeline, 7P-112, which serviced Tank 8D-1, was never used as Tank 8D-1 was the spare HLW receiver tank.

There was no historical radiological survey data located for the Waste Tank Farm HLW legacy piping. Radionuclide concentrations for THOREX waste are available for characterization of transfer Pipeline 7P-120 and the radionuclide concentrations for Line 7P-113 will be the same as current Tank 7D-2 wastes.

2.7 Tank 8D-2 M-8 Riser Pump Pit and Associated Transfer Piping

The Tank 8D-2 M-8 Riser Pump Pit was constructed on top of the Tank 8D-2 vault over the M-8 riser where STS Transfer Pump 50-G-001 is located. This long shafted floating suction vertical turbine pump provided for the transfer of PUREX supernatant and sludge wash solutions from Tank 8D-2 to the STS for HLW pretreatment. Over the past several years, this system provided for the treatment of sodium bearing waste water. The 2½-inch diameter Schedule 40 304L stainless steel supply and return transfer piping is doubly contained in a 200 foot long, 20 inch diameter culvert pipe advancing along the south side of Tanks 8D-1 and 8D-2 to the STS. The return piping drains into a trough around the perimeter of the M-8 Riser to direct the flow back into Tank 8D-2. The M-8 Pump Pit is approximately 75 inches wide by 60 inches long by 90 inches deep and fabricated from ¼-inch stainless steel. Pit shield covers are fabricated of 4-inch thick carbon steel plates and stacked three high for a total thickness of 12 inches.

During STS flushing operations in November and December 2000, dose rate measurements were collected which ranged from 722 mR/hr to 1,244 mR/hr^(11, 12, 13). The radionuclide distribution for the M-8 Riser Pump Pit and associated transfer piping would be the same as that derived for the STS Valve Aisle.

2.8 Conclusion

In summary, based on the Waste Tank Farm operating history, decontamination records, historic radiological survey information, and available analytical data, the following areas of the balance of the Waste Tank Farm were identified as key curie contributing areas:

- HLW Transfer Trench Piping
- Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5
- STS Pipeway Piping
- Waste Tank Farm HLW Legacy Piping
- M-8 Riser Pump-Pit and Associated Piping

The other areas of the Waste Tank Farm, as explained above, are not considered to be key curie contributors to the balance of the Waste Tank Farm.

3.0 Historical Record Review

Referenced herein are existing reports and/or records that were found to contain general background information on the balance of the Waste Tank Farm. As discussed in Section 2.0, existing dose rate measurements and radionuclide distributions were used to identify the key curie contributing areas in the balance of the Waste Tank Farm. As discussed in Section 4 below, additional data is needed to be collected from the key areas to generate a curie estimate for the balance of the Waste Tank Farm.

3.1 Dose Rate Measurements/Surveys

During activities to remove expended equipment from the STS Valve Aisle in May 1998, STS Sample Jumper J-20 was surveyed. Dose rate measurements were recorded at contact of 1,700 mR/hr and at one foot of 1,300 mR/hr on the Radiation and Contamination Survey Report 060042⁽⁹⁾. The STS liquids contacting this jumper would be representative of the liquids also contacting the STS Pipeway/Shield structure piping and the STS Transfer Piping to the Tank 8D-2 M-8 Riser.

Dose rate surveys in the Tank 8D-2 M-8 Riser pump pit were performed in November and December 2000 and ranged from 722 mR/hr to 1,244 mR/hr. These surveys were performed per Work Orders 0001946, 0001985, and 0002260 and would be representative of the activity in the M-8 Riser pump pit following flushing operations^(11, 12, 13).

3.2 Isotopic Distribution Information/Analytical Data

As described in Section 2.0, the HLW Transfer System directly supported HLW processing activities associated with the transfer of HLW from the Waste Tank Farm to the Vitrification Facility. Batch 10 vitrification run data was identified to be representative of the processing activities associated with the HLW Transfer System. Batch 10 vitrification run analytical results are available and are shown Table 1. The utilization of Batch 10 data^(14, 15) to develop HLW scaling factors is considered to be conservative. First, the Batch 10 sample was collected from the first HLW transfer from Tank 8D-2 to the Vitrification Facility in 1996 and represents the waste at its most "concentrated" form with the highest ratios of key alpha-transuranic radionuclides to Cs-137. Since the time of this sample collection, processing of the supernatant in the HLW tanks continued through the cesium removal columns suspended from the roof of Tank 8D-1, selectively removing Cs-137 onto zeolite. The cesium removal columns were routinely emptied and the zeolite transferred back to Tank 8D-2 to be processed through the Vitrification Facility. This increase in the relative amount of Cs-137 in the waste resulted in the ratios of key alpha-transuranic radionuclides to Cs-137 to decrease over time. This makes application of the Batch 10 data conservative relative to defining a HLW distribution. The validation of the Batch 10 data is discussed in Section 6.0.

Relative to existing data that supports development of a radionuclide inventory for the HLW legacy lines, several areas were investigated. As discussed in Section 2, the THOREX waste radionuclide concentrations are available and the data is shown in Table 2 for characterization of Pipeline 7P-120. This data was obtained from samples of THOREX waste collected from Tank 8D-4 circa 1983 for the Waste Characterization Program to support the design the HLW pretreatment and vitrification processes⁽¹⁶⁾. Any residual wastes remaining in Line 7P-120 would be represented by the THOREX waste radionuclide concentrations as this line was only used for the transfer of THOREX waste to Tank 8D-4. As for Line 7P-113, any residual wastes remaining in Line 7P-113 would be best represented by the radionuclide concentrations of the liquids that have been collected in Tank 7D-2 and transferred to Tank 8D-2. Prior to transferring Tank 7D-2 to Tank 8D-2, a volume of Tank 7D-2 is transferred to Tank 3D-2 for sampling. The Tank 3D-2 radionuclide distribution from a sample collected in January 2002 is shown in Table 3.

For the STS Pipeway/Shield Structure and the Tank 8D-2 M-8 Riser Pump Pit, a conservatively bounding radionuclide distribution is available. As explained in Reference 8, the STS Valve Aisle can be bounded by the radionuclide distribution shown in Table 4. Tank 8D-1 fluid samples, STS flushing samples, valve aisle smear samples, and the Batch 10 radionuclide distributions were compared in RIR-403-007 to determine the conservatively bounding radionuclide distribution with a reference date of May 2, 2002. These scaling factors, as reported in RIR-403-007, would be appropriate for characterization here since all wastes processed through the STS Valve Aisle would also have been processed through the STS Pipeway/Shield Structure and the Tank 8D-2 M-8 Riser Pump Pit.

Table 1
Batch 10 Radionuclide Distribution

Project Isotope	Batch 10 Radionuclide Distribution (FCi/gram)
C-14	4.90e-04
Tc-99	8.45e-02
I-129	3.90e-07
U-233	3.60e-03
U-234	1.30e-03
U-235	3.80e-05
Np-237	2.00e-02
U-238	3.40e-04
Pu-238	3.96e+00
Pu-239	1.09e+00
Pu-240	7.70e-01
Pu-241	3.43e+01
Am-241	3.21e+01
Cm-243	2.58e-01
Cm-244	6.72e+00
Cs-137	2.85e+03
Sr-90	2.75e+03

- The radiological analysis of certain alpha-emitting nuclides does not permit ready discrimination between two nuclides of approximately equal energies. Nuclide pairs of particular interest for facility characterization include U-233/U-234, U-235/U-236, Pu-239/Pu-240, and Cm-243/Cm-244. The proportion of each nuclide's contribution to the combined activity was developed using historical analyses and ORIGEN calculations⁽¹⁷⁾.

Table 2
THOREX Data

Project Isotope	THOREX 1987	
	Curies*	Curies/Gallon
C-14	1.30e-01	1.09e-05
Tc-99	1.04e+02	8.75e-03
I-129	1.80e-01	1.51e-05
U-232	2.74e+00	2.30e-04
U-233	2.09e+00	1.76e-04
U-234	2.17e+00	1.83e-04
U-235	5.17e-03	4.35e-07
Np-237	3.02e-01	2.54e-05
U-238	7.11e-05	5.98e-09
Pu-238	4.80e+02	4.04e-02
Pu-239	1.54e+01	1.30e-03
Pu-240	8.09e+00	6.80e-04
Pu-241	8.50e+02	7.15e-02
Am-241	2.41e+02	2.03e-02
Cm-243	2.34e-01	1.97e-05
Cm-244	1.37e+01	1.15e-03
Cs-137	4.57e+05	3.84e+01
Sr-90	4.54e+05	3.82e+01

* For 11,889 gallons of THOREX waste as reported in Reference 16.

Table 3
Tank 3D-2 Sample Data

Project Isotope	Tank 3D-2 Sample 02-1765 (F Ci/ml)
C-14	9.97e-05
Tc-99	1.16e-04
I-129	8.21e-05
U-232	2.06e-05
U-233	8.60e-06
U-234	4.10e-06
U-235	3.30e-08
Np-237	5.17e-06
U-238	4.21e-07
Pu-238	1.37e-03
Pu-239	9.07e-04
Pu-240	6.93e-04
Pu-241	1.34e-02
Am-241	5.77e-03
Cm-243	2.49e-05
Cm-244	6.51e-04
Cs-137	2.32e+00
Sr-90	1.88e-01

- The radiological analysis of certain alpha-emitting nuclides does not permit ready discrimination between two nuclides of approximately equal energies. Nuclide pairs of particular interest for facility characterization include U-233/U-234, U-235/U-236, Pu-239/Pu-240, and Cm-243/Cm-244. The proportion of each nuclide's contribution to the combined activity was developed using historical analyses and ORIGEN calculations⁽¹⁷⁾

Table 4
STS Valve Aisle Scaling Factors

Project Isotope	STS Valve Aisle Scaling Factors May 2, 2002*
C-14	1.24E-06
Tc-99	2.13E-04
I-129	9.86E-10
U-232	8.83E-06
U-233	3.39E-06
U-234	1.62E-06
U-235	7.19E-07
Np-237	7.87E-06
U-238	5.57E-07
Pu-238	1.50E-03
Pu-239	4.60E-04
Pu-240	8.18E-04
Pu-241	1.06E-02
Am-241	1.27E-02
Cm-243	8.99E-05
Cm-244	2.19E-03
Cs-137	1.00E+00
Sr-90	9.61E-01

* From Reference 8.

4.0 Technical Approach/Data Gathering

From the review of the operational processes conducted in the Waste Tank Farm, available historic information, and previously generated data, the following areas of the balance of the Waste Tank Farm were identified as potential key curie contributors:

- HLW Transfer Trench Piping
- Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5
- STS Pipeway/Shield Structure Piping
- Waste Tank Farm HLW Legacy Piping
- M-8 Riser Pump Pit and Associated Piping

4.1 HLW Transfer System

4.1.1 HLW Transfer Trench Piping

The HLW Transfer Trench piping is contained within the 500 foot long concrete waste transfer trench. The approximately 3,000 feet of two- and three-inch Schedule 40 stainless steel piping was used to convey wastes between tanks within the Waste Tank Farm and to the Vitrification Facility for solidification. The interior of the waste transfer trench was last surveyed in January 2002. However, this data could not be validated due to a discrepancy in the probe and rate meter which was that the probe was not calibrated to the rate meter used. Therefore, new dose rate measurements were needed for the transfer trench. Using the new dose rates and the Batch 10 vitrification run isotopic data, the trench transfer piping could then be modeled, scaling factors developed, and a curie estimate calculated for the residual activity in the transfer piping (see Section 7.1).

4.1.2 Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5

The Pits 8Q-1, 8Q-2, 8Q-4 and 8Q-5 are approximately six feet deep and vary in size from 6 feet by 7 feet to 13.5 feet by 12 feet. Each pit accommodates the removal pump, jumpers, and flow monitoring equipment required to process the waste out of the respective waste tank. The interior of pits 8Q-1, 8Q-2, 8Q-4 and 8Q-5 were last surveyed in January 2002. However, this data could not be validated due to a discrepancy in the probe and rate meter. Therefore, new dose rate measurements were needed for these pits. Using the new dose rates and the Batch 10 vitrification run isotopic data, the pits could then be modeled, scaling factors developed, and a curie estimate calculated (see Section 7.2).

4.2 STS Pipeway/Shield Structure Piping

The STS Pipeway/Shield Structure Piping is located on top of the Tank 8D-1 vault adjacent to the first floor of the support building. This concrete and steel structure contains numerous piping runs and structural members that support the STS equipment in Tank 8D-1. These facilities were designed for the pretreatment of the HLW PUREX supernatant and sludge wash solutions. There was no historical radiological survey data located for the STS Pipeway/Shield Structure. However, jumpers in the valve aisle have been surveyed which would be radiologically similar to the pipeway/shield structure piping. A dose rate measurement of a valve aisle jumper taken in May 1998 was 1,700 mR/hr. Using the 1998 dose rate measurement and the existing STS Valve Aisle scaling factors, the pipeway/shield structure piping could then be modeled and a curie estimate calculated (see Section 7.3).

4.3 Waste Tank Farm HLW Legacy Piping

The HLW legacy piping originates at floor nozzles in the CPC. The lines are between 500 and 700 feet long, are constructed of three-inch Schedule 40 stainless steel pipe, and gravity drain to HLW storage tanks in the Waste Tank Farm. These lines were used for the transfer of all reprocessing wastes to the Waste Tank Farm. PUREX HLW was transferred to Tank 8D-2 via Line 7P-113 and for the transfer of THOREX waste to Tank 8D-4, Line 7P-120 was used. Subsequent to reprocessing, Line 7P-113 has been flushed by the process plant decontamination solutions⁽¹⁰⁾ and other miscellaneous wastes such as cell sump liquid and laboratory wastes that were routinely collected in Tank 7D-2 and sampled in Tank 3D-2 before being transferred to Tank 8D-2. The other HLW Pipeline 7P-112 which serviced Tank 8D-1 was never used as Tank 8D-1 was the spare HLW receiver tank. Using existing analytical data to compute the radioisotopic concentrations of the Tank 7D-2 waste stream and the THOREX waste stream, a curie estimate can be calculated volumetrically for residual wastes remaining in the piping (see Section 7.4).

4.4 M-8 Riser Pump Pit and Associated Piping

The M-8 Pump Pit is 75 inches wide by 60 inches long by 90 inches deep and is fabricated from 1/4-inch stainless steel. The associated supply and return transfer piping plus two spare lines are 2 1/4-inch diameter Schedule 40 304L stainless steel doubly contained in a 200 foot long 20 inch diameter culvert pipe. This system was used to transport the PUREX supernatant, sludge wash and sodium bearing waste water to the STS for treatment.

The interior of the M-8 Riser Pump Pit was last surveyed in November and December 2000 during STS flushing operations. Surveys were taken through existing valve access ports in the pit cover located 65 inches from the top of the pit covers into the pit. Dose rates ranged from 722 mR/hr to 1,244 mR/hr. Using the 2000 dose rate measurements and the existing STS Valve Aisle scaling factors, the pipeway/shield structure piping could then be modeled and a curie estimate calculated (see Section 7.5.1).

There was no historical radiological survey data located for the associated piping of the M-8 Riser. However, jumpers in the valve aisle have been surveyed which would be radiologically similar to this piping. A dose rate measurement of a valve aisle jumper taken in May 1998 was 1,700 mR/hr. Using the 1998 dose rate measurement and the existing STS Valve Aisle scaling factors, the associated piping of the M-8 Riser could then be modeled and a curie estimate calculated (see Section 7.5.2).

4.5 Conclusion

Process knowledge was available that identified the STS Pipeway/Shield Structure, HLW Legacy Piping, and the M-8 Riser pump pit and associated transfer piping as the key curie contributing areas in the balance of the Waste Tank Farm. New dose rate measurements from the HLW Transfer System trench piping and pits are needed to generate MicroShield™ models for these particular areas. Existing Batch 10 analytical data, STS Valve Aisle data, and THOREX waste analytical data assist in the development of the scaling factors. This information allowed for the generation of a conservatively bounded curie estimate for each of the areas (Section 7).

5.0 Sampling Procedures

5.1 HLW Transfer Trench Piping

Surveying of the HLW Transfer Trench piping was conducted in January 2004 in accordance with Work Instruction Package 99456⁽¹⁸⁾ and recorded on Radiation and Contamination Survey Report

123244⁽¹⁹⁾. Access was gained through two existing conductivity probe penetrations CS-138 and CS-271. Penetration CS-138 is located adjacent to Tank 8D-2 and CS-271 is between the 8Q-1 and 8Q-2 Pits (Appendix A). On January 20, 2004 dose rates were taken at 6-inch intervals from the bottom of the trench cover to the bottom of the trench by lowering the radiation probe through each trench penetration on a cable⁽¹⁸⁾. The dose rates were taken with a Ludlum 133-6 Geiger-Mueller Detector (Serial Number PR192701) (linear range 4 mR/hr to 10 R/hr) which is range energy compensated and halogen quenched and used for general area monitoring. The Ludlum probe was used in conjunction with a Ludlum Model 2241 Digital Survey Meter (Serial Number 151606), which is typically used with not only Geiger-Mueller detectors but can be used in proportional and scintillation detectors as well. This rate meter directly displays in R/hr. Survey readings were taken and verified in accordance with West Valley Nuclear Services Company (WVNSCO) policies and procedures as identified in the CMP (e.g., WVDP-010, "WVDP Radiological Controls Manual," RC-ADM-19, "Performing Surface Radioactivity Measurements").

5.2 Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5

Surveying of Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5 was conducted in December 2004 in accordance with existing procedures. Access was gained through existing pit cover penetrations. On December 30, 2003 dose rates were taken at 1-foot intervals from the top of the pit cover to the bottom of the pit by lowering the radiation probe through each pit penetration on a cable. Dose rate measurements were recorded on Radiation and Contamination Survey Report 122979⁽²⁰⁾. The dose rates were taken with a Ludlum 133-6 Geiger-Mueller Detector (Serial Number PR192701) (linear range 4 mR/hr to 10 R/hr) which is range energy compensated and halogen quenched and used for general area monitoring. The Ludlum probe was used in conjunction with a Ludlum Model 2241 Digital Survey Meter (Serial Number 151606), which is typically used with not only Geiger-Mueller detectors but can be used in proportional and scintillation detectors as well. This rate meter directly displays in R/hr. Survey readings were taken and verified in accordance with WVNSCO policies and procedures as identified in the CMP (e.g., WVDP-010, "WVDP Radiological Controls Manual," RC-ADM-19, "Performing Surface Radioactivity Measurements").

5.3 Previous Data Collection Activities

Sections 3.0 and 4.0 provide information on the STS Pipeway/Shield Structure piping, Waste Tank Farm HLW Legacy Piping, and M-8 Riser Pump Pit and associated piping data collection activities implemented previously that resulted in the generation of the preexisting data discussed in Sections 3.0, 4.0, and 7.0.

6.0 Sampling Results/Data Validation

6.1 HLW Transfer Trench Piping

6.1.1 Dose Rate Measurements

Dose rate measurements from the interior of the HLW Transfer Trench were taken on January 20, 2004⁽²¹⁾. The recorded dose rates are shown in Table 5.

The dose rates were taken with a Ludlum 133-4 Geiger-Mueller Detector (Serial Number PR192701) (linear range 4 mR/hr to 10 R/hr) in conjunction with a Ludlum Model 2241 Digital Survey Meter (Serial Number 151606). The calibration of the instrumentation used to take the dose rates of the Transfer Trench was performed in accordance with WVDP-318, "WVDP Radiological Instrumentation Calibration and Maintenance Program Manual," RC-IOC-1, "Administrative Aspects of Radiological Instrument Calibration and

Table 5
HLW Transfer Trench Piping Dose Rate Measurements

Insertion Depth From Bottom of Trench Cover (Inches)	Dose Rate mR/hr	
	Penetration CS-138	Penetration CS-271
0	0.8	3.2
6	1.5	6.5
12	1.8	8.3
18	2.9	8.6
24	2.9	9.7
30		9.8
36		9.0
42		9.6

- See Reference 18.

Maintenance," and applicable instrument specific calibration procedures. The dose rate data was reviewed and validated by WVNSCO. The overall conclusion of the data validation was that the January 20, 2004 dose rates were unconditionally acceptable for their intended use⁽²¹⁾.

6.2 Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5

6.2.1 Dose Rate Measurements

Dose rate measurements from the interior of Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5 were taken on December 30, 2003⁽²⁰⁾. The recorded dose rates are shown in Table 6.

The dose rates were taken with a Ludlum 133-4 Geiger-Mueller Detector (Serial Number PR192701) (linear range 4 mR/hr to 10 R/hr) in conjunction with a Ludlum Model 2241 Digital Survey Meter (Serial Number 151606). The calibration of the instrumentation used to take the dose rates of the pits were performed in accordance with WVDP-318, "WVDP Radiological Instrumentation Calibration and Maintenance Program Manual," RC-IOC-1, "Administrative Aspects of Radiological Instrument Calibration and Maintenance," and applicable instrument specific calibration procedures. The dose rate data was reviewed and validated by WVNSCO. The overall conclusion of the data validation was that the December 30, 2003 dose rates were unconditionally acceptable for their intended use⁽²²⁾.

6.3 Previously Generated Data

Sections 3.0 and 4.0 discuss the previously generated analytical results for the Batch 10 vitrification run data, STS Valve Aisle scaling factors, Tank 3D-2, and the THOREX waste sample data. The analytical data was reviewed by WVNSCO and its acceptability for use is discussed below.

6.3.1 Batch 10 Vitrification Run Data

With the exception of Tc-99 and I-129, the Batch 10 data was validated and unconditionally approved for use. The Tc-99 results were conditionally approved for use due to demonstrated interference from Ru resulting in elevated levels of Tc-99 being reported. The samples were radiochemically separated and the Tc-99 analysis repeated. Two laboratory control samples (two blank spikes) were prepared for the analysis of Tc-99. The laboratory control samples for the Tc-99 exhibited recoveries of 62% and 64%. This could indicate a possible low bias in the sample results of about 40%. However, because the matrix spike sample demonstrated an acceptable recovery, the data was not rejected but was qualified with a "J" flag and should be considered estimated. The reported values were used with no adjustments. The I-129 results were conditionally approved for use due to depressed matrix spike sample recoveries. Per the reports submitted by Pacific Northwest National Laboratory (PNNL)^(14, 15), the results reported were corrected for the average spike yield. It was also indicated that the low yield may have been caused by a loss of iodine due to light sensitivity. In recognition of this, the data validator flagged the I-129 data as estimated ("J"), indicating the results should be considered estimated and conservative.

Table 6
Dose Rate Measurements from Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5

Insertion Depth From Top of Pit Cover (Feet)	Dose Rate (mR/hr)			
	Pit 8Q-1	Pit 8Q-2	Pit 8Q-4	Pit 8Q-5
0 (Top)	0.0	10.9	0.0	0.2
2' 2"	11.2	936.0	1.4	2.7
3'	36.2	3,200	2.0	5.1
4'	49.4	5,600	2.5	5.0
5'	53.4	9,800	5.5	6.0
6'	45.2	33,500	5.2	5.5
7'	45.5	15,200	7.8	5.5
8'	51.3	7,700	16.2	N/A

- See Reference 20.

6.3.2 THOREX Waste Sample Data

Information necessary to meet current Level 1 data validation protocol for the THOREX waste sample data obtained from Reference 16 is not available. However, as reported in Reference 16, radiochemical analyses of the Tank 8D-4 THOREX samples were independently performed by both the Westinghouse Atomic Energy Services Division and Oak Ridge National Laboratory. In addition to the analytical work, an ORIGEN computer code run was made using the spent thorium fuel, irradiation, and processing parameters obtained from NFS records. ORIGEN is a computer code that models the radionuclide characterization of spent nuclear fuel based on its physical characteristics such as elemental composition. Good agreement between the analytical results and the ORIGEN run were reported which showed that the data was acceptable for use.

6.3.3 Tank 3D-2 Sample Data

Sample 3D-2 #8 (Sample 02-1765) was collected in December of 2002 and submitted to the Analytical and Process Chemistry (A&PC) Laboratory for analysis. The sample was prepared and analyzed according to approved A&PC Laboratory procedures.

Validation was accomplished by comparing the results of the data packages provided to the requirements imposed by the CMP and the approved validation procedure in place at the time. The details for each package are documented in the applicable validation packages which are maintained in the project files⁽²³⁾. Please refer to the data validation packages for the criteria utilized in the validation process.

With the exception of I-129, the data was found unconditionally acceptable for its intended use. The I-129 result in Sample 02-1765 was qualified "U", that is, undetected by the data validator. The data was qualified because the activity demonstrated was less than the Minimum Detectable Activity (MDA) for this sample. This does not impact the usability of the sample result.

6.3.4 STS Valve Aisle Scaling Factors

The following samples were collected in the STS Valve Aisle over a period encompassing December 2000 to February 2002 and submitted to the A&PC Laboratory for analysis: S-007#26 A-F (00-2427), S007#27 A-F (00-2428), R1 (01-1140), R2 (01-1141), R3 (01-1142), S-001 #1 (02-0222), S-1 #2A, #2B (02-0223), S-001 #3A, #3B (02-0224), S-001 #4A, #4B (02-0234), Valve Aisle Sump #1A (02-0307) and Valve Aisle Sump #1B (02-0308).

The samples were prepared and analyzed according to approved A&PC Laboratory procedures.

Validation was accomplished by comparing the results of the data packages provided to the requirements imposed by the applicable sample management plan and the approved validation procedure in place at the time. The details for each package are documented in the applicable validation packages which are maintained in the project files⁽²⁴⁾. Please refer to the data validation packages for the criteria utilized in the validation process.

Please note that because the data was not intended solely for the use of the Facility Characterization Project, some of the data validation packages contain an assessment of all data reported and the validation was performed to a standard other than WVDP-403. In these cases, the only data considered for this report is that of those isotopes required by the CMP.

Unless otherwise indicated below, the data was found unconditionally acceptable for its intended use.

The Np-237 results in Samples 00-2427 and 00-2428 were qualified "J", that is, estimated, by the data validator. The qualifier was assigned due to spectral interference observed in the Np-237 region of interest. Therefore, the data validator concluded that the Np-237 results for Sample 00-2427 were potentially biased high. Since the use of the reported value generates a more conservative ratio, if it is present at all, the data was utilized in establishing ratios.

The Tc-99 result in Sample 01-1142 was qualified "J" by the data validator. This qualifier was assigned because the uncertainty associated with the sample result was greater than 50% of the activity detected in the sample. Since the use of the reported value generates a more conservative ratio, if it is present at all, the data was utilized in establishing ratios. Please note that there is a typographical error in the data validation report cover sheet indicating the qualifier was assigned to Sample 01-1140. The VAST report and data validation checklist support the qualifier as assigned to Sample 01-1142.

The Cs-137 results in Samples 01-1140, 01-1141, and 01-1142 were qualified "J", that is, estimated, by the data validator. The qualifier was assigned due to contamination in the blank. Therefore, the Cs-137 results were suspected to be biased high, that is, the data validator indicated the Cs-137 may be present in quantities less than that reported. The validation report indicated however, that the activity of Cs-137 in the blank was less than 10% of that found in the samples. Therefore, any impact to the data was minimal. A positive bias of 10% is not considered significant when calculating ratios. Therefore, this data was utilized in establishing ratios.

The Cm-243/244 results in Samples 01-1140, 01-1141, and 01-1142 were qualified "J", that is, estimated, by the data validator. The qualifier was assigned due to depressed recovery of the quality control standard indicating the curium results could be biased low. The data was utilized in establishing ratios because the data validator indicated that even though the results were outside the criteria allowed by the A&PC Laboratory, they were within the limits of 80% - 120% recovery allowed by the WVNSCO data validation procedure.

The U-232, U-233/234, U-235/236, and U-238 results in Samples 01-1140, 01-1141, and 01-1142 were qualified "J", that is, estimated, by the data validator. The qualifier was assigned due to depressed recovery of the quality control standard indicating the uranium results could be biased low. The data was utilized in establishing ratios because the percent recovery was within the limits established by the laboratory.

The following isotopes were qualified "U", that is, undetected, by the data validator: Tc-99 in Sample 01-1140, I-129 in Samples 02-0307 and 02-0308, U-235/236 and U-238 in Samples 01-1141, 02-0307, and 02-0308, and U-232, U-233/234, U-235/236 and U-238 in Samples 01-1140 and 01-1142. In each case, the data was qualified because the activity demonstrated was less than the MDA for these samples. This does not impact the usability of the sample results.

6.3.5 M-8 Pump Pit

Dose rates surveys were taken of the M-8 Pump Pit in November and December 2000 per the Work Instruction Packages 0001946, 0001985, and 0002260. These surveys were performed per approved radiological protection procedures and the applicable approved work instruction document.

Validation was accomplished by comparing the result of the data packages provided to the requirements imposed by the CMP and WVDP-409, "Verification and Validation of Analytical, Field, and Dose Rate Data." The details for each package are documented in the applicable validation packages which are maintained in the project files⁽²⁵⁾.

There were no qualifiers assigned to the data and the data is acceptable for its intended use.

6.3.6 STS Jumper

Dose rate surveys were taken of the STS Valve Aisle Jumper in May 1988 and recorded on Radiation and Contamination Survey Report 060042. These surveys were performed per approved radiological protection procedures.

Validation was accomplished by comparing the result of the data packages provided to the requirements imposed by the CMP and WVDP-409. The details for each package are documented in the applicable validation packages which are maintained in the project files⁽²⁶⁾.

There were no qualifiers assigned to the data and the data is acceptable for its intended use.

7.0 Data Analysis

Dose-to-curie modeling of the balance of the Waste Tank Farm key curie contributors, with the exception of the HLW legacy piping, was conducted using MicroShield™ software. As identified in the CMP, the modeling was performed by a person trained in the use of the MicroShield™ software and the modeling calculations provided in the referenced appendices have been peer reviewed. The radionuclide inventory for the HLW legacy piping was determined from a conservative residual volume estimate and the radionuclide concentrations.

Dose-to-curie modeling inputs include a dose rate measurement, an isotopic distribution/scaling factors that can be associated with the contamination, and the configuration/dimensions of the particular area. The modeling was performed using a dose rate that was attributed solely to Cs-137. While many radioisotopes emit gamma radiation during decay, their contribution would not significantly change the dose rate due to lower energies and/or low abundance. Per the CMP, the Balance of the Tank Farm MicroShield™ modeling and associated calculated results have been decayed to the reference date of September 30, 2004. Area specific assumptions and modeling results are described below and in the supporting documentation.

7.1 HLW Transfer Trench Piping

On January 20, 2004, dose rates of the HLW Transfer Trench were collected. Dose rate measurements below the pit covers are shown in Table 5. Dose rate measurements were collected inside the trench at two locations along its length. Utilizing the dose rates collected and assuming the dose rate was due entirely to Cs-137, the piping at each survey location was modeled. The piping in the trench was modeled conservatively by using the highest dose rate measured at each survey location and assuming all radiation was from a five foot length of the individual pipeline being modeled. Dose-to-curie modeling calculations and assumptions are provided in Appendix B. Table 7 shows the application of the MicroShield™ modeling results to each pipeline segment to determine the total Cs-137 source term for the HLW Transfer Trench. It was not necessary to decay the Cs-137 source term as the survey data was within one year of September 30, 2004.

The Batch 10 vitrification run scaling factors (Table 8) were then used calculate the HLW Transfer Trench piping radionuclide inventory shown in Table 10. Calculation of the Batch 10 vitrification run scaling factors is provided in Appendix C.

7.2 Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5

On December 30, 2003, dose rates of the 8Q-1, 8Q-2, 8Q-4, and 8Q-5 pits were collected. Dose rate measurements below the pit covers are shown in Table 6. Utilizing the highest dose rate measured in each respective pit and assuming the dose rate was due entirely to Cs-137, each pit was modeled. Each pit was treated as a rectangular volume. Because the pits contain a collection of components, jumpers, pipes, and valves, an internal density had to be assigned. Using iron as the source material, a density was calculated for each pit based on the mass of the components in each pit. Dose-to-curie modeling calculations and assumptions are provided in Appendix D. Table 9 shows the component mass, internal density, and the Cs-137 source term determined for each of the pits. It was not necessary to decay the Cs-137 source term as the survey date was within one year of September 30, 2004.

The Batch 10 vitrification run scaling factors (Table 8) were then used to calculate the 8Q-1, 8Q-2, 8Q-4 and 8Q-5 radionuclide inventory shown in Table 10.

7.3 STS Pipeway/ Shield Structure Piping

Dose rate measurements of an STS Valve Aisle Jumper taken in May 1998 was 1,700 mR/hr. Using the 1998 STS Valve Aisle Jumper dose rate measurement and assuming the dose rate was due entirely to Cs-137 uniformly distributed on the internal surfaces, the jumper was modeled.

Dose-to-curie modeling calculations and assumptions are provided in Appendix E. A Cs-137 areal concentration of 138 Fci/cm^2 as of the survey date was determined for the STS Valve Aisle Jumper. When applied to the STS Pipeway/Shield Structure piping surface area estimates, a Cs-137 source term of 414 curies was calculated as shown in Appendix F.

The decay corrected STS Valve Aisle scaling factors shown in Table 11 were then used to calculate the radionuclide inventory of the associated piping shown in Table 10. Calculation of the STS Valve Aisle scaling factors is provided in Appendix G.

7.4 Waste Tank Farm HLW Legacy Piping

7.4.1 Line 7P120

The radionuclide concentrations of the THOREX waste decay corrected to September 30, 2004 were used to calculate the radionuclide inventory of the 3-inch diameter THOREX Transfer Line 7P120. A residual waste volume of 2% of the total line was conservatively estimated based on engineering judgement as explained below. This pipeline is constructed of stainless steel and welded with full-penetration butt weld joints to preclude the accumulation of waste in crud traps. In addition, the piping is sloped at a minimum of 1/16-inch per foot to promote gravity draining of the line to the waste tank. All liquids transferred via Line 7P120 were non-viscous neutronium fluids. At the low point of the line near the Tank 8D-3/8D-4 vault, there is a short 3-foot branch piping connection with a valve which results in a dead leg. About one gallon of liquid holdup is estimated from the reference Drawing 8A-I-12.

Table 7

Determination of Cs-137 Source Term for the HLW Transfer Trench

Line Segment	Pipeline	Service	Pipe Diameter (Inches)	Total Length (Feet)	Cs-137 Curies per 5 Foot Length from MicroShield™ Modeling (Appendix B)	Total Cs-137 Curies
Vitrification Facility to Tanks 8D-3 and 8D-4	55-PH-3-021	Condensate Return	3	550	0.312	34.3
	5-PH-3-003	Waste Header	3	550	0.312	34.3
Vitrification Facility to Pit 8Q-5	55-PH-2-032	Spare Sludge Transfer	2	110	0.113	2.5
	55-PH-2-033	Sludge Transfer	2	110	0.113	2.5
	55-PH-2-015	Spare Return	2	110	0.113	2.5
	55-PH-2-006	Return	2	110	0.113	2.5
Pit 8Q-5 to Pit 8Q-2	55-PH-2-005	Spare Sludge Transfer	2	213	0.113	4.8
	55-PH-2-004	Sludge Transfer	2	213	0.113	4.8
	55-PH-2-008	Return	2	213	0.113	4.8
Pit 8Q-2 to Pit 8Q-1	55-PH-2-034	THOREX Transfer	2	96	0.278	5.3
	55-PH-2-038	Zeolite Transfer	2	96	0.278	5.3
Pit 8Q-1 to Pit 8Q-4	55-PH-2-018	THOREX Transfer	2	126	0.278	7.0
	55-PH-2-014		2	126	0.278	7.0
Totals				2,623		118

Table 8
Batch 10 Scaling Factors

Project Isotope	Batch 10 Scaling Factors Decayed/Ingrown to September 30, 2004
C-14	2.03e-07
Tc-99	3.51e-05
I-129	1.62e-10
U-232	3.85e-06
U-233	1.49e-06
U-234	5.73e-07
U-235	1.58e-08
Np-237	8.30e-06
U-238	1.41e-07
Pu-238	1.55e-03
Pu-239	4.52e-04
Pu-240	3.21e-04
Pu-241	9.96e-03
Am-241	1.33e-02
Cm-243	8.96e-05
Cm-244	2.10e-03
Cs-137	1.00e+00
Sr-90	9.54e-01

Table 9

Component Mass, Internal Density, and Cs-137 Source Term for 8Q Pits

Pit	Highest Dose Rate Measurement (mR/hr)	Mass of Component (lbs)	Internal Density (g/cm³)	Cs-137 Source Term Curies*
8Q-1	53.4	382	0.0073	0.31
8Q-2	33,500	417	0.0068	221
8Q-4	16.2	927	0.059	0.051
8Q-5	6.0	N/A	3.93	0.753
Total				222.1

* See Appendix D.

Table 10

Calculation of Radionuclide Inventory for the Balance of the Tank Farm

	Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5	HLW Transfer Trench Piping	HLW Legacy Piping Pipeline 7P113 to Tank 8D-2	HLW Legacy Piping Pipeline 7P120 to Tank 8D-4	STS Pipeway/ Shield Structure	M-8 Riser Pump Pit Piping	Associated Piping (M-8 Pump Pit to STS)
Cs-137 Curies from MicroShield™	2.22e+02 (See Note 1)	1.18e+02 (See Table 7)	N/A	N/A	414.1 (See Appendix F)	3.7	74.5 (See Appendix K)
Cs-137 Curies Aged to 9/30/04	(See Note 2)	(See Note 2)	N/A	N/A	392.1	3.35	64.3
Gallons of Liquid	N/A	N/A	4 (See Appendix I)	7 (See Appendix H)	N/A	N/A	N/A
Project Isotope	Aged Batch 10 Scaling Factors		Aged Tank 3D-2 Analytical Results (VAST 02-1767) (FCi/ml)	Aged THOREX Radionuclide Distribution	Aged STS Valve Aisle Scaling Factors		
C-14	2.03e-07	2.03e-07	9.79e-05	1.09e-05	1.31e-06	1.31e-06	1.31e-06
Tc-99	3.51e-05	3.51e-05	1.16e-04	8.75e-03	2.25e-04	2.25e-04	2.25e-04
I-129	1.62e-10	1.62e-10	8.21e-05	1.51e-05	1.04e-09	1.04e-09	1.04e-09
U-232	3.85e-06	3.85e-06	2.02e-05	1.94e-04	9.12e-06	9.12e-06	9.12e-06
U-233	1.49e-06	1.49e-06	8.60e-06	1.76e-04	3.58e-06	3.58e-06	3.58e-06
U-234	5.73e-07	5.73e-07	4.11e-06	1.85e-04	1.72e-06	1.72e-06	1.72e-06
U-235	1.58e-08	1.58e-08	3.30e-08	4.35e-07	7.60e-07	7.60e-07	7.60e-07
Np-237	8.30e-06	8.30e-06	5.17e-06	2.54e-05	8.32e-06	8.32e-06	8.32e-06
U-238	1.41e-07	1.41e-07	4.21e-07	5.98e-09	5.89e-07	5.89e-07	5.89e-07
Pu-238	1.55e-03	1.55e-03	1.35e-03	3.51e-02	1.56e-03	1.56e-03	1.56e-03
Pu-239	4.52e-04	4.52e-04	9.07e-04	1.30e-03	4.86e-04	4.86e-04	4.86e-04
Pu-240	3.21e-04	3.21e-04	6.93e-04	6.80e-04	8.65e-04	8.65e-04	8.65e-04
Pu-241	9.96e-03	9.96e-03	1.23e-02	3.04e-02	9.97e-03	9.97e-03	9.97e-03
Am-241	1.33e-02	1.33e-02	5.79e-03	2.11e-02	1.34e-02	1.34e-02	1.34e-02
Cm-243	8.96e-05	8.96e-05	2.38e-05	1.28e-05	8.96e-05	8.96e-05	8.96e-05
Cm-244	2.10e-03	2.10e-03	6.08e-04	5.83e-04	2.11e-03	2.11e-03	2.11e-03
Cs-137	1.00e+00	1.00e+00	2.23e+00	2.56e+01	1.00e+00	1.00e+00	1.00e+00
Sr-90	9.54e-01	9.54e-01	1.88e-01	1.80e-01	9.58e-01	9.58e-01	9.58e-01

Table 10 (Continued)

Project Isotope	Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5	HLW Transfer Trench Piping	HLW Legacy Piping Pipeline 7P113 to Tank 8D-2	HLW Legacy Piping Pipeline 7P120 to Tank 8D-4	STS Pipeway/ Shield Structure Piping	M-8 Riser Pump Pit	Associated Piping (M-8 Pump Pit to STS)	Totals
Balance of Tank Farm Inventory Decayed/Ingrown to September 30, 2004								
C-14	4.52e-05	2.40e-05	1.48e-06	7.63e-05	5.14e-04	4.39e-06	8.42e-05	7.49e-04
Tc-99	7.79e-03	4.14e-03	1.76e-06	6.13e-02	8.82e-02	7.54e-04	1.45e-02	1.77e-01
I-129	3.59e-08	1.91e-08	1.24e-06	1.06e-04	4.08e-07	3.48e-09	6.69e-08	1.19e-04
U-232	8.56e-04	4.55e-04	3.06e-07	1.36e-03	3.58e-03	3.06e-05	5.86e-04	6.86e-03
U-233	3.32e-04	1.76e-04	1.30e-07	1.23e-03	1.40e-03	1.20e-05	2.30e-04	3.39e-03
U-234	1.27e-04	6.76e-05	6.22e-08	1.30e-03	6.74e-04	5.76e-06	1.11e-04	2.28e-03
U-235	3.50e-06	1.86e-06	5.00e-10	3.05e-06	2.98e-04	2.55e-06	4.89e-05	3.58e-03
Np-237	1.84e-03	9.79e-04	7.83e-08	1.78e-04	3.26e-03	2.79e-05	5.35e-04	6.82e-03
U-238	3.13e-05	1.66e-05	6.37e-09	4.19e-08	2.31e-04	1.97e-06	3.79e-05	3.19e-04
Pu-238	3.45e-01	1.83e-01	2.04e-05	2.46e-01	6.12e-01	5.23e-03	1.00e-01	1.49e+00
Pu-239	1.00e-01	5.34e-02	1.37e-05	9.10e-03	1.91e-01	1.63e-03	3.12e-02	3.86e-01
Pu-240	7.13e-02	3.79e-02	1.05e-05	4.76e-03	3.39e-01	2.90e-03	5.56e-02	5.12e-01
Pu-241	2.21e+00	1.18e+00	1.86e-04	2.13e-01	3.91e+00	3.34e-02	6.41e-01	8.18e+00
Am-241	2.96e+00	1.57e+00	8.77e-05	1.48e-01	5.25e+00	4.49e-02	8.62e-01	1.08e+01
Cm-243	1.99e-02	1.06e-02	3.60e-07	8.96e-05	3.51e-02	3.00e-04	5.76e-03	7.18e-02
Cm-244	4.67e-01	2.48e-01	9.21e-06	4.08e-03	8.27e-01	7.07e-03	1.36e-01	1.69e+00
Cs-137	2.22e+02	1.18e+02	3.38e-02	1.79e+02	3.92e+02	3.35e+00	6.43e+01	9.79e+02
Sr-90	2.12e+02	1.13e+02	2.73e-03	1.74e+02	3.76e+02	3.21e+00	6.16e+01	9.39e+02

Notes:

- 1 Sum of MicroShield™ modeling results: 8Q-1 (0.31 Ci); 8Q-2 (221 Ci); 8Q-4 (0.051 Ci); 8Q-5 (0.75 Ci).
- 2 The aging of MicroShield™ results was not required since, per the CMP, the surveys were taken within one year of September 30, 2004.

Table 11

**STS Valve Aisle Scaling Factors
Decayed to September 30, 2004**

Project Isotope	STS Valve Aisle Scaling Factors Decayed to 9/30/04
C-14	1.31e-06
Tc-99	2.25e-04
I-129	1.04e-09
U-232	9.12e-06
U-233	3.58e-06
U-234	1.72e-06
U-235	7.60e-07
Np-237	8.32e-06
U-238	5.89e-07
Pu-238	1.56e-03
Pu-239	4.86e-04
Pu-240	8.65e-04
Pu-241	9.97e-03
Am-241	1.34e-02
Cm-243	8.96e-05
Cm-244	2.11e-03
Cs-137	1.00e+00
Sr-90	9.58e-01

Calculations and assumptions are provided in Appendix H. The calculated radionuclide inventory is also shown in Table 10.

7.4.2 Line 7P113

The radionuclide concentrations of the Tank 3D-2 liquid waste sample decay corrected to September 30, 2004 were used to calculate the radionuclide inventory of the Tank 8D-2 3-inch diameter Waste Transfer Line 7P113. A residual waste volume of 2% of the total line was conservatively estimated based on engineering judgement as explained above. Calculations and assumptions are provided in Appendix I. The calculated radionuclide inventory is shown in Table 10.

7.5 M-8 Riser Pump Pit and Associated Piping

7.5.1 M-8 Riser Pump Pit

The interior dose rate measurements of the M-8 Riser Pump Pit were collected in November and December 2000 during STS flushing operations. Surveys were taken through existing valve access ports in the pit cover located 65 inches from the top of the pit covers into the pit. Dose rates ranged from 722 mR/hr to 1,244 mR/hr. Using the highest dose rate measurement in the pit and assuming the dose rate was due entirely to Cs-137, each pit was modeled. The pits were treated as a rectangular volume. Because the pits contain a collection of components, pipes, and valves, an internal density had to be assigned. A density of 0.21 g/cm³ was calculated based on the components in the pit and iron was used as a source material.

Dose-to-curie modeling calculations and assumptions are provided in Appendix J. A Cs-137 source term of 3.7 curies was determined for the M-8 Riser Pump Pit.

The decay corrected STS Valve Aisle Scaling Factors shown in Table 11 were then used to calculate the M-8 Riser Pump Pit radionuclide inventory shown in Table 10.

7.5.2 Associated Piping (M-8 Pump Pit to STS)

A dose rate measurement of an STS Valve Aisle jumper taken in May 1998 was 1,700 mR/hr. Using the 1998 valve aisle jumper dose rate measurement and assuming the dose rate was due entirely to Cs-137 uniformly distributed on the internal surfaces, the jumper was modeled.

Dose-to-curie modeling calculations and assumptions are provided in Appendix E. A Cs-137 areal concentration of 138 Fci/cm² was determined for the STS valve aisle jumper. When applied to the approximately 900 feet of 2 ½ inch Schedule 40 stainless steel piping which runs between the STS and M-8 Pump Pit, a Cs-137 source term of 74.5 Cs-137 curies was calculated as shown in Appendix K.

The decay corrected STS Valve Aisle scaling factors were then used to calculate the radionuclide inventory of the STS to M-8 Pump Pit piping shown in Table 10.

7.6 Total Curie Estimate

Summing the conservatively estimated curie contributions from each of the key curie contributing areas in the balance of the Waste Tank Farm, the conservative curie estimate for the entire balance of the Waste Tank Farm (decayed/ingrown to September 30, 2004) was calculated (Appendix L) and is shown in Table 12.

The sum total of performance assessment radioisotopes, as depicted in Table 12 (minus Cs-137 and Sr-90), is approximately 23.3 curies.

Table 12
Total Performance Assessment Radionuclides
for the Balance of Tank Farm*
(Decayed and Ingrown to September 30, 2004)

Project Isotope	Total Curies
C-14	7.49e-04
Tc-99	1.77e-01
I-129	1.19e-04
U-232	6.86e-03
U-233	3.39e-03
U-234	2.28e-03
U-235	3.58e-03
Np-237	6.82e-03
U-238	3.19e-04
Pu-238	1.49e+00
Pu-239	3.86e-01
Pu-240	5.12e-01
Pu-241	8.18e+00
Am-241	1.08e+01
Cm-243	7.18e-02
Cm-244	1.69e+00
Cs-137*	9.79e+02
Sr-90**	9.40e+02

* The method for choosing the project isotopes is outlined in WVDP-403, "Characterization Management Plan for the Facility Characterization Project" (CMP).

** Cs-137 and Sr-90 are not critical radionuclides for the outcome of the performance assessment but are reported for completeness per WVDP-403.

8.0 Data Limitations

The curie estimates identified above were generated to meet the objectives of the Facility Characterization Project and to facilitate their potential use in the site's performance assessment model. The technical approach, model inputs and assumptions, and the conclusion that the generated curie estimates are conservatively bounding, has been reviewed and validated/approved by the project's Technical Review and Approval Panel (Appendix M) pursuant to the requirements of the CMP.

9.0 References

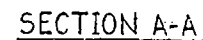
1. WVDP-403, "Characterization Management Plan for the Facility Characterization Project" (2002).
2. WVNSCO Radiation and Contamination Survey Report 57042, February 21, 1998.
3. Routine Radiation and Contamination Survey Report 1Nw2004 (PVS Building), December 27, 2003.
4. Routine Radiation and Contamination Survey Report 1Aw2004 (Waste Tank Farm), December 27, 2003.
5. WVDP-EIS-017, "High-Level Waste/Vitrification Facility Characterization Study," Revision 1, Page Change 1, September 28, 1995.
6. URS Report, "Conceptual Approach for the Integrated Closure of Waste Management Areas 1 & 3," September 13, 2002.
7. WVNS-IRP-005, "HLW Processing Systems Flushing Operations Run Plan," Revision 4, April 29, 2002.
8. RIR-403-007, "Supernatant Treatment System (STS) Valve Aisle Radioisotope Inventory Report,"
9. Radiation and Contamination Survey Report 060042 for STS Valve Aisle Operating Aisle, May 8, 1998.
10. Reithmiller, G. Ellis, "History of Decontamination," Nuclear Fuel Services, 1981.
11. Work Order STS0001946, "Perform Flush of STS Flush Path #4," October 23, 2000.
12. Work Order STS0001985, "Perform Flush of STS Flush Path #2," October 30, 2000.
13. Work Order STS0002260, "Perform Flush of STS Flush Path #3," December 7, 2000.
14. Pacific Northwest National Laboratory Report WVSP 00-28, "WVDP Radioactive Waste Characterization Letter Report - Part 1: Physical, Chemical, and Radiochemical Analytical Data," March 2000.
15. Pacific Northwest National Laboratory Report WVSP 01-07, "WVDP Radioactive Waste Characterization Letter Report - Part 3: Iodine-129 Measurement by Low Energy Photon Spectrometry (LEPS)," November 2000.
16. Topical Report DOE/NE/44139-14 "High-Level Waste Characterization at West Valley," June 2, 1986.
17. URS Memorandum, Wolniewicz, J., "Nuclide Ratios for Use in the Facility Characterization Project," Memorandum to L. Michalczak, July 29, 2002.

18. Work Instruction Package 99456, "Radiation Readings in SMS Trench to Support Facility Characterization," January 2004.
19. Radiation and Contamination Survey Report 123244, January 20, 2004.
20. Radiation and Contamination Survey Report 122979, December 30, 2003.
21. Data Validation Package 2004-012 - HLW Transfer Trench Dose Rate Surveys, January 28, 2004.
22. Data Validation Package 2004-002 - Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5 Dose Rate Surveys, January 8, 2004.
23. Data Validation Package 2003-32 - Laboratory Report 03-1765, Tank 3D-2 Sample, March 17, 2003.
24. Data Validation for S007 #26 A - F, Laboratory Report 00-2427; Data Validation for S007 #27 A - F, Laboratory Report 00-2428; Data Validation for R1, R2, and R3, Laboratory Report 01-1140, 01-1141, and 01-1142; Data Validation for S-001 #1, S-001 #2AB, S-001 #AB, and S-001 #4AB, Laboratory Reports 02-0222, 02-0223, 02-0224, and 02-0234; Data Validation for Sump #1A and Sump #1B, Laboratory Reports 02-0307 and 02-0308.
25. WVNSCO Data Validation Package 2004-003 - M-8 Pit and STS Valve Aisle Dose Rate Surveys, January 26, 2004.
26. WVNSCO Data Validation Packages 2004-014 - STS Valve Aisle Jumper Dose Rate Surveys, January 29, 2004.

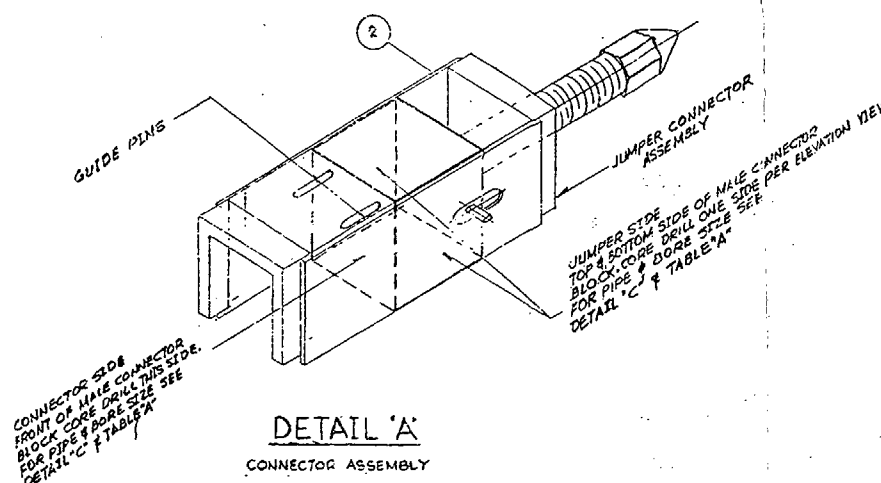
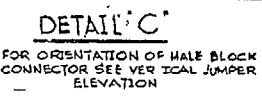
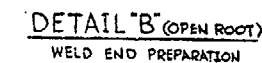
Appendix A

Drawings 900D-1079, 900D-1170, 900D-1305 Sheets 1 & 10, 900D-2826, 903D-055 - 903D-059,
904D-060 Sheets 1-5, 904D-125, 904D-126, 904D-127, 904D-128, 904D-140 - 904D-144,
904D-146, 8A-L-1, 8A-L-10, 8A-L-12, 8A-L-13, 8B-M-591, 8B-M-4, and 900D-1175

EXPANSION OF JOINT TYPE, MAX.	POSITION TOP, BOTTOM	JUMPER NUMBER	"A"	"B"	"C"	JUMPER LINE NO.	VALVE SIZE VALVE NO.	VALVE HANDLE ORIENTATION	"D"	LIMIT SWITCH	GRID COORDINATE	"E"
4 3/4"	TOP	J10	18"	10"	6"	1 1/2-013	1 1/2 FV402B	LEFT	1.6101D	YES	63133, J5733	1.6101D
6"	BOTTOM	J12	22 1/2"	11 1/2"	6"	1 1/2-062	1 1/2 FV403	RIGHT	1.6101D	YES	6155, J5155	1.6101D
4 3/4"	TOP	J13	18"	10"	6"	1 1/2-005	1 1/2 FV401	LEFT	1.6101D	YES	J17, L17	1.6101D
4 3/4"	TOP	J17	18"	10"	6"	1 1/2-012	1 1/2 FV302B	LEFT	1.6101D	YES	4520, J520	1.6101D
6"	BOTTOM	J19	22 1/2"	11 1/4"	6"	1 1/2-061	1 1/2 FV303	RIGHT	1.6101D	YES	622, J522	1.6101D
4 3/4"	TOP	J20	18"	10"	6"	1 1/2-009	1 1/2 FV301	LEFT	1.6101D	YES	J235, L235	1.6101D
4 3/4"	TOP	J24	18"	10"	6"	1 1/2-011	1 1/2 FV202B	LEFT	1.6101D	YES	63245, J5245	1.6101D
6"	BOTTOM	J26	22 1/2"	11 1/4"	6"	1 1/2-060	1 1/2 FV203	RIGHT	1.6101D	YES	6285, J5285	1.6101D
4 3/4"	TOP	J27	18"	10"	6"	1 1/2-008	1 1/2 FV201	LEFT	1.6101D	YES	J30, L30	1.6101D
4 3/4"	TOP	J31	18"	10"	6"	1 1/2-010	1 1/2 FV202B	LEFT	1.6101D	YES	6333, J533	1.6101D
6"	BOTTOM	J33	22 1/2"	11 1/2"	6"	1 1/2-009	1 1/2 FV103	RIGHT	1.6101D	YES	636, J536	1.6101D
4 3/4"	TOP	J34	18"	10"	6"	1 1/2-047	1 1/2 FV101	LEFT	1.6101D	YES	J164, L164	1.6101D
4 3/4"	BOTTOM	J48	18"	10"	6"	1 1/2-010	1 1/2 FV202B	RIGHT	1.6101D	YES	D12, F12	1.6101D
4 3/4"	TOP	J50	18"	10"	6"	1 1/2-131	1 1/2 FV092	RIGHT	1.6101D	YES	D13, F13	1.6101D
4 3/4"	TOP	J52	18"	10"	6"	1 1/2-053	1 1/2 FV401	LEFT	1.6101D	YES	F15, F15	1.6101D
4 3/4"	TOP	J57	18"	10"	6"	1 1/2-052	1 1/2 FV307	LEFT	1.6101D	YES	D20, F20	1.6101D
4 3/4"	TOP	J60	18"	10"	6"	1 1/2-042	1 1/2 FV066	LEFT	1.6101D	YES	D23, F23	1.6101D
4 3/4"	BOTTOM	J61	18"	10"	6"	1 1/2-075	1 1/2 FV083	RIGHT	1.6101D	NO	D24, F24	1.6101D
4 3/4"	BOTTOM	J62	18"	10"	6"	1 1/2-067	1 1/2 FV084	LEFT	1.6101D	NO	D26, F26	1.6101D
4 3/4"	TOP	J63	18"	10"	6"	1 1/2-051	1 1/2 FV207	LEFT	1.6101D	YES	D27, F27	1.6101D
4 3/4"	TOP	J68	18"	10"	6"	1 1/2-050	1 1/2 FV107	RIGHT	1.6101D	YES	D32, F32	1.6101D
4 3/4"	TOP	J74	18"	9 1/2"	6"	1"-040	1"-FV018	LEFT	1.0491D	YES	C30, L30	1.0491D
4 3/4"	BOTTOM	J75	18"	10"	6"	1 1/2-001	1 1/2 FV077	LEFT	1.6101D	NO	C35, F35	1.6101D



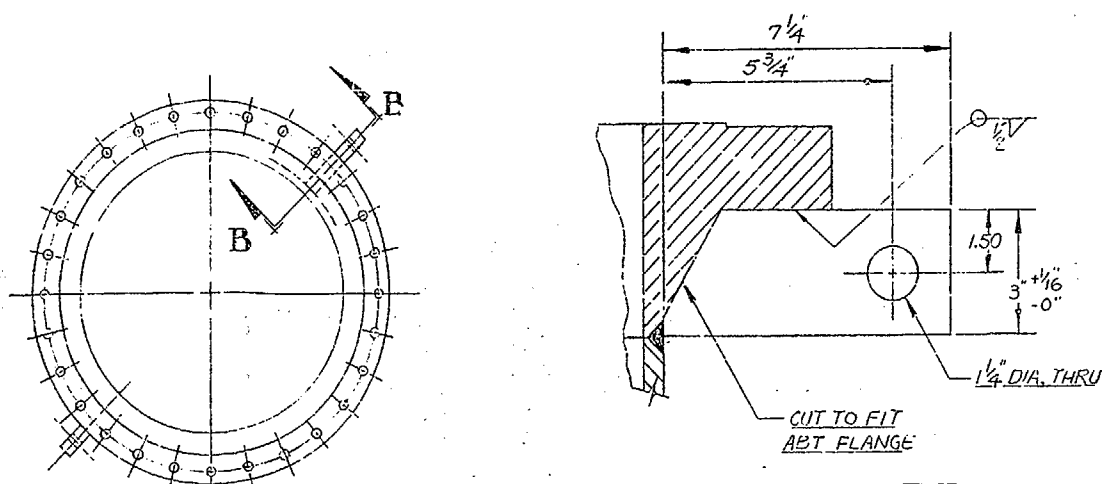
7) JUMPER #27(J30,L30), WAS REPLACED BY JUMPER #J49



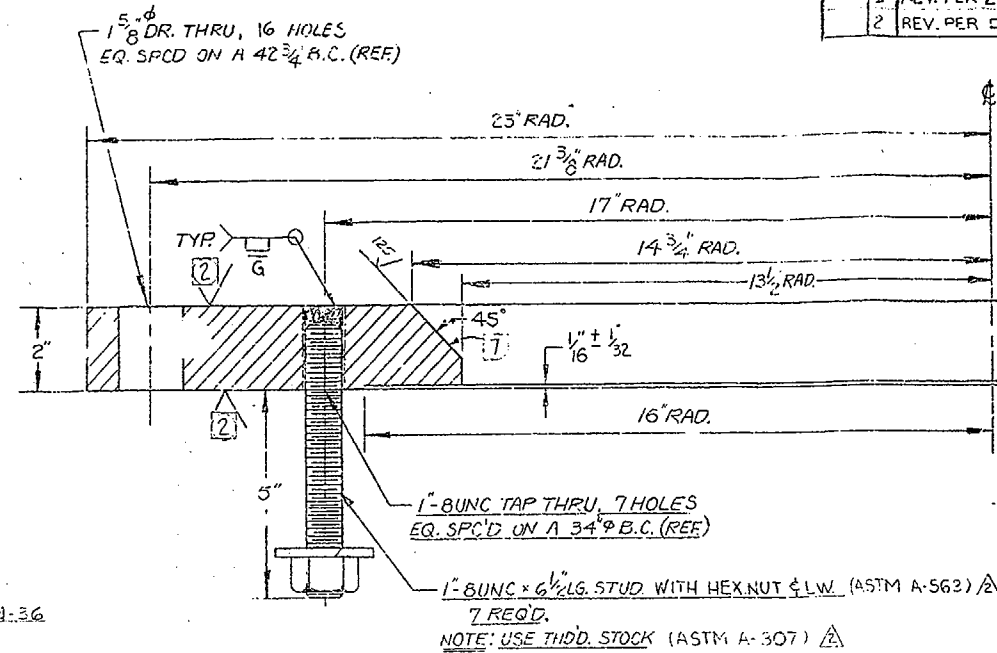
1. VALVE AISLE FRONT FACE JUMPER LOCATION
ELEVATION A-A 900D-1080, SH. 2
2. WVN: JUMPER DETAILS DWG 900D-D-813
3. ISA DATA SHEETS FOR VALVES WVN-1S-097
4. ITT GRUNDEL MANUAL BALLVALVE DETAILS 900D-1089
5. STD LEAK TEST VALVE FOR VERTICAL JUMPERS 900D-1441

FOR DRAWING INDEX SEE DRAWING NO.				APPROV. DESIG. CO. <i>10/10/68</i> PROJECT NO. <i>10/10/68</i> ENG. DES. <i>10/10/68</i> LEAD DISC. ENGR. <i>10/10/68</i> DEEL. <i>10/10/68</i> CHECKED <i>10/10/68</i> DRAWN: <i>10/10/68</i> DATE <i>10/10/68</i>	
APPROV. DESIG. CO. <i>10/10/68</i> PROJECT NO. <i>10/10/68</i> ENG. DES. <i>10/10/68</i> LEAD DISC. ENGR. <i>10/10/68</i> DEEL. <i>10/10/68</i> CHECKED <i>10/10/68</i> DRAWN: <i>10/10/68</i> DATE <i>10/10/68</i>				EBASCO SERVICES INCORPORATED A/E O.P.S. NO. 2388 TASK ORDER 013 FOR WEST VALLEY NUCLEAR SERVICES COMPANY, INC WEST VALLEY, NEW YORK	
APPROV. DESIG. CO. <i>10/10/68</i> PROJECT NO. <i>10/10/68</i> ENG. DES. <i>10/10/68</i> LEAD DISC. ENGR. <i>10/10/68</i> DEEL. <i>10/10/68</i> CHECKED <i>10/10/68</i> DRAWN: <i>10/10/68</i> DATE <i>10/10/68</i>				WEST VALLEY DEMONSTRATION PROJECT FRONT FACE VERTICAL JUMPER MANUAL VALVE ASSEMBLY	
APPROV. DESIG. CO. <i>10/10/68</i> PROJECT NO. <i>10/10/68</i> ENG. DES. <i>10/10/68</i> LEAD DISC. ENGR. <i>10/10/68</i> DEEL. <i>10/10/68</i> CHECKED <i>10/10/68</i> DRAWN: <i>10/10/68</i> DATE <i>10/10/68</i>				SIZE INDEX CODE NUMBER DRAWING NO. REV. AREA DR. TYP. CL. ORIE. <i>900d-1079</i> 5 SUBTRACT NO. SH.1 SPEC. CODES A/E SHEET NO. SK-M-211 SH 1 B	

REVISIONS			
ZONE	REV	DESCRIPTION	DATE
	0	E.L. 370	3/15/86
	1	REV. PER E.C.N. No. 485 & 700	5/15/86
	2	REV. PER E.C.N. 742-796 & 253	6/27/86



—SECTION B-B—
TYP. 2 PLATES LOCATED
180° APART, ROTATED 45°
AS SHOWN STRADDLING HOLES
—MAT'L: CARB. STL. 1/2" THK. ASTM A-36
—SCALE: 1/2

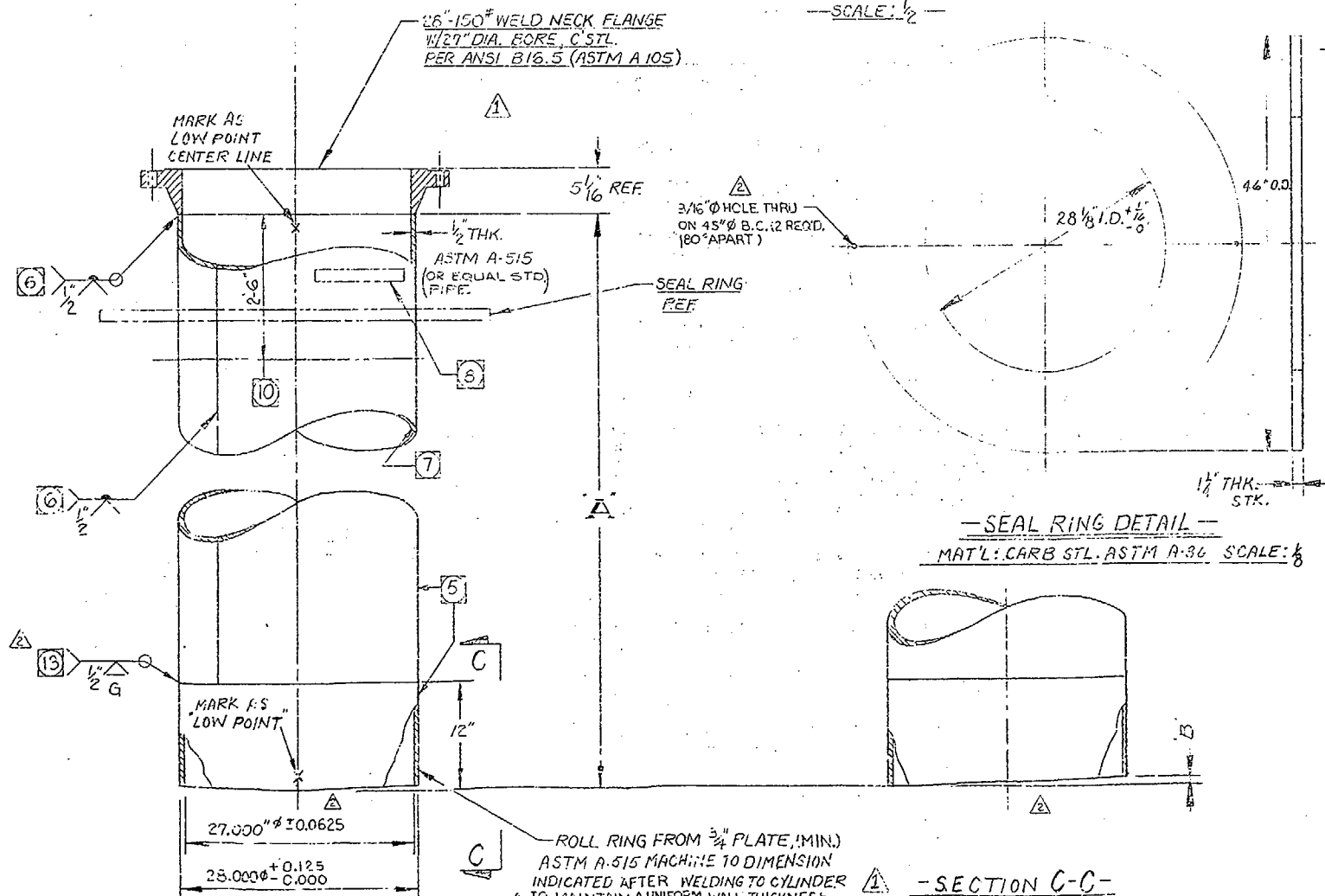


—ADAPTER PLATE FOR 28" Ø RISER—
MAT'L: CARB. STL. ASTM A-36
SCALE: 1/2

GENERAL NOTES: (UNLESS OTHERWISE SPECIFIED)

- DIMENSIONING AND TOLERANCING PER ANSI Y 14.5 TOLERANCES: .XX ± .01, ANGULAR ± 1°, FRACTIONAL ± 1/8" UNLESS NOTED.
- ALL MACHINE SURFACES 250 IN ACCORDANCE WITH ANSI B46.1 (LATEST REVISION).
- BREAK ALL SHARP EDGES, REMOVE ALL BURRS.
- MATERIAL SHALL BE AS SPECIFIED ANY MATERIAL SUBSTITUTION REQUIRES WRITTEN APPROVAL OF WIVINS.
- ASTM-A-515 PLATE TO BE ROLLED ACCORDING TO ASTM-A-671, CLASS 10 SPECIFICATIONS.
- LONGITUDINAL AND CIRCUMFERENTIAL BUTT JOINTS SHALL BE WELDED AND VISUALLY INSPECTED (VT) IN ACCORDANCE WITH AWS D1.1, STRUCTURAL WELDING CODE, SECTION 10.17.1, OR ASME SECT. IX ARTICLE II. IN ADDITION, A VACUUM BOX TEST, OR PRESS. TEST PER ASME BOILER AND PRESSURE VESSEL CODE, SECTION V SHALL BE CONDUCTED ON THE RISER WELDS AT TIME OF MANUFACTURE.
- APPLY AMERCOAT 90 EPOXY, AMERON INC. TO INTERIOR SURFACE PER MANUFACTURER'S INSTRUCTIONS. COAT TO AN AVERAGE THICKNESS OF 3-10 MILS. DO NOT APPLY TO MACHINED AREA.
- MARK WHERE NOTED WITH TANK NO. AND RISER NO. USING 1 IN. STENCIL AND WHITE PAINT.
- WELD METAL TO JOIN CARBON STEEL TO CARBON STEEL SHALL BE AWS-A5.1E70XX, OR PER ASME, SECTION IX ARTICLE IV, QW-442.
- SEAL RING SHALL BE SHOP FIT AROUND TOP 2.5' LENGTH OF RISER PRIOR TO WELDING THE WELD NECK FLANGE. GRIND RISER WHERE NECESSARY FOR FIT. WIRE RING TO LIFTING EARS.
- PROVIDE INTERNAL STEEL SUPPORT FOR BOTTOM LENGTH TO PROTECT DIA. TOLERANCE DURING SHIPMENT AND STORAGE. NO WELDING PERMITTED.
- FOR GENERAL NOTES—SEE DWG. 903D-111
- BACK-STEP WELDING METHOD IS RECOMMENDED FOR MACHINED RING TO CYLINDER WELD TO MINIMIZE INTERNAL STRESS IN 12" LONG RING.

RISER DATA		
TANK NUMBER	RISER NUMBER	DIM. "A" ± 1/4
8D-1	M-2	17'-0 3/4"
8D-1	M-5	17'-0 3/4"
8D-1	M-6	17'-9"
8D-1	M-7	17'-4"
8D-1	M-8	6'-11"
8D-2	M-2	17'-10"
8D-2	M-3	17'-10"
8D-2	M-4	17'-9 1/4"
8D-2	M-5	17'-8 1/2"
8D-2	M-6	17'-8 1/2"
8D-2	M-7	17'-9 1/4"
8D-2	M-8	8'-1 1/2"
8D-2	M-9	7'-1"



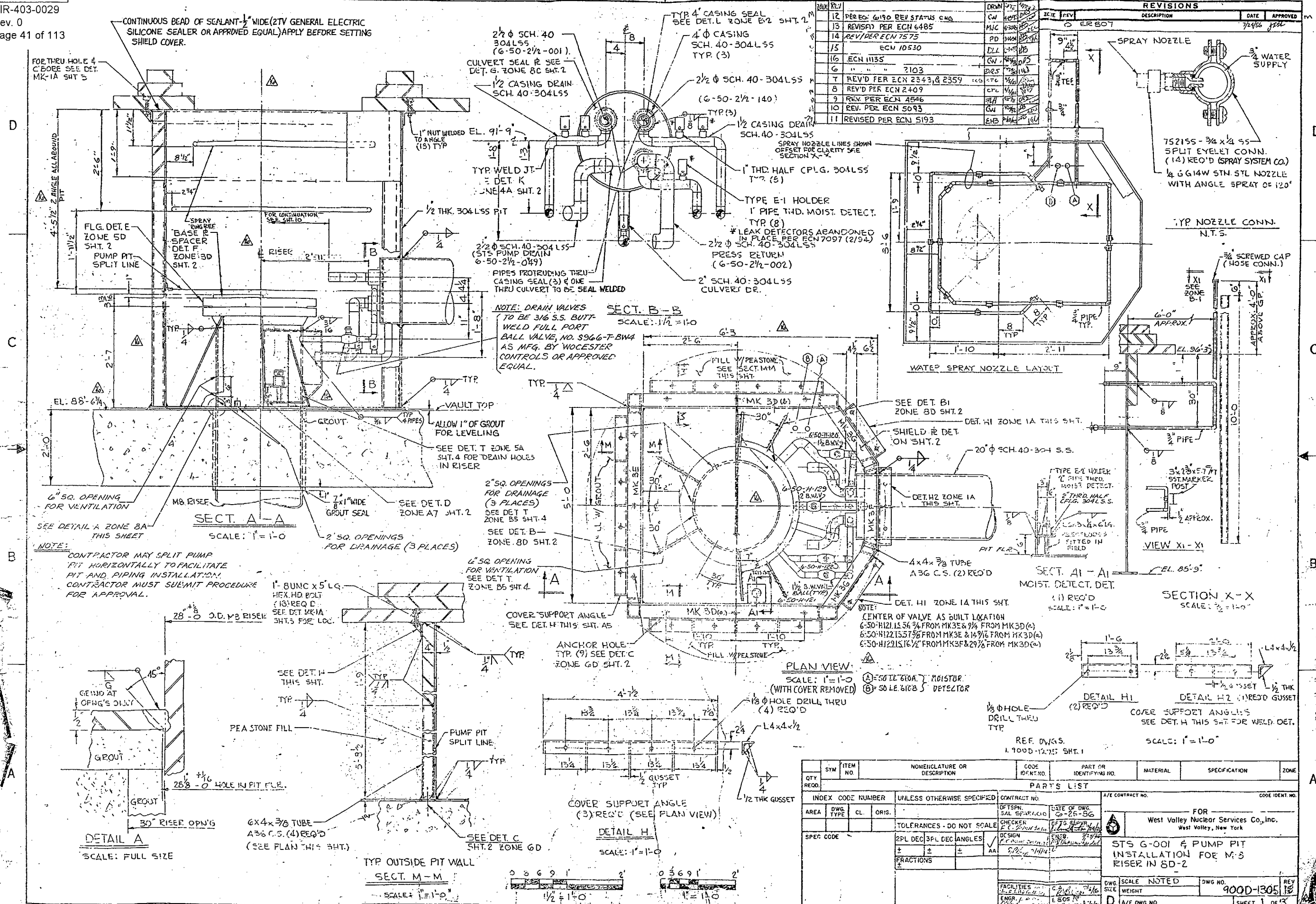
—SECTION C-C—

TANK RISERS	"B" DIM. ± 1/16"
8D-1	0.467"
8D-2	TO BE CUT TRUE & SQ.

1 —RISER—
MAT'L. AS NOTED

ROLL RING FROM 3/4" PLATE (MIN.)
ASTM A-515 MACHINE TO DIMENSION
INDICATED AFTER WELDING TO CYLINDER
TO MAINTAIN A UNIFORM WALL THICKNESS
TOLERANCES ONLY APPLIES TO THE 12" LONG
MACHINED RING

SYM	ITEM NO.	NOMENCLATURE OR DESCRIPTION	CODE IDENT. NO.	PART OR IDENTIFYING NO.	MATERIAL	SPECIFICATION	ZONE
PARTS LIST							
INDEX	CODE NUMBER	UNLESS OTHERWISE SPECIFIED	CONTRACT NO.	DATE OF DOW.	FOR		
AREA	DWG. TYPE	CL.	OPIC.	CHECKER	West Valley Nuclear Services Co., Inc.		
800	78	55	01	DATE OF DOW.	West Valley, New York		
SPEC CODE	2PL DEC	SPL DEC	ANGLES	DESIGN	—HLW-TANK FARM 8D-1 & 2—		
	± .01	± .0625	±	AA	MOBILIZATION PUMP RISER DETAILS		
	FRACTIONS 1/8				DWG. SCALE NOTED		
					DWG. NO. 700D-1170		
					REV 2		
					SHEET 1 OF 1		

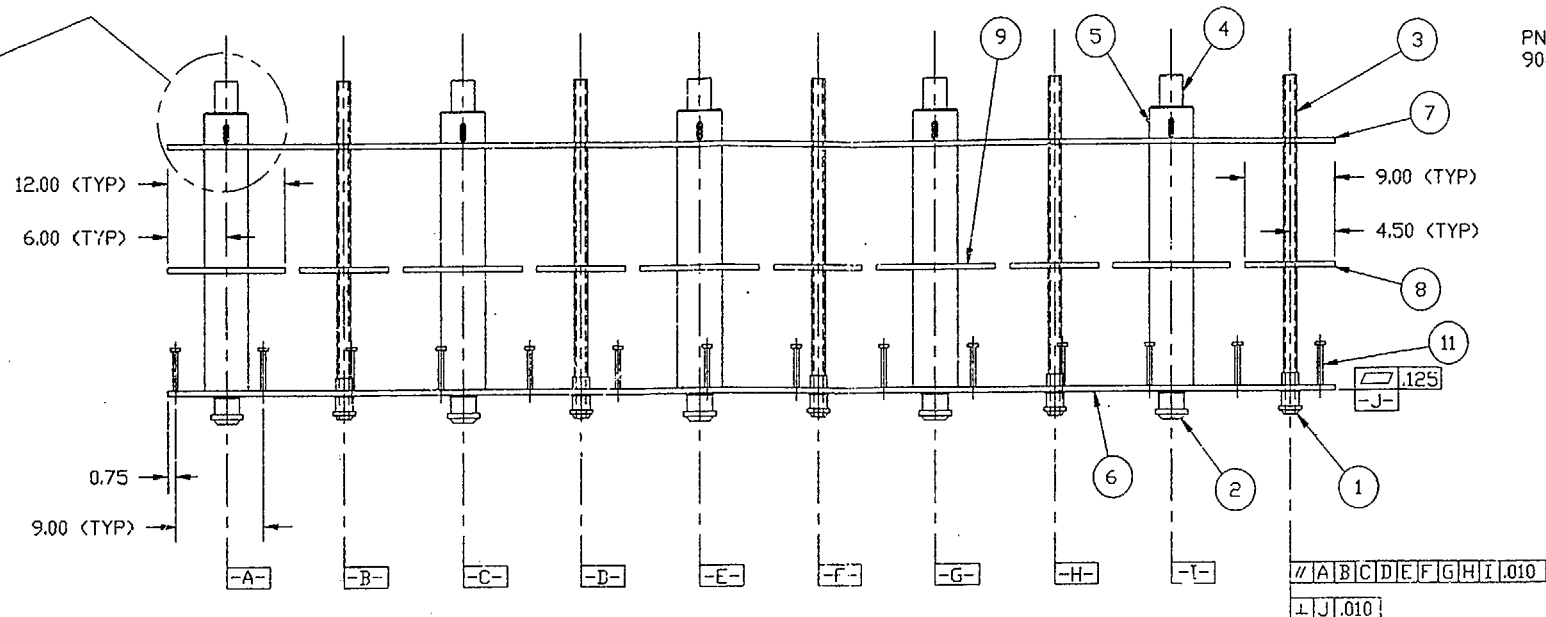
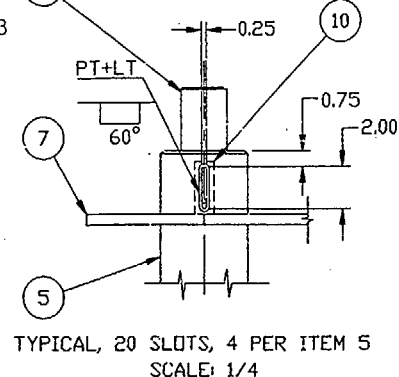


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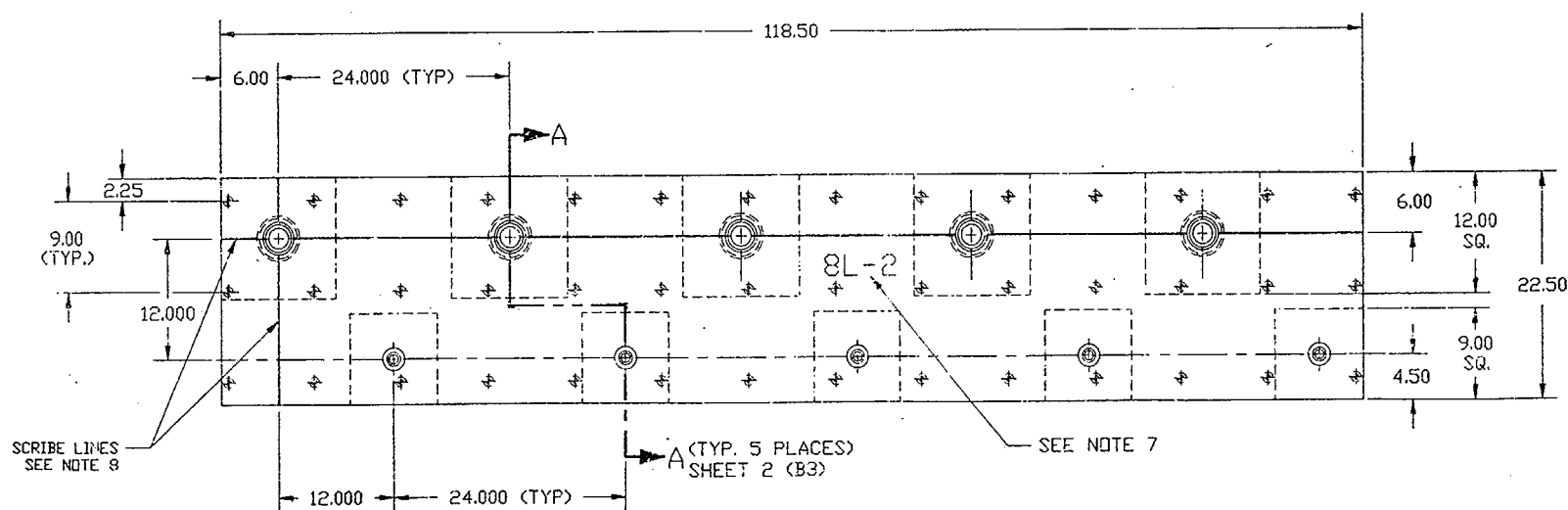
DWG NO 900D-2826 1

REFERENCE DRAWINGS:

PNL - 704-02 8Q-2 PUMP PIT LINER LAYOUT
904D - 130 SMS 8Q-2 PUMP PIT LINER PLAN & SECTIONS



PLAN VIEW



ELEVATION VIEW

- 8 - PERMANENT SCRIBE LINES, .005" x .010" WIRE SHALL SERVE AS DATUMS FOR INSTALLATION OF THE WALL EMBEDMENTS. SCRIBE LINES TO EXTEND THE FULL WIDTH AND HEIGHT OF THE 1/2" SST PLATE AND ARE TO BE PRESERVED THROUGHOUT ASSEMBLY.
- 7 - IDENTIFICATION NUMBERS SHALL BE 2" IN HEIGHT AND STENCILED ON USING BLACK AMERLOCK 490 HIGH SOLIDS EPOXY COATING IN ACCORDANCE WITH AMERON PROTECTIVE COATINGS DIVISION APPLICATION INSTRUCTIONS
- 6 - SENSITIVE LEAK TEST SHALL BE PERFORMED IN ACCORDANCE WITH PARAGRAPH 345.8 OF ANSI/ASME B31.3.
- 5 - RADIOGRAPHIC EXAMINATION SHALL BE PERFORMED IN ACCORDANCE WITH PARAGRAPH 344.5 OF ANSI/ASME B31.3.

- 4 - LIQUID DYE PENETRANT EXAMINATION SHALL BE PERFORMED IN ACCORDANCE WITH PARAGRAPH 344.4 OF ANSI/ASME B31.3.
- 3 - ALL WELDS SHALL BE VISUALLY INSPECTED IN ACCORDANCE WITH PARAGRAPH 344.2 OF ANSI/ASME B31.3 FOR PIPING AND AWS D11 SECTION 6.0 FOR STRUCTURAL WELDS.
- 2 - ALL WELDING SHALL BE IN ACCORDANCE WITH AWS D11 FOR STRUCTURAL WELDS AND ANSI/ASME B31.3 FOR PIPING.

WVNS SUPPLIED

NOTES:

A/R 11	NELSON STUD, 1/2 X 4-1/8 TYPE H4L		A-240, 304L
A/R 10	PLATE, 1/2 THK.		A-240, 304L
A/R 9	PLATE, 1/2 THK.		A-240, 304L
A/R 8	PLATE, 1/2 THK.		A-240, 304L
A/R 7	PLATE, 1/2 THK.		A-240, 304L
A/R 6	PLATE, 1/2 THK.		A-240, 304L
A/R 5	4 DIA. PIPE SCHED 40S, SMLS		A-312, 304L
A/R 4	2 DIA. PIPE SCHED 40S, SMLS		A-312, 304L
A/R 3	1 DIA. PIPE SCHED 80S, SMLS		A-312, 304L
A/R 2	2 DIA. MALE CONN. NOZ.	DWG PNL-334-01	A-351, CD-4MCU
A/R 1	1 DIA. MALE CONN. NOZ.	DWG PNL-334-01	A-351, CD-4MCU

PARTS LIST		CODE IDENT. NO.	
QTY	ITEM NO.	NOMENCLATURE OR DESCRIPTION	PART OR IDENTIFYING NO. MATERIAL OR SPEC
UNLESS OTHERWISE SPECIFIED			
ALL DIMENSIONS IN INCHES		TOLERANCES-DO NOT SCALE	
2 PL DEC 3 PL DEC ANGLES N/A		FRACTIONS N/A	
D.SPEC NO. 1579		NEXT ASSEMBLY	
DRAFTED W. KOCH		CHECKED K. QUEALY	
DATE 10/30/89		DATE 2/8/90	
ENGR. P. BEDNARZ		DATE 2/9/90	
COGMOGRAPHY D.C. BURNS		DATE 2-9-90	
ENGR. APPVL P.A. SZALINSKI		DATE 2/9/90	
QA APPVL J.L. DEMPSTER		DATE 2-9-90	
DFTG SUPR. JOHN HORTON		DATE 2/12/90	
FOR		West Valley Nuclear Services Co., Inc. West Valley, New York	
SMS		TRANSFER PIT 8Q-2	
WALL NOZZLE EMBEDMENT ASSEMBLY		SCALE 1/8	
DWG NO. 900D-2826		REV 1	
A/E DWG NO.		SHEET 1 OF 2	

CAD DRAWING-DO NOT REVISE THIS ORIGINAL

903 D 055

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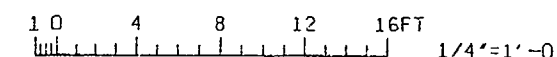
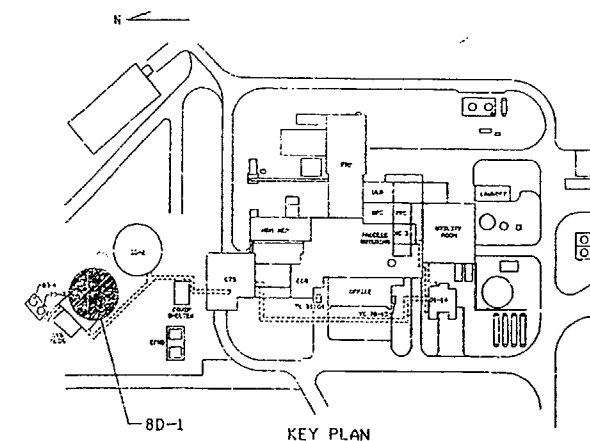
NO.	DATE	REVISION	DR	CH	APPROVED
B	03-29-85		DH	RAN	R/L NDT LBS
GENERAL REVISION					
C	06-13-85		DH	RAN	R/L NDT LBS
REVISED PER WVNS COMMENTS ON EBAR 422					
D	12-12-85		DH	RAN	R/L NDT LBS
REVISED PER WVNS COMMENTS ON EBAR 422 A					
O	2/7/86	ER 624			R/L
1	2-28-86	REMOVED PIPE CHASE OPENING	G/L		R/L
2	7/7/87	REV'D. PER EGN 1764	S/G		R/L
3	1-6-89	REV PER EGN 2733	QW		R/L

GENERAL NOTES

1. WVNS TO MODIFY ANNULUS PUMP PAD TO CLEAR NEW EQUIPMENT SUPPORT STEEL AND CONCRETE COLUMNS.
2. WVNS SLUICING PUMPS MOUNTING AND EQUIPMENT DETAILS BY WVNS.
3. SECTION OF COVER PLATE OVER VALVE AISLE HATCH AND SECTION OF METAL BUILDING ROOF OVER VALVE AISLE HATCH TO BE REMOVABLE. BOTH REMOVABLE SECTIONS TO HAVE MIN 6'-0" x 8'-0" OPEN AREA DIRECTLY ABOVE VALVE AISLE HATCH.

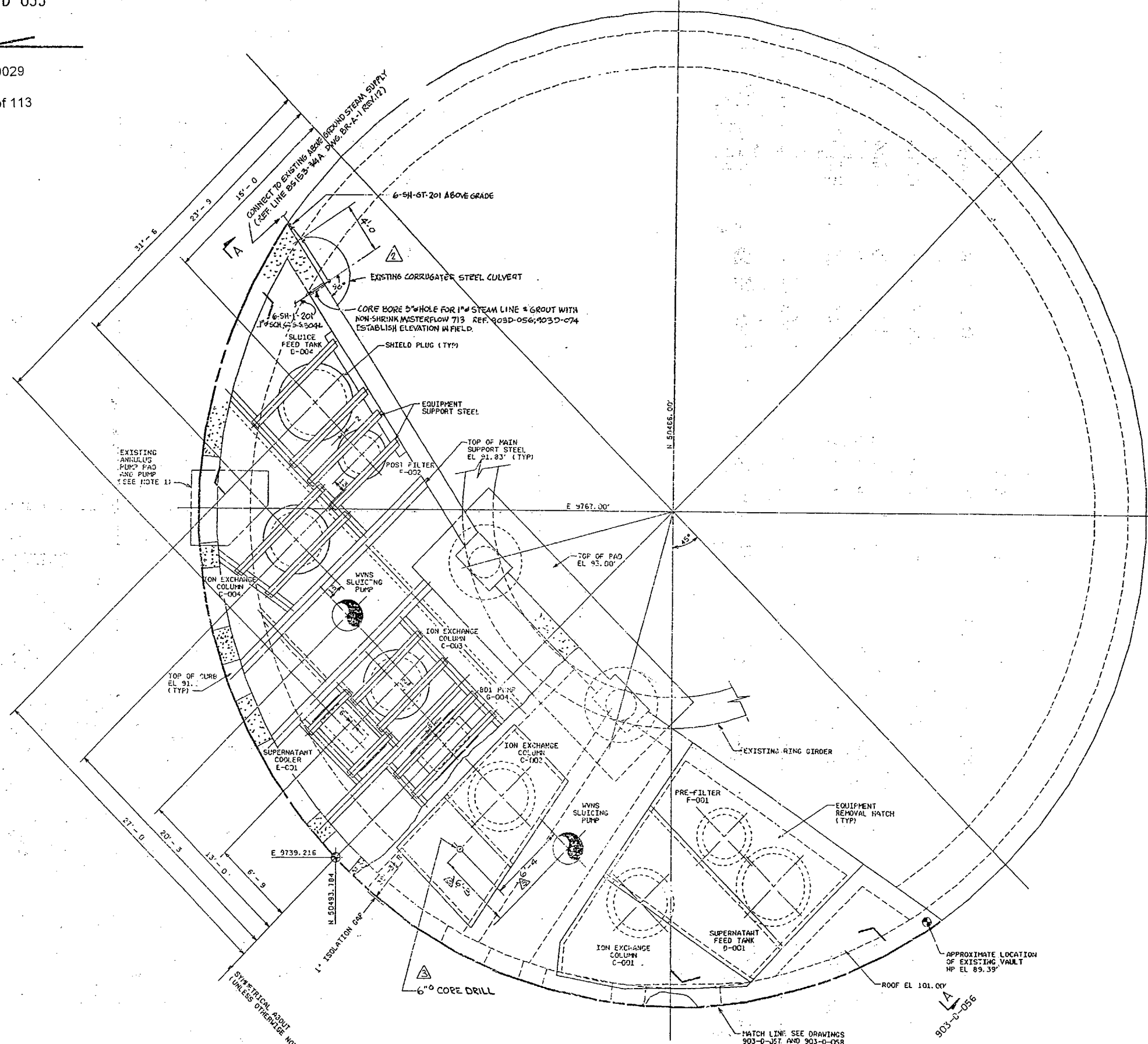
REFERENCE DRAWINGS

- GENERAL ARRANGEMENT - STS BLDG - 801 TANK
SECTION DRAWING NO. 903-D-056
- GENERAL ARRANGEMENT - STS BLDG AND 80-3 & 4 TANKS
PLAN EL 92.00' DRAWING NO. 903-D-057
- GENERAL ARRANGEMENT - STS BLDG
PLAN EL 107.00' DRAWING NO. 903-D-058
- GENERAL ARRANGEMENT - STS BLDG
PLAN AND SECTIONS DRAWING NO. 903-D-059



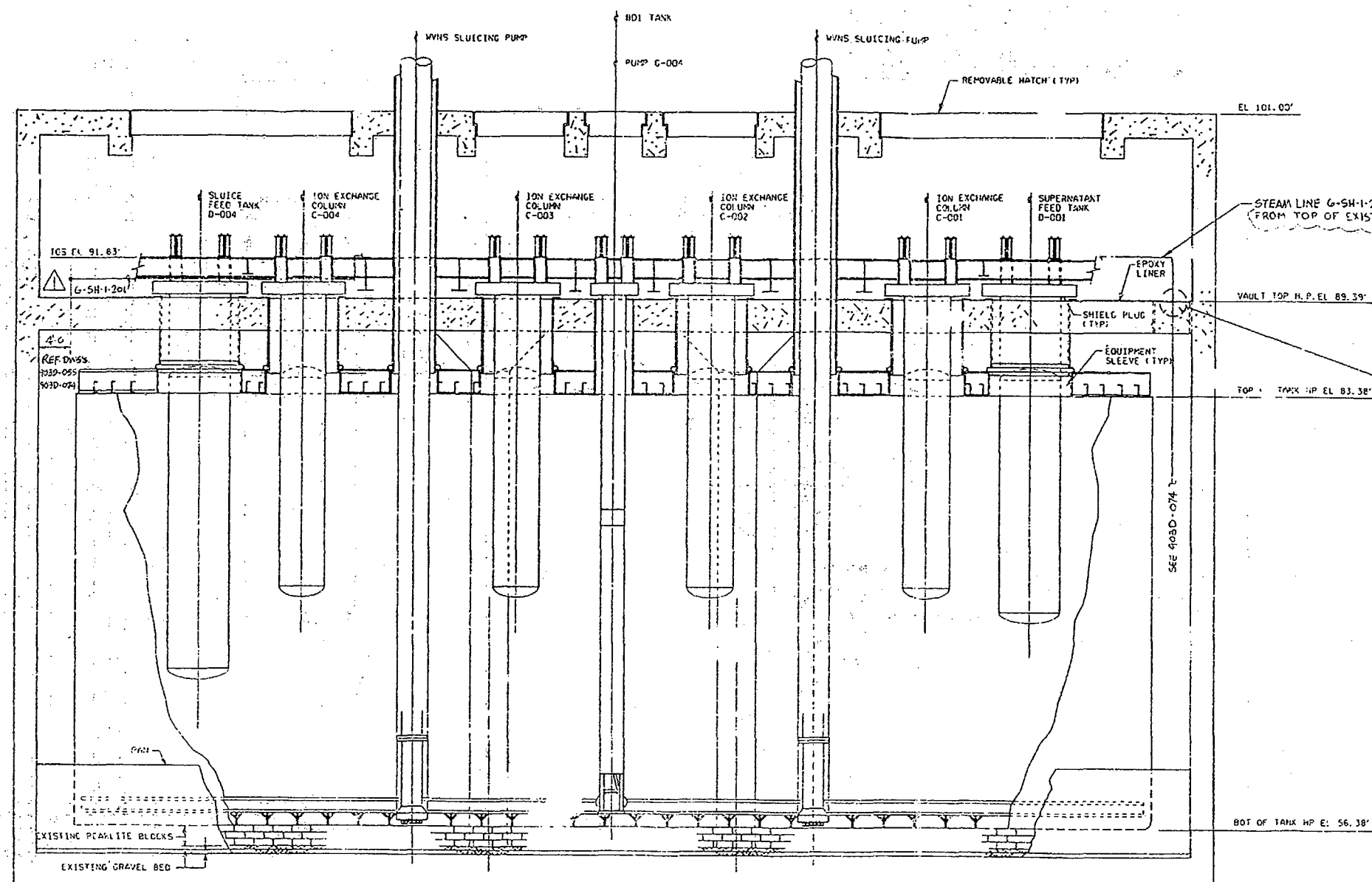
FOR DRAWING INDEX SEE DRAWING NO.

APPROVED WVNS CO. L. S. SHAW	2/13/86	EGASCO SERVICES INCORPORATED A/E G.F.S. NO. 2382	TASK ORDER 014
PROJECT MGR M. J. LEBKA	10-2-84	FOR WEST VALLEY NUCLEAR SERVICES COMPANY, INC WEST VALLEY, NEW YORK	
ENGINEER SUPV R. J. LEBKA	10-2-84	WEST VALLEY DEMONSTRATION PROJECT	
LEAD DISC ENGR S. J. LEBKA	10-2-84	GENERAL ARRANGEMENT STS 801 TANK PLAN 88.50'	
DESIGN S. J. LEBKA	10-2-84		
CHECKED S. J. LEBKA	10-2-84		
DRAWN D. HADY	10-2-84		
DE-ACOT-81NE44139 PROJECT NO.		SIZE INDEX CODE NUMBER AREA OR TYP CL ORIG	DRAWING NO. 903D-055
15-CW-02275 SUBCONTRACT NO.		SCALE 1/4"=1'-0"	REV. 3
ISSUED FOR CONSTRUCTION		SPEC. CODES A/E SHEET NO. 903-D-055	D

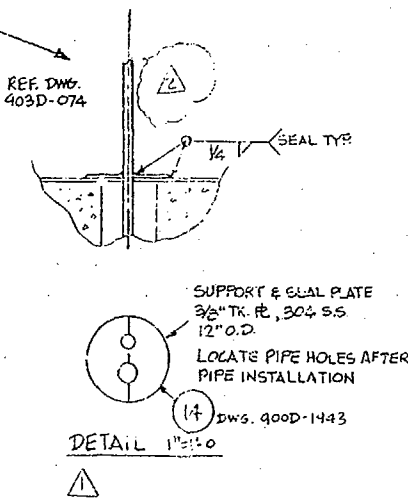


PLAN AT EL 88.50'

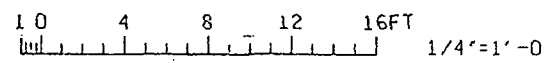
NO.	DATE	REVISION	DR	CH	APPROVED
B	03-29-65		DR	RAW	R/L LES
GENERAL REVISION					
C	6-13-65		DR	RAW	R/L MDW LES
REVISED PER WVNS COMMENTS ON EBAR 422					
D	12-12-85		R/L	RAW	R/L LES
REVISED PER WVNS COMMENTS ON EBAR 422A					
O	2/7/86	ER 624			1/24
1	7/20/87	REV'D PER ECH 1764	5/6		7/22/87
2	8/6/87	REVISED PER ECH 1831	LRP		8/11/87



NOTE
1. FOR GENERAL NOTES AND REFERENCE DRAWINGS
SEE 903-0-055.



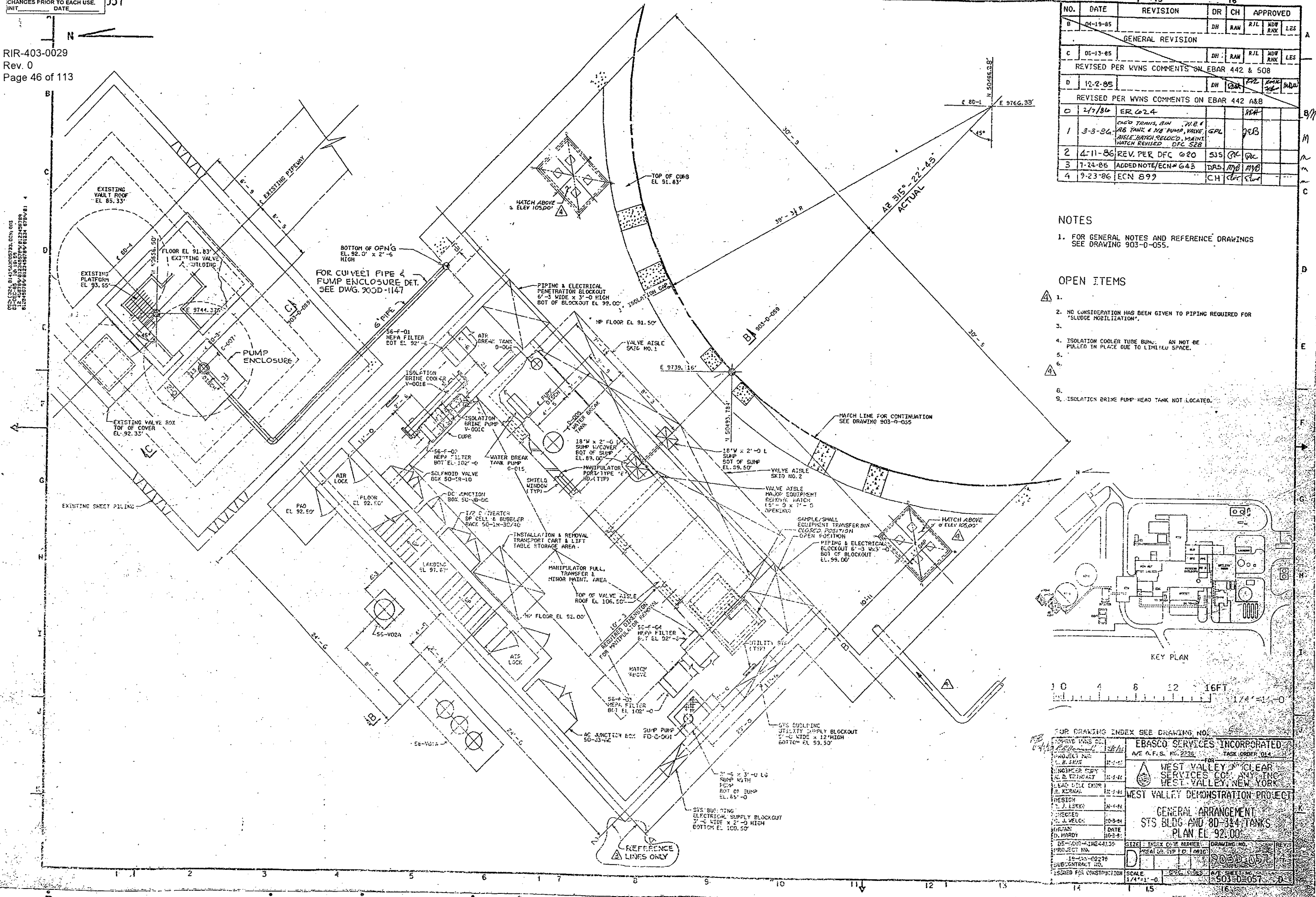
SECTION A-A
903-0-055
(13)



FOR DRAWING INDEX SEE DRAWING NO. _____

APPROVED WVNS CO. _____	EBASCO SERVICES INCORPORATED
PROJECT MGR. _____	A/E O.F.S. NO. 2338 TASK ORDER 014
E.L. SHAF. _____	FOR WEST VALLEY NUCLEAR SERVICES COMPANY, INC. WEST VALLEY, NEW YORK
ENGINEER SUPV. _____	WEST VALLEY DEMONSTRATION PROJECT
A. WEINGART. _____	GENERAL ARRANGEMENT STS 801 TANK SECTION
LEAD DTSC ENGR. _____	
P. KEENE. _____	
DESIGN R. J. LEWIS _____	
CHECKED S. J. WELCH _____	
DRAWN B. INGHAMORTE _____	
DE-AC07-81HE44139	SIZE INDEX CODE NUMBER DRAWING NO. REV.
PROJECT NO. _____	AREA DR. TYP. CL. ORIG. 903D-056 2
19-CW-02275	
SUBCONTRACT NO. _____	
ISSUED FOR CONSTRUCTION	SCALE 1/4\"/>

33-1324, 31-141 623065733, DCN, 6015
33-OEC-65 101 18109
12 436789/0123456789/0123456789
1123456789/0123456789/01234 6789/01 4



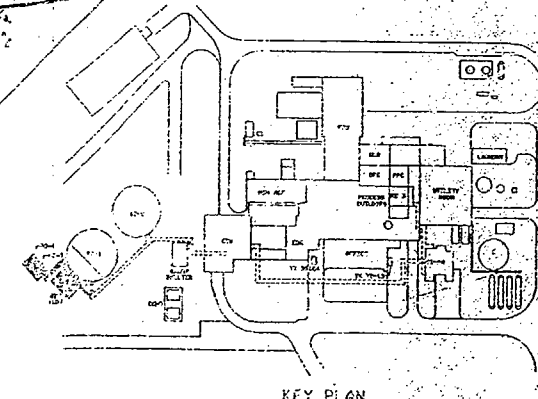
NO.	DATE	REVISION	DR	CH	APPROVED
B	04-19-85		DH	RAN	R/L NDB R/NK L25
GENERAL REVISION					
C	06-13-85		DH	RAN	R/L NDB R/NK L25
REVISED PER WVNS COMMENTS ON EBAR 442 & 508					
D	12-2-85		DH	RAN	R/L NDB R/NK L25
REVISED PER WVNS COMMENTS ON EBAR 442 A&B					
E	2/7/86	ER 624			RAN
1	3-3-86	DRG TRANS, IN NO. 4 AS PUMP, VALVE, ASSE. BATCH SELOCD, MAINT. WATCH REVISED DFC 528	GPL		RAN
2	4-11-86	REV. PER DFC 620	SJS	RAN	RAN
3	7-24-86	ADDED NOTE/ECN# 643	DRS	RAN	RAN
4	9-23-86	ECN 899	CH	RAN	RAN

NOTES

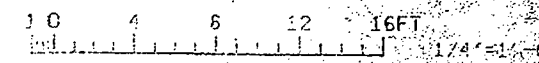
1. FOR GENERAL NOTES AND REFERENCE DRAWINGS
SEE DRAWING 903-D-055.

OPEN ITEM

4. 1.
 2. NO CONSIDERATION HAS BEEN GIVEN TO PIPING REQUIRED FOR "SLUDGE MOBILIZATION".
 - 3.
 4. ISOLATION COOLER TUBE BUNDLE: AN NOT BE PULLED IN PLACE DUE TO LIMITED SPACE.
 - 5.
 - 6.
- 4.
- 5.
 6. ISOLATION BRINE PUMP HEAD TANK NOT LOCATED.



KEY POINT

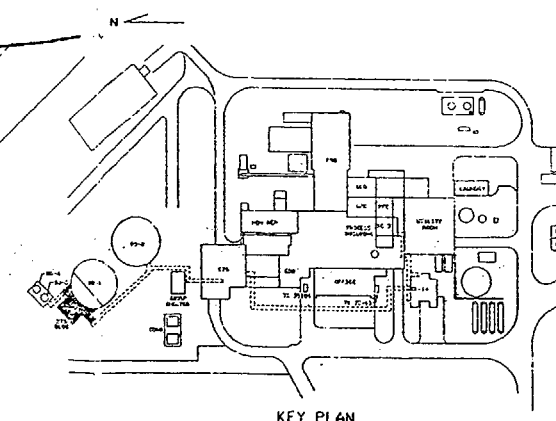
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NO.	DATE	REVISION	DR	CH	APPROVED
1	09-11-85		DH	RAW	RJL RHK LES
GENERAL REVISION 1 WVNS COMMENTS ON EBAR 508					
2	12-2-85		RJL	RHM	RJL RHK LES
GENERAL REVISION 2 WVNS COMMENTS ON EBAR 442-448					
3	2/7/86	ER 624			RHM
4	3-3-86	REMOVED ZEOLITE CONY. & HOPPER, MOD. ZEOLITE TANK, RELOC. INSPECTION HATCH'S ADD RAD. MONIT. PENETRATIONS DFC-528	GDL		REL
5	7/24/86	CHGD. COL. LINE/ECN 893	DES	MYH	1/1/88
6	9-23-86	ECN 893	CH	FLW	5/2/87
7	10/13/86	REV. PER ECN 1094	JAW		
8	1/15/88	REV. PER ECN 2150	PAS		
9	4/13/88	REV. PER ECN 2153	CCG		
10	5-3-88	" " " #2395	DES	FRY	12/1/88
11	4-20-2001	ECN 12791	CAM	HPD	

NOTE

1. FOR GENERAL NOTES AND REFERENCE DRAWINGS
SEE DRAWING 903-D-055.

FOR BEAM, HOIST AND SUPPORT DETAILS,
SEE DRAWING 903D-120, SHEET 20F2
FOR BOTH MONORAIL SYSTEMS



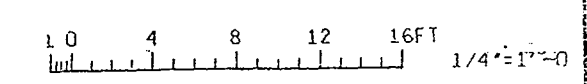
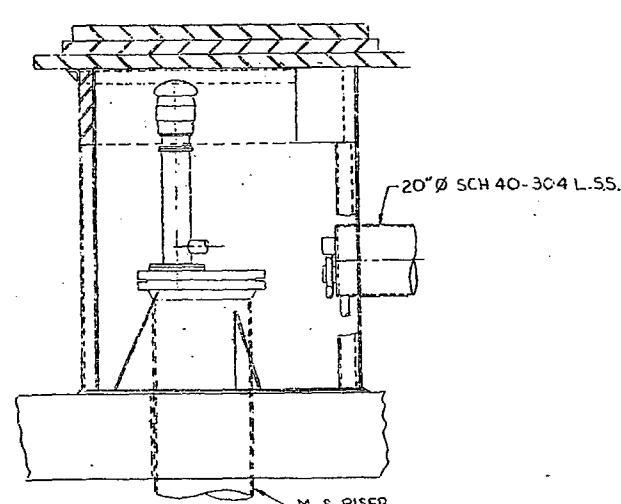
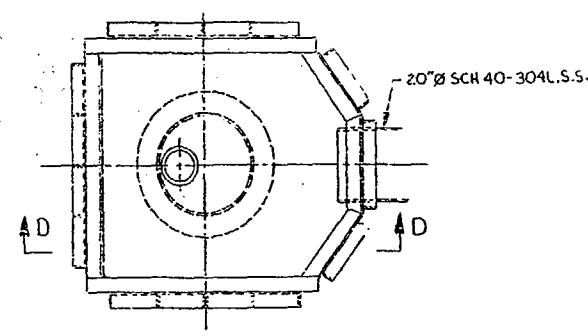
10 4 8 12 16 FT
1/4" = 1'-0"

FOR DRAWING INDEX SEE DRAWING NO.

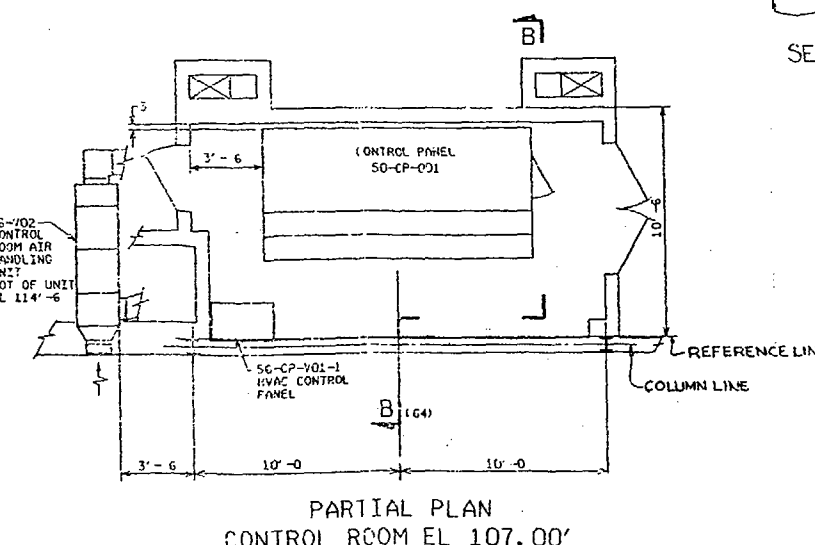
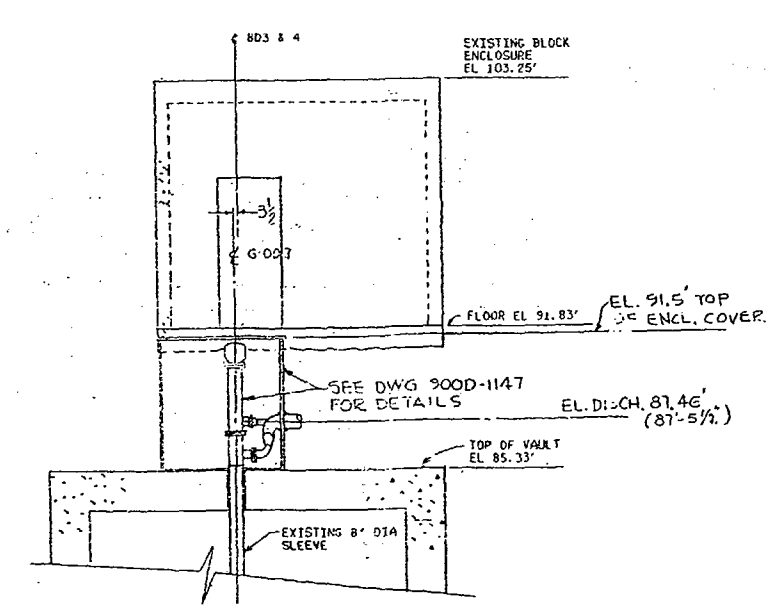
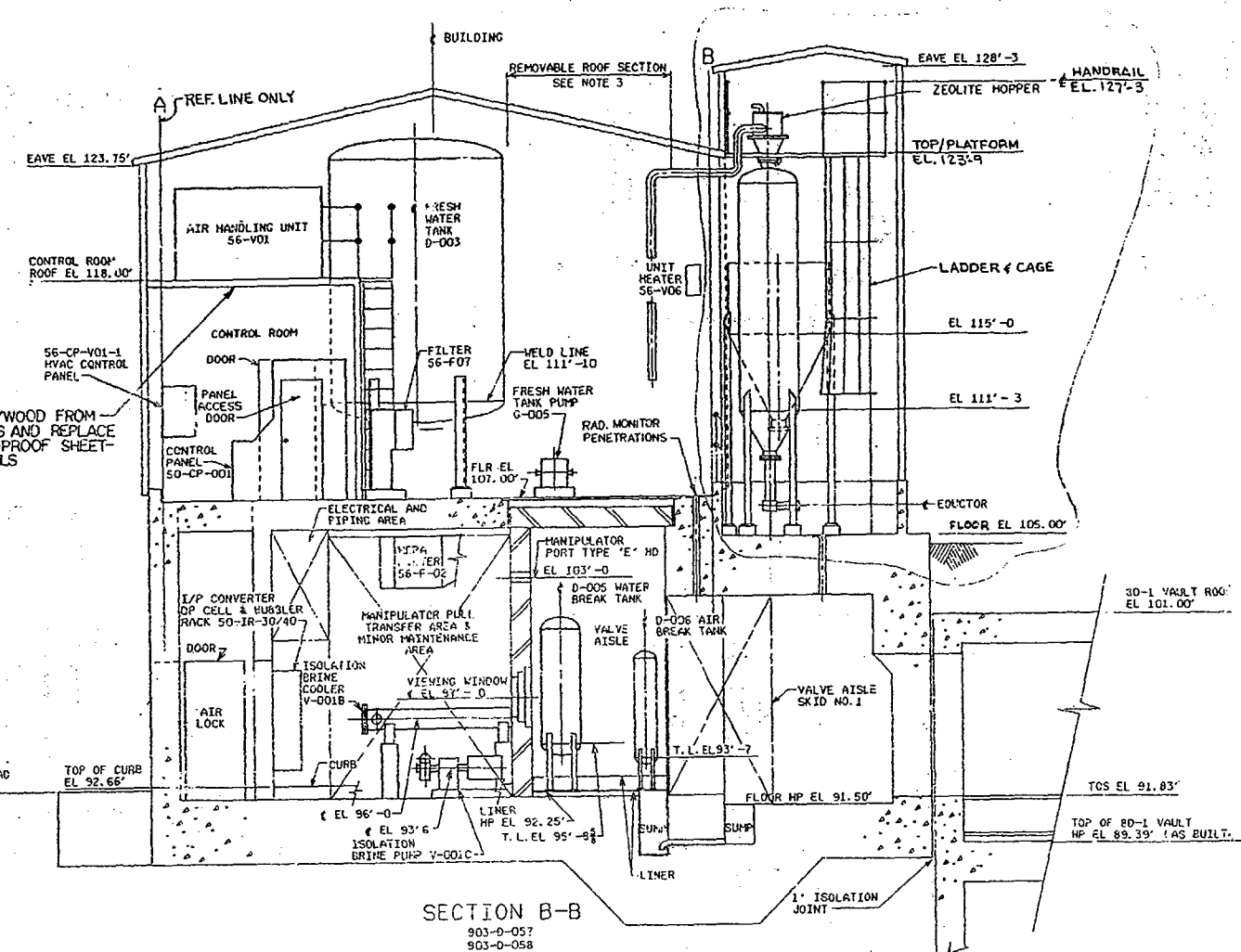
APPROVED WVNS CO.	1/5/86	EBASCO SERVICES INCORPORATED	
PROJECT MGR	1-19-85	AVE O.F.S. NO. 2382	TASK ORDER 014
ENGINEER SUPV	1-19-85	FOR	
ENGINEER	1-19-85	WEST VALLEY NUCLEAR SERVICES COMPANY, INC	
LEAD DTSC ENGR	1-19-85	WEST VALLEY, NEW YORK	
DESIGN	1-19-85	WEST VALLEY DEMONSTRATION PROJECT	
CHECKED	1-19-85	GENERAL ARRANGEMENT	
DRAWN	1-19-85	STS BUILDING	
		PLAN EL. 107.00'	
DE-1007-BINE-4139	SIZE	INDEX CODE NUMBER	REV.
PROJECT NO.	18-CW-02275	AREA DR. TYP. CL. ORIG.	
SUBCONTRACT NO.			
ISSUED FOR CONSTRUCTION	SCALE	SPEC. CODES	AVE SHEET NO.
	1/4" = 1'-0"		903D-058 7
			903-D-058

NO.	DATE	REVISION	DR	CH	APPROVED
0	8-23-85		DH	RAM	R/L R/WK LES
GENERAL REVISION & WYNS COMMENTS ON EBAR 508					
1	12-2-85		AUL	DDM	OK WS JME ADW
GENERAL REVISION & WYNS COMMENTS ON EBAR 742-A&B					
0	2/7/86	ER 624			PCH
1	3-4-86	ADDED ZEO-LITE HOPPER. REMOVED NOTE 4 IN OPEN ITEMS. MONITOR LOC. REMOVED ZEO-LITE SCR CONV. LOAD HW 15017 COLL. DFC 528		GPL	9EB
2	4-11-86	REV. PER DFC 620	SJS	QK	QK
3	7-24-86	MOVE COLL. LINE/ECN#643	D.S.	MP	MD
4	9-24-86	ECN 899	CH	SW	EB
5	5-4-88	REV/ECN#2395	DES	SW	SW
6	9-21-89	REV. PER ECN # 3164	CGR	KMR	RKS

NOTE
1. FOR GENERAL NOTES AND REFERENCE DRAWINGS SEE
DRAWING 903-D-055.



FOR DRAWING INDEX SEE DRAWING NO.	
APPROVED WYNS CO. PROJECT MGR L. E. SHAW ENGINEER SUPV S. D. EMBART LEAD DISC ENGR S. KEENAN DESIGN R. J. LEWIS CHECKED S. MILLER DRAWN D. HARDY	EBASCO SERVICES INCORPORATED A/E O.F.S. NO. 2388 TASK ORDER 014 WEST VALLEY NUCLEAR SERVICES COMPANY, INC WEST VALLEY, NEW YORK WEST VALLEY DEMONSTRATION PROJECT GENERAL ARRANGEMENT STS BUILDING PLAN AND SECTIONS
DE-ACOT-81NC44130 PROJECT NO. 19-CW-02275 SUBCONTRACT NO. ISSUED FOR CONSTRUCTION	SIZE INDEX CODE NUMBER AREA DR. TYP. CL. ORIG. DRAWING NO. 903D-059 REV. 6 SCALE 1/4"=1'-0" SEC. CODES A/E SHEET NO. 903-D-059



904-D-060 SH.1

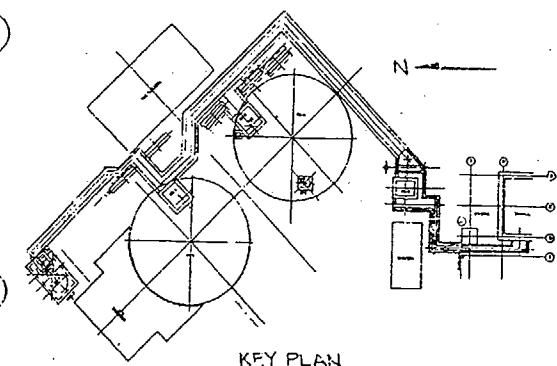
REV NO	DATE	REVISION	DR	CH	APPROVED
1	4/1/90	ER 1874	PLP	ATV	PLP
GENERAL REVISION					
0	4/8/90	ER 1874			
1	6/26/90	REV. PER ECN 3742	CGR	HAS	J.M.
2	10-12-90	REV. PER ECN 3930	GM	HAS	J.M.
3	5-1-92	REV. PER ECN 4831	PD	HAS	J.M.
4	6-1-92	REV. PER ECN 5155	GM	HAS	J.M.
5	8-10-92	REV. PER ECN 5155	PD	HAS	J.M.
6	11-2-93	REV. ECN 7016	PD	HAS	J.M.

NOTES:

1. ALL TRANSFER PIPES ELBOWS TO BE LONG RADIUS. ALL CONTAINMENT (GUARD) PIPES ELBOWS TO BE SHORT RADIUS UNLESS INDICATED BY (H) WHICH WILL BE GUARD PIPE MITERED TO FORM THE REQUIRED BEND. SEE DET. 1 OR 2 AS REQUIRED.
2. NO ALLOWANCE HAS BEEN MADE FOR WELDS & FLANGES.
3. FITTINGS & COMPONENTS NOT DIMENSIONED ARE FITTING TO FITTING.
4. CUT BACK EXISTING PIPING TO INSTALL NEW ANCHORS FOR TRANSFER LINES TO GUARD PIPE SEE DWG. 904D-560.
5. WORK POINT (WP) LOCATIONS SEE 9000-2960 CONTINUED BELOW.

REF DWG'S.

- SMS TRANSFER LINES LEAK DETECTION 9000-2615
- 1" HLW TRANSFER PIPING 904D-060 SH.2
- SMS PIP LINES TYP SECT & LET'S. 904D-132
- CONTINGENT HEADERS TO PU-2 PNL 299-01
- WASTE HEADER 28-V-045 PNL 299-01
- VIT. CELL WEST WALL COL. 2 & 3 H-3-53846
- MODULE INSTALLATION
- SMS 2" VERTICAL WALL NOZZLE WALL 5700-2212
- EMBEDMENT 28-1
- SMS TRANSFER PIT 28-2 WALL 9000-2960 SH.1
- NOZZLE EMBEDMENT ASSY
- SMS 2" MAIN LINE INTERFACE DET. 904D-132
- VIT. CELL WEST WALL COL. 2 & 3 COMPONENT MODULE H-3-53845 SH.7
- HLW TRANSFER PROCESS PIPING 904D-560
- SUPPORT LOCATIONS 9000-2960
- S.M.S TRENCH 9000-2960



FOR DRAWING INDEX SEE DRAWING NO.			
APPROV WWS CO.	EBASCO SERVICES INCORPORATED	A/E O.F.S. NO. 2389	TASK ORDER 015
PROJECT MGR	8/15/93	ENGINEER SUPV	8/15/93
LEAD DISC ENGR	8/15/93	DESIGN	8/15/93
CHECKED	8/15/93	DATE	8/15/93
DRAWN	8/15/93	DATE	8/15/93
DF-AC07-81NE41139	SIZE	INDEX CODE NUMBER	DRAWING NO.
PROJECT NO.	19-CWY-02215	CL 0316	904D-060 6
SUBCONTRACT NO.	ISSUED FOR CONSTRUCTION	SCALE	AS NOTED
		SPEC. CODES	A/E SHEET NO. 904-D-060 SH.1 B

SECTION A-A (J12)

1/2" = 1'-0"

SECTION C-C (F4)

1/2" = 1'-0"

SECTION B-B (H4)

1/2" = 1'-0"

- NOTES:
1. CONTINUED.
 2. Work Point (WP) elevations shown, except as otherwise noted, are for center line of pipe.
 3. All pipe segments between the Vitrification Facility and Pit 8Q-1 shall slope continuously from the high point elevation of the pipe to the low point elevation of the pipe at 1/8" (+1/16", -1/16") per foot. Pipe segments between Pit 8Q-1 and Pit 8Q-4 shall slope continuously at 1/4" (+1/8", -1/8") per foot. Work Point elevations, and length of pipe from WP's establish slope within each segment.
 4. Each pipe segment shall be run with the noted slope from point to point using ending embed Work Point elevations unless intermediate WP elevations are given. If an intermediate WP elevations are given, the pipe segment shall be worked from each of the given WP's while maintaining the noted slope from the high elevation to the low elevation of the two end points.

WVNS APPROVAL

COG. MGR.	
COG. ENGR.	
DRFT. SUPR.	
O.A. MGR.	
R & S MGR.	
PROJ. MGR.	

PLAN

1/4" = 1'-0"

904-D-060 SH.2

BOP W.P.E.L 91'-1/4"
(FOR 55-PH-2-002 ONLY)

MATCH LINE
SEE SH. 3 (C2)

TANK 8D-2

39'-3 1/2" RAD. (REF)

TANK 8D-2

55-PH-2-002
(PIT DR. LINE)

55-PH-6-021
55-PH-3-021
55-PH-6-003
55-PH-3-003

55-PH-4-008
55-PH-2-008
55-PH-4-004
55-PH-2-004
55-PH-4-005
55-PH-2-005
55-PH-2-002

SECTION D-D (F6, SH3 D9)
1/2" = 1'-0"

REMOVABLE COVERS

PROCESS & CONTAINMENT LINES
FOR LINE NO. SEE DWG. 900D-2818
FOR CONT. SEE DWG 900-D-2818

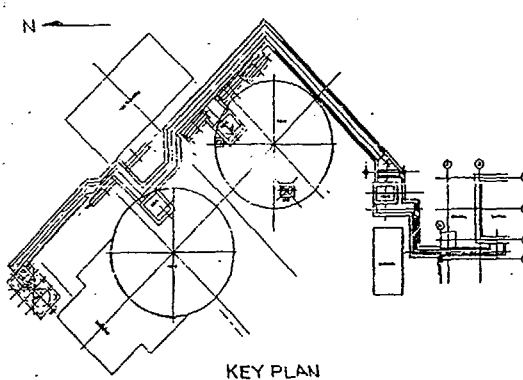
FIGURE 1

FOR CONT. SEE DWG 900-D-2818
FOR LINE NO. SEE DWG. 900D-2818
FOR NOZZLE N.S. TABLE SEE DWG. 900D-2818

FIGURE 2

NOTE
FOR GENERAL NOTES & REFERENCE DRAWINGS SEE DWG. 904-D-060 SH.1

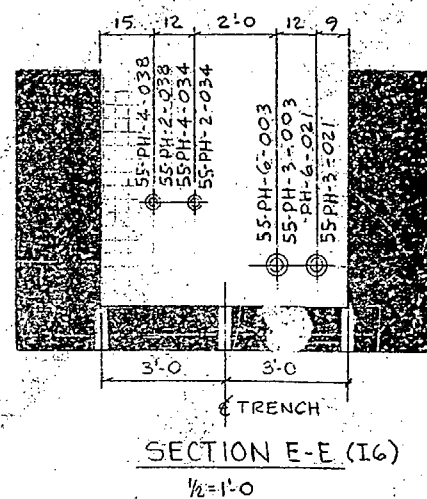
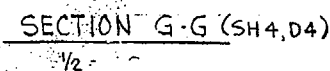
REF. DWG'S:
SMS HLW TRANSFER PIPING 904D-060 SH.1
SMS HLW TRANSFER PIPING 904D-060 SH.3
SMS TRANSFER LINES LEAK DETECTIONS 900D-2818



WVNS APPROVAL
COG. MGR. [Signature]
COG. ENGR. [Signature]
DRFT. SUPV. [Signature]
C.A. MGR. [Signature]
R & S MGR. [Signature]
PROJ. MGR. [Signature]

FOR DRAWING INDEX SEE DRAWING NO.	
APPROVED WVNS CO.	EBASCO SERVICES INCORPORATED
PROJECT MGR. [Signature]	A/E O.F.S. NO. 2388 TASK ORDER 015
ENGINEER SUPV. [Signature]	WEST VALLEY NUCLEAR SERVICES COMPANY, INC.
LEAD DISC. ENGR. [Signature]	WEST VALLEY, NEW YORK
DESIGN [Signature]	WEST VALLEY DEMONSTRATION PROJECT
CHECKED [Signature]	SLUDGE MOBILIZATION SYSTEM
DRAWN [Signature]	HLW TRANSFER PIPING
DE-AF07-B1ME44139	SIZE INDEX CODE NUMBER DRAWING NO.
PROJECT NO.	904D-060 5
19-CWV-02275	SCALE AS NOTED SPEC. CODES
SUBCONTRACT NO.	ISSUED FOR CONSTRUCTION
904-D-060 SH.2 B	

TOP OF 8Q-1
EL 97'-8



SECTION E-E (IG)
1/2=1'-0

PLAN
 $\frac{1}{4} = 1 - 0$

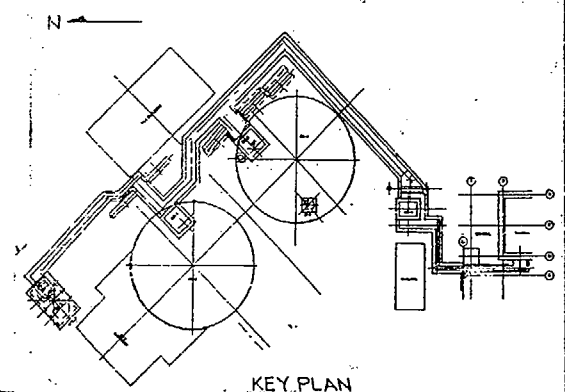
REV NO	DATE	REVISION	DR	CH	APPROVED
B	4/3/90		AS	ADY	PAK JAL JAL
GENERAL REVISION					
0	6/2/90	ER1874			PAK
1	6/29/90	REV PER ECN 3742	CGR	NAB	J.A.
2	10-12-90	REV. PER ECN 3930	GW	NAB	PAK
3	5-4-92	GEN REV PER ECN 4831	PD	WBS	PAK
4	5-28-92	REV. PER ECN 5155	CAK	DRS	PAK
5	8-10-92	REV/FCNVF-2B-0063	PD	WBS	PAK

NOTE
FOR GENERAL NOTES & REFERENCE
DRAWINGS SEE DWG 904-D-0605H.1

REF. DWGS.:

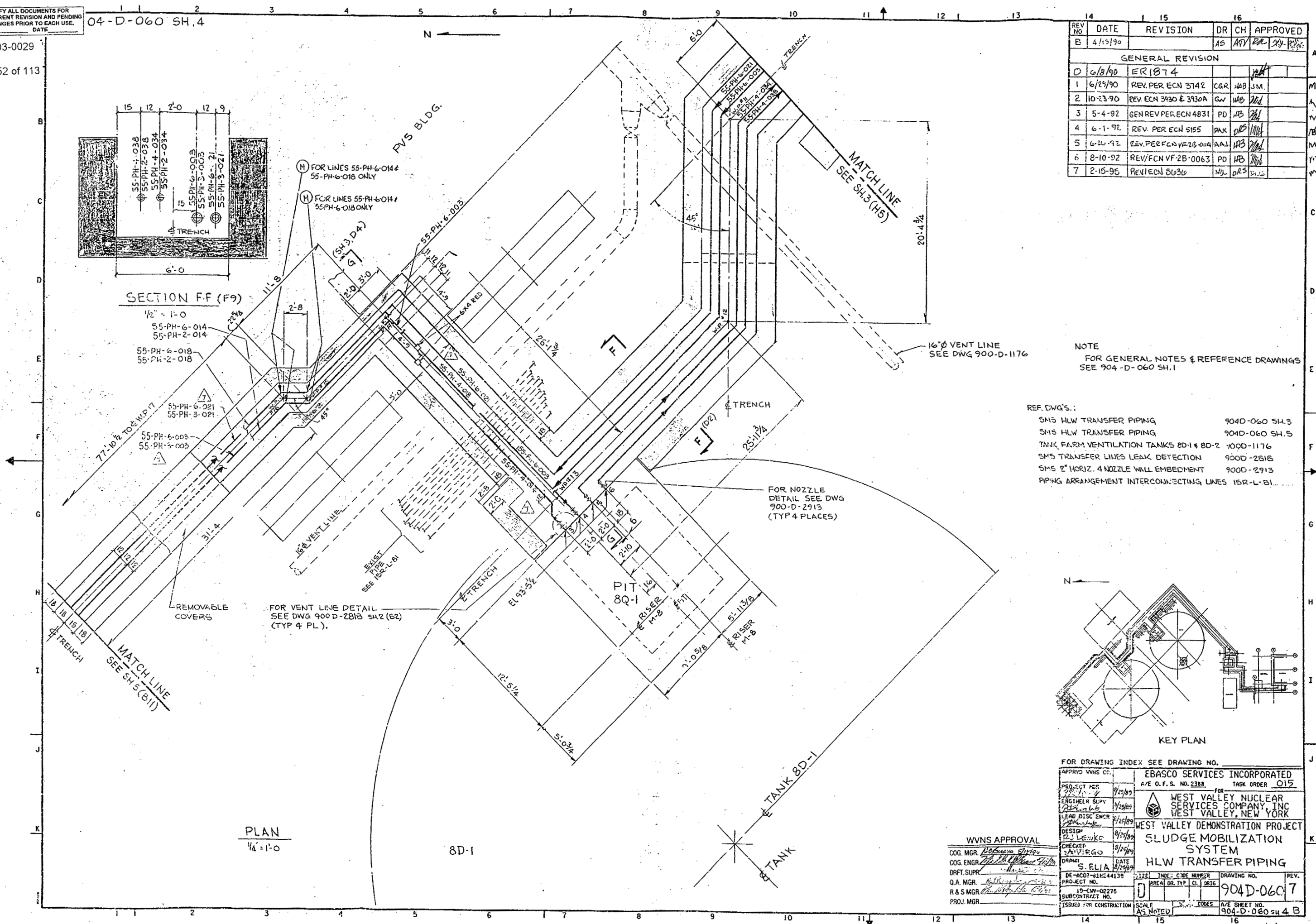
SMS HLW TRANSFER PIPING	904D-060-SH.2
SMS HLW TRANSFER PIPING	904D-060-SH.4
SMS HLW PIT LINER SUPPORT TYR SECT. DETS.	904D-133
SMS TRANSFER LINES LEAK DETECTION	900D-2818
SMS TRANSFER PIT 8Q-2 WALL NOZZLE	900D-2826

EMBLEMENT



KEY PLAN

FOR DRAWING INDEX SEE DRAWING NO.			
APPROV. WWS COL.		EBCSO SERVICES INCORPORATED	
PROJECT MGR. <i>W. J. H. H.</i>		A/E O.F.S. NO. 2388	
ENGINEER SUPV. <i>W. J. H. H.</i>		TAX ORDER <u>015</u>	
LEAD UIC. ENGR. <i>W. J. H. H.</i>		FOR	
DESIGN <i>W. J. H. H.</i>		WEST VALLEY NUCLEAR SERVICES COMPANY, INC.	
CHECKED <i>W. J. H. H.</i>		WEST VALLEY, NEW YORK	
DRAWN <i>W. J. H. H.</i>		WEST VALLEY DEMONSTRATION PROJECT	
DATE <i>1/14/69</i>		SLUDGE MOBILIZATION SYSTEM	
DATE <i>1/14/69</i>		HLW TRANSFER PIPING	
DE-AC07-2#INE44239		SIZE INDEX CODE NUMBER	
PROJECT NO.		DRAWING NO.	
19-CW-02275		AREA, E.R. TYP. CL. ORIG.	
SUBCONTRACT NO.		904D-0605	
ISSUED FOR CONSTRUCTION		SCALE	
AS NOTED		SPEC. CODES	
		A/E SHEET NO.	
		904-D-060 SH3B	

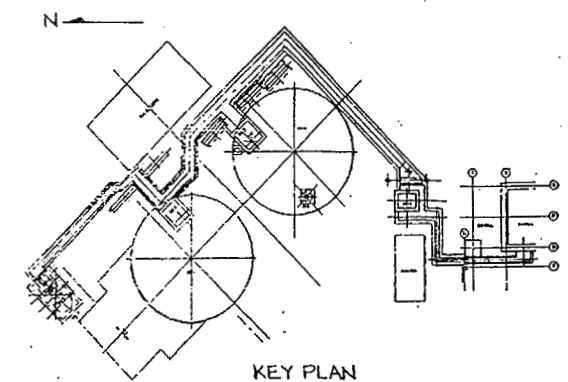


REV NO	DATE	REVISION	DR	CH	APPROVED
B	4/13/90		AS	ATV	BAK 20-10-90
GENERAL REVISION					
O	6/8/90	ER1874			YAT
1	6/29/90	REV. PER ECN 3742	CGR	HAB	JM
2	10-23-90	REV. ECN 3930 & 3930A	GW	HAB	206
3	5-4-92	GEN REV PER ECN 4831	PD	AB	241
4	6-1-92	REV. PER ECN 5155	PAK	DRS	11/14
5	6-26-92	REV. PER ECN VF2B-0114	AAJ	AB	206
6	8-10-92	REV/FCN VF2B-0063	PD	HAB	206
7	2-15-95	REV/ECN 80636	MJL	DRS	21-10

NOTE
FOR GENERAL NOTES & REFERENCE DRAWINGS
SEE 904-D-060 SH.1

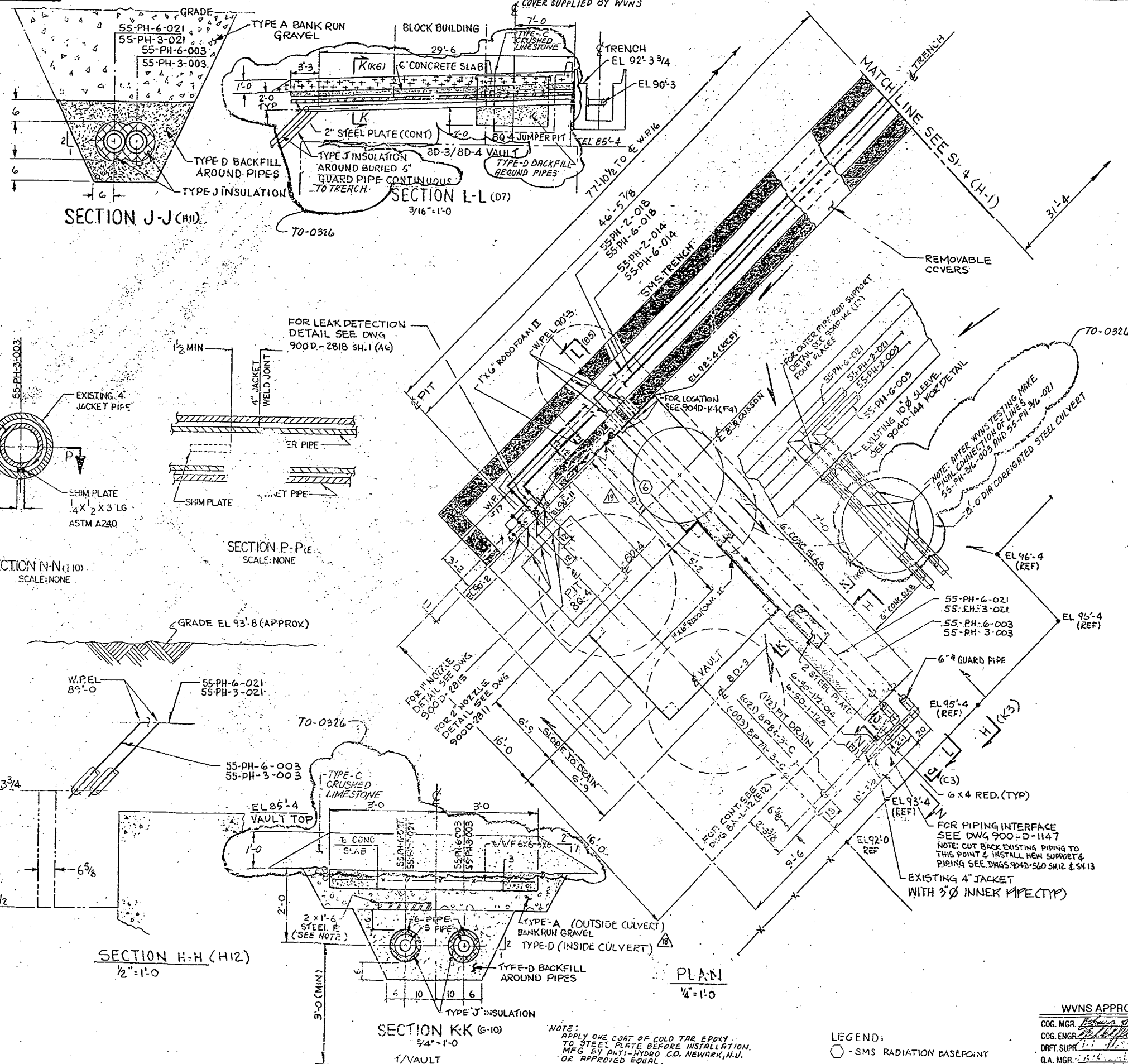
REF. DWG'S.:

SMS HLW TRANSFER PIPING	904D-060 SH.
SMS HLW TRANSFER PIPING	904D-060 SH.
TANK FARM VENTILATION TANKS 2D-1 & 2D-2	900D-1176
SMS TRANSFER LINES LEAK DETECTION	900D-2818
SMS 2" HORIZ. 4 NOZZLE WALL EMBEDMENT	900D-2913
PIPING ARRANGEMENT INTERCONNECTING LINES	15R-L-81...



FOR DRAWING INDEX SEE DRAWING NO.	
APPROV WVNS CO.	EBASCO SERVICES INCORPORATED
PROJECT NO. <u>2211-1-4</u>	A/E O.F.S. NO. <u>2388</u> TASK ORDER <u>015</u>
ENGINEER SUPV. <u>W. W. W. W.</u>	FOR <u>WEST VALLEY NUCLEAR SERVICES COMPANY, INC</u>
LEAD DISC ENGR. <u>W. W. W. W.</u>	<u>WEST VALLEY, NEW YORK</u>
DESIGN <u>R. J. W. W.</u>	WEST VALLEY DEMONSTRATION PROJECT
CHECKER <u>R. J. W. W.</u>	SLUDGE MOBILIZATION SYSTEM
DRAWN <u>S. ELIA</u>	HLW TRANSFER PIPING
DE-AC07-314244139	
PROJECT NO.	
10-CW-02275	
SUBCONTRACT NO.	
ISSUED FOR CONSTRUCTION	

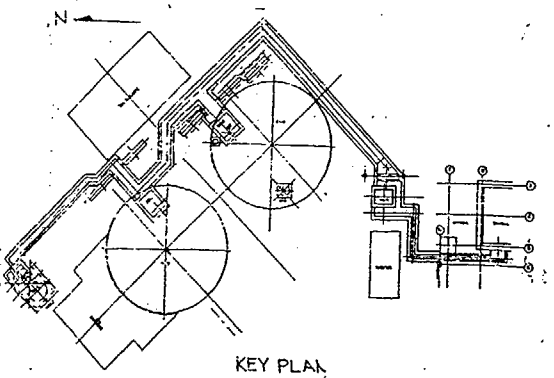
904-D-060 SH.5



REV NO	DATE	REVISION	DR	CH	APPROVED
B	4/13/90		PLP	ATY	R/L J/L P/L
GENERAL REVISION					
C	4/19/90		AV	R/L	R/L J/L P/L
GENERAL REVISION					
0	4/8/90	ER1874			
19	5/20/96	REV/ECN 9946	SRD	HAB	
2	10-15-90	REV PER ECN 3930	GW	HAB	
3	11/5/90	REV PER ECN 4022	KKA	HAB	
4	5-4-92	GEN REV PER ECN 4831	PD	HAB	
5	6-1-92	REV PER ECN 5155	PAK	DRS	
6	8-10-92	REV/ECN VF-2B-0063	PD	HAB	
7	4-27-93	GEN REV PER ECN 6059	PD	HAB	
8	6-18-93	REV/ECN VF-2B-0981	PD	HAB	
9	9-8-95	REV/ECN VF-2B-0980	EM5	HAB	P.S.
10	9-27-93	REV/ECN 6647A	PD	DRS	P.B.
11	1-12-94	REV/ECN VF-2B-1544	AAJ	HAB	P.B.
12	5-24-94	REV/ECN VF-2B-1142	DSJ	HAB	P.B.
13	6-21-94	REV/ECN VF-2B-2321	ML	HAB	P.B.
14	7-9-94	REV/ECN VF-2B-2401	PD	MA	P.B.
15	9-14-94	REV PER ECN 2402	GW	HAB	P.B.
16	11-21-94	REV/ECN VF-2B-1561	PD	CS	P.B.
17	11-1-95	REV/ECN 9509	RHS	ATY	
18	4-16-96	REV/ECN 245	SRD	HAB	

NOTES:
FOR GENERAL NOTES & REFERENCE DRAWINGS SEE 904-D-060 SH.1
DENOTES DIRECTION OF SLOPE AT FINISHED GRADE
ELEV. DENOTES TOP OF SLOPE AT FINISHED GRADE

- REF. DWGS.:**
- SMS HLW TRANSFER PIPING 904D-060 SH.4
 - SMS TRENCH PLAN & SECT'S. SH.4 904D-144
 - PIPE ROUTING & MECH. DET. FROM VALVE AISLE 900D-1147 SH.1
 - TO 8D-3
 - SMS 2" HORIZ. 2 NOZZLE WALL EMBEJMENT 900D-2811
 - SMS TRANSFER PIT 24-4 1" WALL NOZZLE EMBED. 900D-2815
 - SMS TRANSFER LINES LEAK DETECTION PIPING 900D-2818
 - PLAN & SECTIONS
 - BECHTEL COND WASTE STORAGE TANKS. 8A-L-112
 - HLW TRANSFER PROCESS PIPING SUPPORT LOCATIONS 904D-560 SH.12
 - " " " " 904D-560 SH.13



FOR DRAWING INDEX SEE DRAWING NO.					
APPROV WWS CO.	EBASCO SERVICES INCORPORATED	A/E O.F.S. NO. 12	TASK ORDER	015	
PROJECT MGR	9/25/93				
ENGINEER SUPV	9/25/93				
LEAD DISC ENGR	9/25/93				
DESIGN	9/25/93				
CHECKED	9/25/93				
DRAWN	9/25/93				
DATE	9/25/93				
DE-ACUT-81WE44139	SIZE	INDEX CODE NUMBER	DRAWING NO.	REV.	
PROJECT NO.	AREA	DR. TYP	CL	ORIG	
13-ENR-02275					
SUBCONTRACT NO.					
ISSUED FOR CONSTRUCTION	SCALE	SPEC. CODES	A/E SHEET NO.		
	AS NOTED		904D-060 SH.5 C		

1-D-125

N

45°

3' JOINT

SEE TYP. W.S. & SEALING DET. (K10)

6" WS

DIRECTION OF CONCRETE

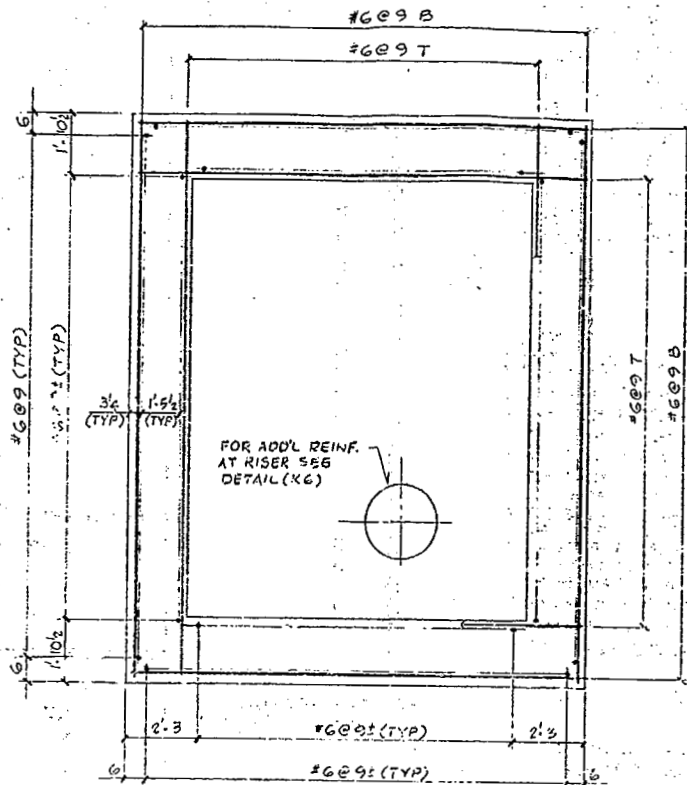
(M-8) 1/2 EXIST. 28" RISER
FOR LOCATION SEE
DWG. PHL 704-01

5'-11 5/8"

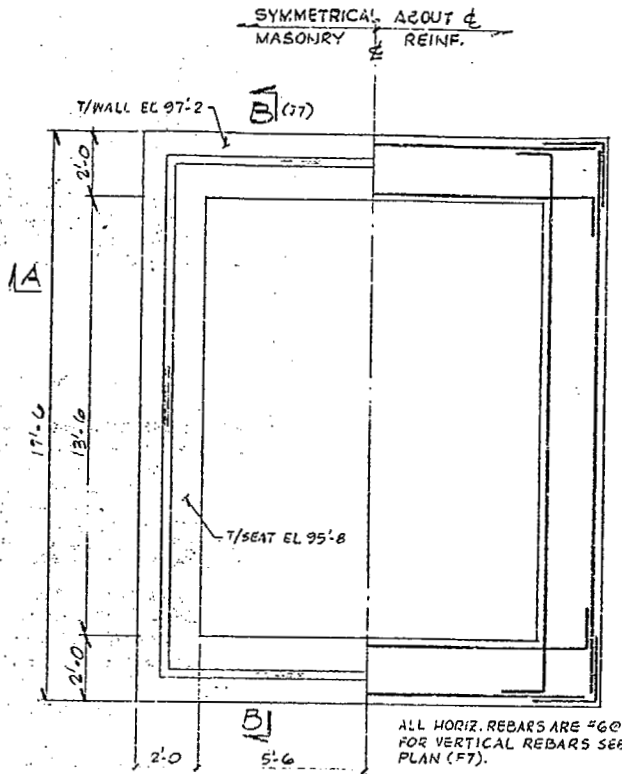
6" PVC WATERSTOP
(CONT.)

UTILITY PIT
DWG. 900-D-2861

FOUNDATION PLAN
(MASONRY)



PLAN
(FON REINF. & DOWELS)



PLAN
(WALLS - M & R)

REV NO	DATE	REVISION	DR	CH	APPROVED
B	1-26-90	GENERAL REVISION	AGS	1-26-90	REV
C	1-26-90	GENERAL REVISION AND AS PER EBAR 1325A	VS.	1-26-90	REV
O	2/11/90	ER 1775			
1	2-16-90	REV PER ECN 3475	GM	DES	
2	2-22-90	REV PER ECN 3485	CGR	DES	
3	4-26-91	REV PER ECN 4173	AAI	DES	
4	5-14-91	REV PER ECN 4247	GW	DES	
5	5-23-91	REV PER ECN 4443	GW	DES	
6	8-5-92	REV/ECN 5420	PD	DES	

NOTES:

1. FOR GENERAL NOTES SEE DWG. 905-D-710
2. SEE DWG. 904-D-146 FOR KEY PLAN
3. FOR LINER EMBED LOCATIONS SEE DWG. 904-D-129 & PNL-704-01 SH.1
4. FOR LINER SUPPORT SECTIONS & DETAILS SEE DWG. 904-D-133
5. FOR WALL PENETRATIONS SEE DWG. PNL-704-01
6. FOR COVERS SEE DRAWINGS 904-D-150 & 151
7. FOR RISER DETAILS SEE DWG. 904-D-061
8. THE SL-1 VAULT TOP ELEVATION UNDER THE SQ-1 PUMP FIT WALL VARY. THE FIT INVERT ELEV. SHALL BE MAINTAINED.
9. INVERT OF PIT SLOPES TO PIT DRAIN. SEE DWG. 904-D-061 FOR DRAIN ELEVATIONS
10. THE INSTALLATION OF MULTI-ADHESIVE ANCHORS SHALL BE INSTALLED AS PER MANUFACTURER'S SPECIFICATIONS. RELOCATE DOWELS TO CLEAR HARDWARE: RE-BARS, PIPE SLEEVES, ETC. (± 3" IN BOTH DIRECTIONS)

THIS DRAWING IS PART OF CS-194
EXCEPT AS NOTED BELOW:

CS-139 ZONE (G6) AND RELATED
DETAILS

REFERENCE DRAWINGS:

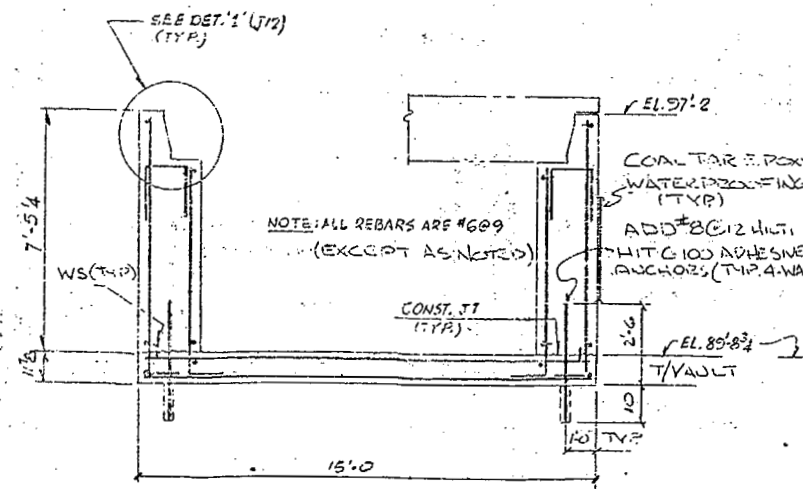
SMS-8Q-1 UTILITY PIT M&R PLAN & SECTIONS	900-D-2861
SMS-8Q-2 PUMP PIT M&R PLAN & SECTIONS	904-D-126
SMS-8Q-4 PUMP PIT M&R PLAN & SECTIONS	904-D-127
SMS-8Q-5 PUMP PIT M&R PLAN & SECTIONS	905-D-123
SMS TYP PIT COVER M&R PLAN & SECTIONS SH.1	904-D-150
SMS TYP PIT COVER M&R PLAN & SECTIONS SH.2	904-D-151
8Q-1 PUMP PIT LINER LAYOUT	PNL-704-01
SMS-8Q-1, 8Q-2, 8Q-4 RISER FLANGES DETAILS	904-D-061
SMS-8Q-1 PUMP PIT LINER PLAN & SECTIONS	904-D-129
SMS PIT LINER SUPPORT TYP. SECT. & DET.	904-D-133
V.F. GENERAL NOTES AND REFERENCE DWGS.	905-D-710
SMS KEY PLAN	904-D-140

WVNS APPROVAL

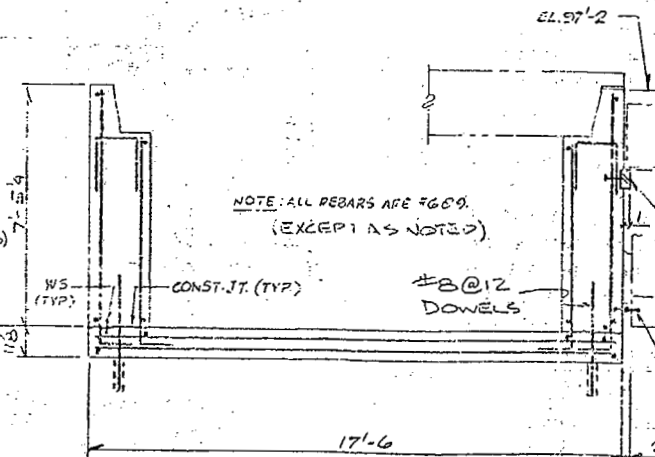
COG. MGR.	
COG. ENGR.	
DRIFT. SFT.	
QA. MGR.	
RA. S.MGR.	
PRG. MGR.	

FOR DRAWING INDEX SEE DRAWING NO.

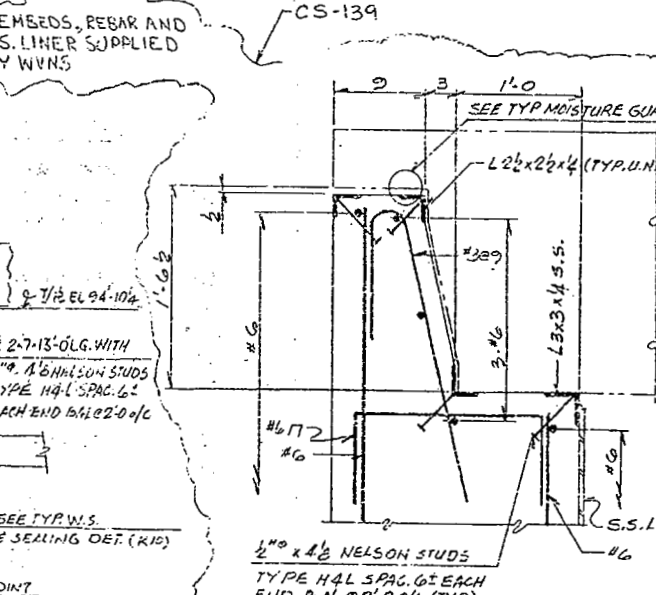
EBASCO SERVICES INCORPORATED	
A/E O.F.S. NO. 2388	TACK ORDER 015
FOR WEST VALLEY NUCLEAR SERVICES COMPANY, INC. WEST VALLEY, NEW YORK	
WEST VALLEY DEMONSTRATION PROJECT	
8Q-1 PUMP PIT M&R	
PLAN & SECTION	
PROJECT NO.	904D-125
DATE	8-11-92
SCALE	1/8" = 1'-0"
SHEET NO.	6
904D-125 C	



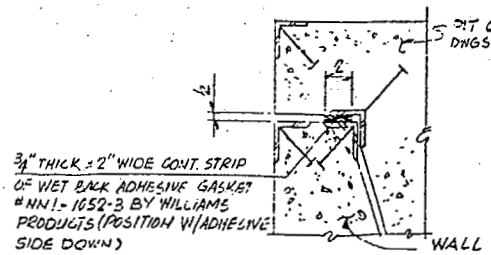
SECTION A-A (B13)



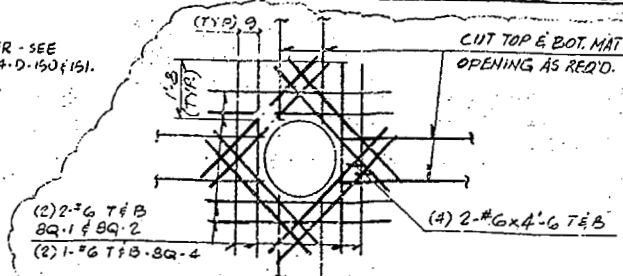
SECTION B-B (A11)



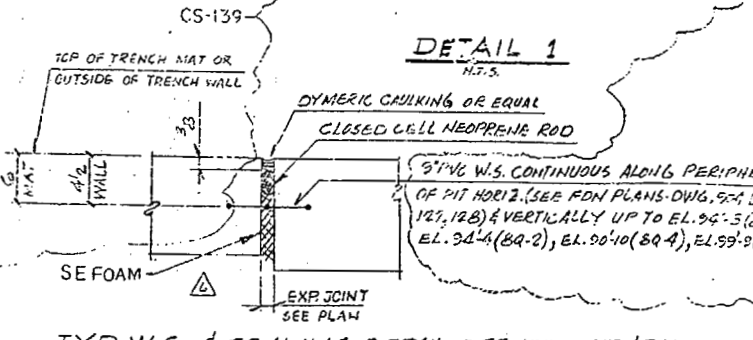
DETAIL 1



TYP. MOISTURE GUARD DETAIL



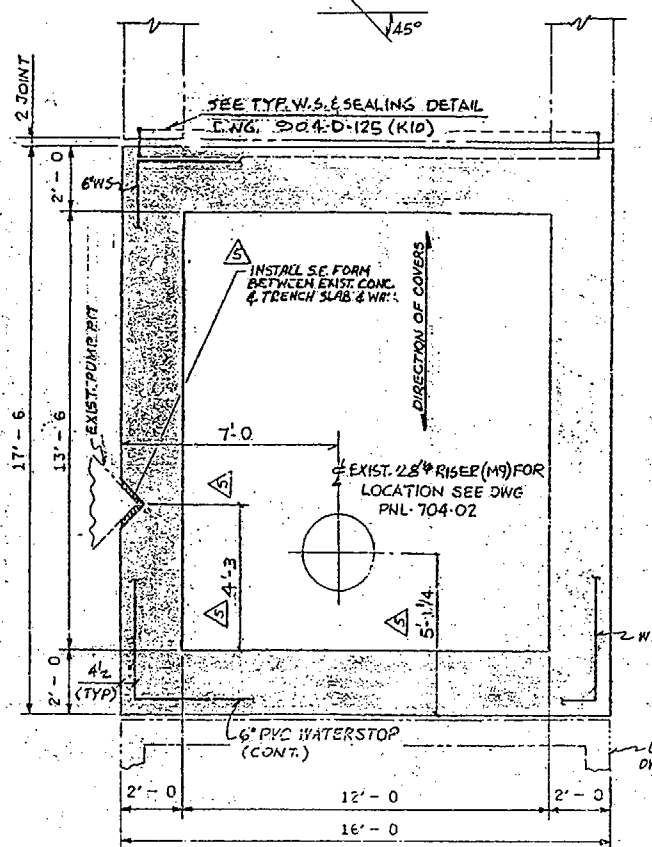
TYP. ADD'L REINF. AT ALL RISER OPENINGS



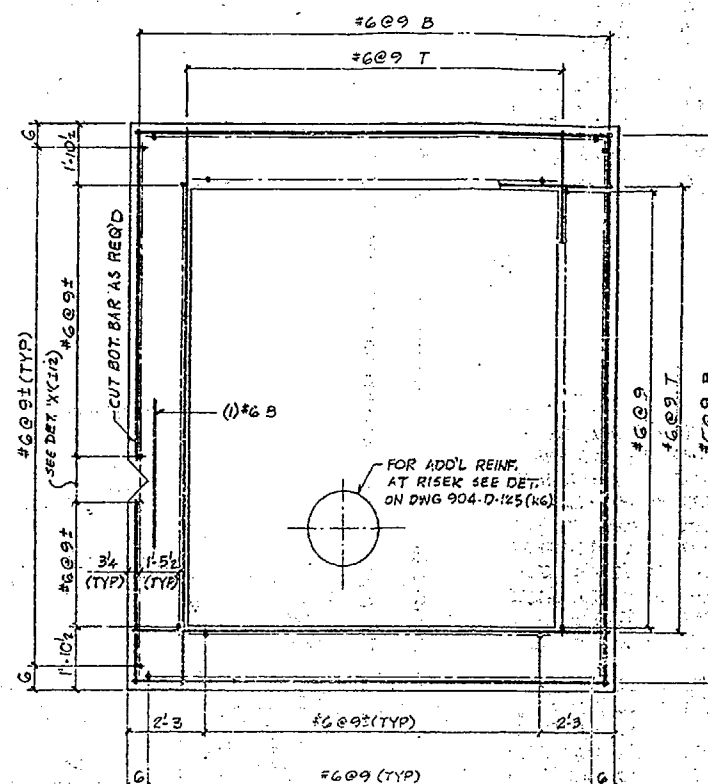
TYP. W.S. & SEALING DET. BETWEEN PIT & TRENCH

904-D-126

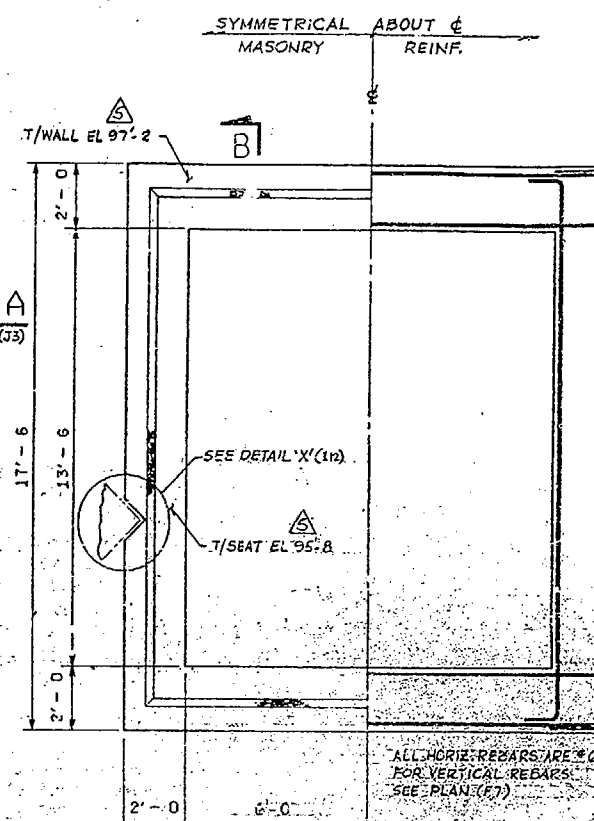
NO.	DATE	REVISION	DR	CH	APPROVED
5	10-13-97	GENERAL REVISION	AGS	26	3/11/98
C	1-26-90	GENERAL REVISION AND AS PER EBAR 1235A	Y.S.	26	3/11/98
O	2/1/90	ER 1775			1/1/91
1	2-16-90	REV. PER ECN 3475	GM	265	1/1/91
2	2-22-90	REV. PER ECN 3483	CGR	265	1/1/91
3	10/31/90	REV. PER FCN VF-2A-056	LKX	265	1/1/91
4	2/26/90	REV. PER ECN 4173	AAI	265	1/1/91
5	5-14-91	REV. PER FCN VF-2A-241	GM	265	1/1/91



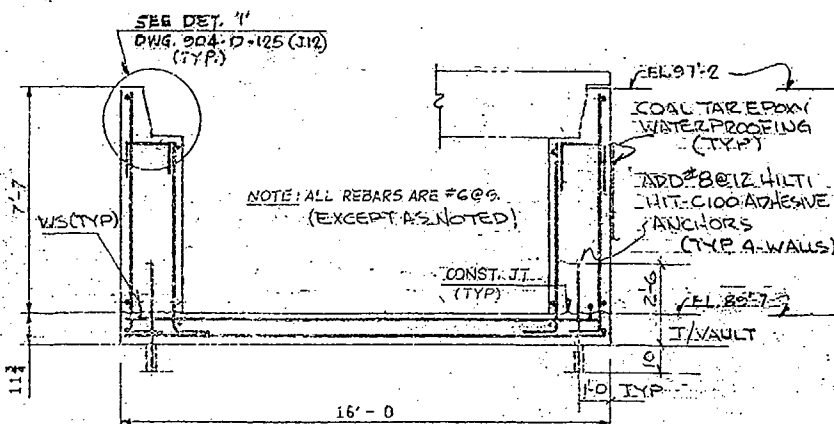
FOUNDATION PLAN
(MASONRY)



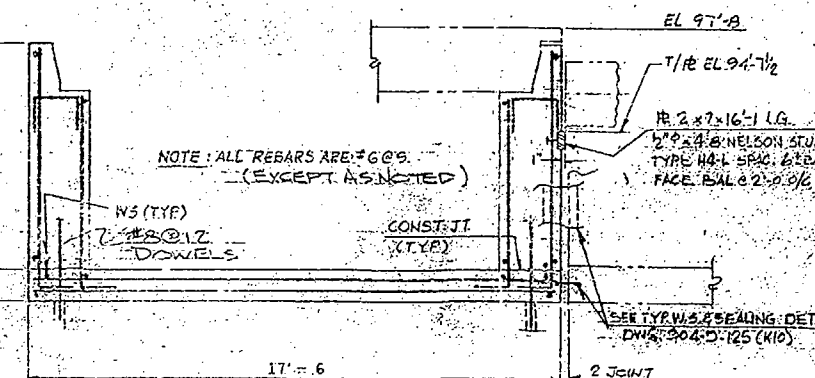
PLAN
(FON REINF. & DOWELS)



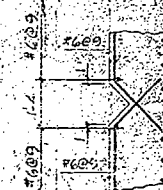
PLAN
(WALLS M&R)



SECTION A-A (C10)
NTS



SECTION B-B (F11)
NTS



DETAIL 'X'(C10)
N.T.S.

NOTES:

1. FOR GENERAL NOTES SEE DWG. 904-D-110
2. SEE DWG. 904-D-140 FOR KEY PLAN
3. FOR LINER EMBOSSED LOCATIONS SEE DWG. 904-D-130 PNL 104-D-130
4. FOR LINER SUPPORT SECTIONS & DETAILS SEE DWG. 904-D-133
5. FOR WALL PENETRATIONS SEE DWG. PNL 704-02
6. FOR COVERS SEE DRAWINGS 904-D-150 & 151
7. FOR RISER DETAILS SEE DWG. 904-D-061
8. THE ED-2 VAULT TOP ELEVATION UNDER THE 80-2 PUMP PIT WILL VARY THE PIT INVERT ELEVATION SHALL BE MAINTAINED
9. INVERT OF PIT SLOPES TO PIT DRAIN SEE DWG. 904-D-061 FOR DRAIN ELEVATIONS
10. THE INSTALLATION OF MULTIS ADHESIVE ANCHORS SHALL BE INSTALLED AS PER MANUFACTURER'S SPECIFICATIONS.
- RELOCATE DOWELS TO CLEAR HARDY: REBARS, PIPE, SLEEVES, ETC.

REFERENCE DRAWINGS:

- SMS-8Q-2 UTILITY PIT M&R: PLAN & SECTIONS 904-D-2862
- SMS-8Q-1 PUMP PIT M&R: PLAN & SECTIONS 904-D-125
- 8Q-2 PUMP PIT LINER LAYOUT PNL 704-02
- SMS-8Q-1, 8Q-2 (8Q-4) RISER PLANS & DETAILS 904-D-061
- V.F. GENERAL NOTES AND REFERENCE DWGS 905-D-110
- SMS-8Q-2 PUMP PIT LINER PLAN AND SECT. 904-D-130
- SMS PIT LINER SUPPORT TYP. SECT. (DET. 904-D-133)
- SMS TYP. PIT COVER M&R: PLAN & SECT. SH. 122 904-D-150A
- SMS KEY PLAN 904-D-140

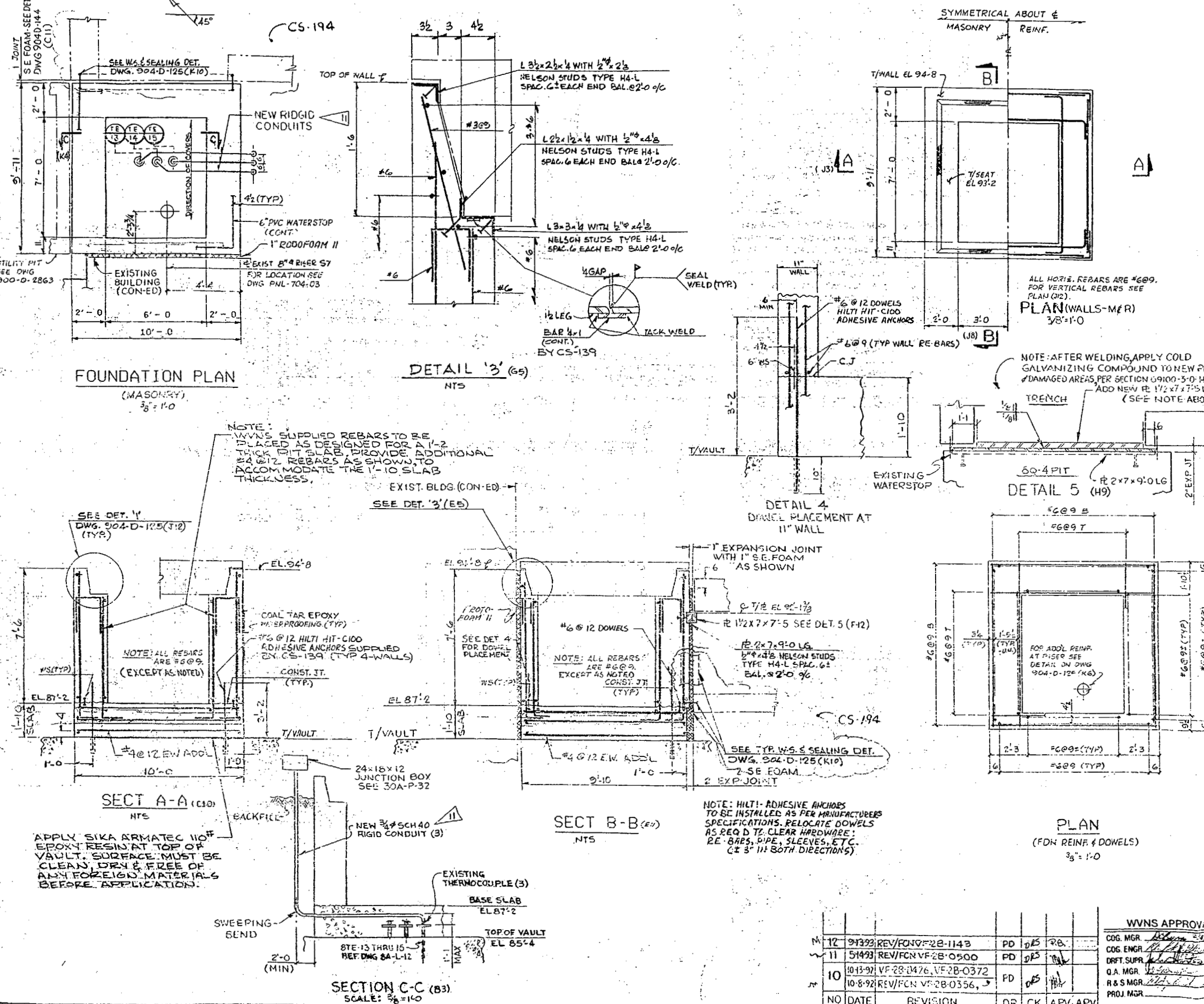
FOR DRAWING INDEX SEE DRAWING NO.

APPROV. WWS CO.	EBASCO SERVICES INCORPORATED
PROJECT MGR	A/E, D, F, S, NO. 2388
ENGINEER	WEST VALLEY NUCLEAR SERVICES COMPANY INC.
LEAD DESIGNER	WEST VALLEY, NEW YORK
DESIGN	WEST VALLEY DEMONSTRATION PROJECT
CHECKED	SLUDGE MOBILIZATION SYSTEM
ISSUED	8Q-2 PUMP PIT M&R
DATE	PLAN & SECTION
PROJECT NO.	904-D-126
DRAWING NO.	5
SCALE	3/4" = 1'-0"
ISSUED FOR CONSTRUCTION	

WWS APPROVAL

COG. MGR. [Signature]
COG. ENGR. [Signature]
DRAFT SUPR. [Signature]
O.A. MGR. [Signature]
R & S MGR. [Signature]
PROJ. MGR. [Signature]

904-D-127



NO.	DATE	REVISION	DR	CH	APPROVED
B	10-13-89	GENERAL REVISION	WJ	AGS	WJ
C	1-26-90	GENERAL REVISION AND AS PER EBAR 1325A	WJ	AGS	WJ
O	2/11/90	ER 1775	WJ	AGS	WJ
1	2-16-90	REV. PER ECN 3475	WJ	AGS	WJ
2	2-22-90	REV. PER ECN 3483	WJ	AGS	WJ
3	11-1-90	REV. PER ECN VF-2A-057	WJ	AGS	WJ
4	3-5-91	REV. PER ECN VF-2A-057	WJ	AGS	WJ
5	8-2-91	REV. PER ECN 4443	WJ	AGS	WJ
6	6-1-92	GEN. RE. PER ECN 5524	WJ	AGS	WJ
7	8-5-92	REV. ECN 5420	WJ	AGS	WJ
8	8-24-92	REV. ECN 5456	WJ	AGS	WJ
9	9-21-92	REV. ECN 5524	WJ	AGS	WJ

- NOTES:**
- FOR GENERAL NOTES SEE DRAWING 905-D-710
 - SEE DWG. 904D-140 FOR KEY PLAN
 - FOR LINER EMBED LOCATIONS SEE DWG. 904D-131 & PNL-704-01 & 13
 - FOR LINER SUPPORTS SECTIONS & DETAILS SEE DWG. 904-D-133
 - FOR WALL PENETRATIONS SEE DWG. PNL-704-03
 - FOR COVERS SEE DRAWINGS 904-D-150 & 151
 - FOR RISER DETAILS SEE DWG. 904-D-061
 - THE 80-3/4 VAULT TOP ELEVATION UNDER 8Q-1 PUMP PIT WILL VARY. THE PIT INVERT ELEV. SHALL BE MAINTAINED.
 - INVERT OF PIT SLOPES TO PIT DRAIN. SEE DWG. 904D-061 FOR DRAIN ELEVATION.
 - NEW VAULT PLUG TO BE INSTALLED IN PLACE BY WVNS PRIOR TO PLACEMENT OF PUMP PIT CONCRETE. SEE DWG. 900D-2863
 - WORK PROCEDURE FOR WVNS APPROVAL IS REQUIRED PRIOR TO REPLACING THESE CONDUIT.

THIS DRAWING IS PART OF CS-139 EXCEPT AS NOTED BELOW:

CS-194, ZONE A4, HIO WVNS SUPPLIED MATERIALS, ALL RE-BAR AND EMBEDS EXCEPT AS NOTED

- REFERENCE DRAWINGS:**
- SMS-8Q-4 UTILITY PIT M&R PLAN & SECT'S 900-D-2863
 - SMS-8Q-1 PUMP PIT M&R PLAN & SECTIONS 904-D-123
 - 8Q-4 PUMP PIT LINER LAYOUT PNL-704-03
 - VF GENERAL NOTES AND REF. DRAWINGS 905-D-710
 - SMS 8Q-1, 8Q-2, AND 8Q-4 RISER FLANGE DETS. 924-D-061
 - SMS 8Q-4 PUMP PIT LINER PLAN AND SECT. 904-D-131
 - SMS PIT LINER SUPPORT TYP. SECT. & DETAILS 904-D-133
 - SMS TYP. PIT COVER M&R PLAN & SECT. SH. 112 904-D-150/151
 - SMS KEY PLAN 904D-140

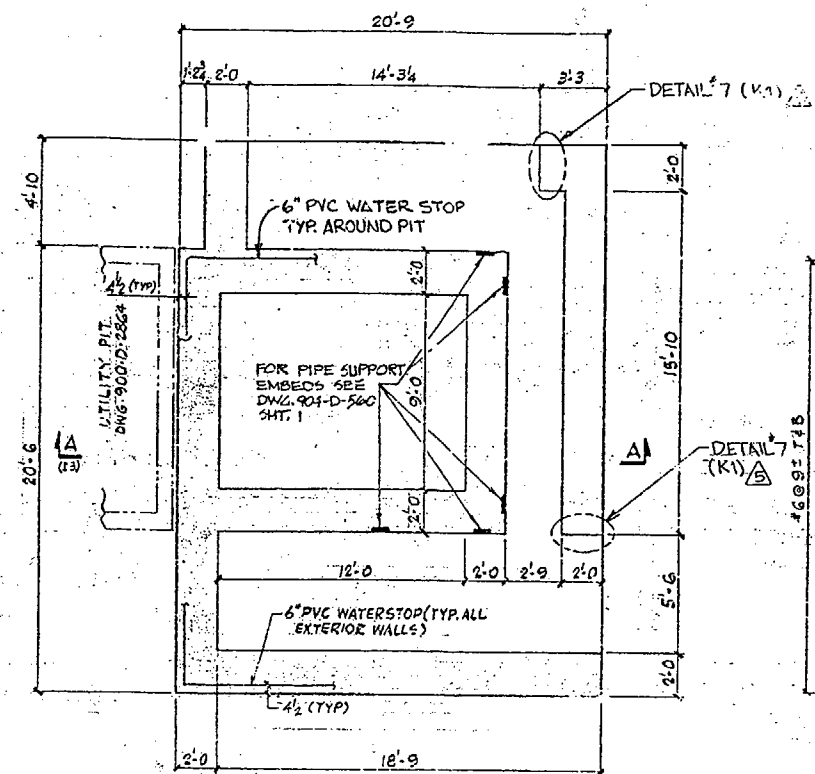
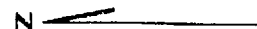
FOR DRAWING INDEX SEE DRAWING NO.

APPROV. WVNS COJ	EBASCO SERVICES INCORPORATED
PROJECT MGR	AVE D.F.S. NO. 2388 TASK ORDER 815
ENGINEER	WEST VALLEY NUCLEAR SERVICES COMPANY, INC
LEAD DESIG. ENGR	WEST VALLEY, NEW YORK
DESIGN	WEST VALLEY DEMONSTRATION PROJECT
CHECKED	SLUDGE MOBILIZATION SYSTEM
DRAWN	8Q-4 PUMP PIT M&R
DATE	PLAN & SECTION
PROJECT NO.	904D-127
ISSUED FOR CONSTRUCTION	SCALE: AS NOTED

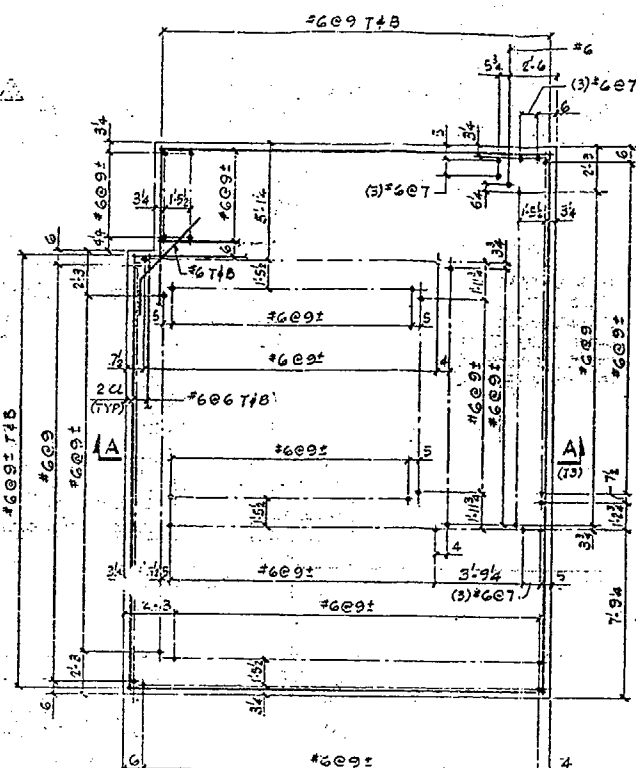
WVNS APPROVAL

COG. MGR.	REV. 11/23/92	REV. 11/23/92	PD	DES	RB
COG. ENGR.	REV. 11/23/92	REV. 11/23/92	PD	DES	RB
DRAFT. SUPR.	REV. 11/23/92	REV. 11/23/92	PD	DES	RB
Q.A. MGR.	REV. 11/23/92	REV. 11/23/92	PD	DES	RB
R & S MGR.	REV. 11/23/92	REV. 11/23/92	PD	DES	RB
PROJ. MGR.	REV. 11/23/92	REV. 11/23/92	PD	DES	RB

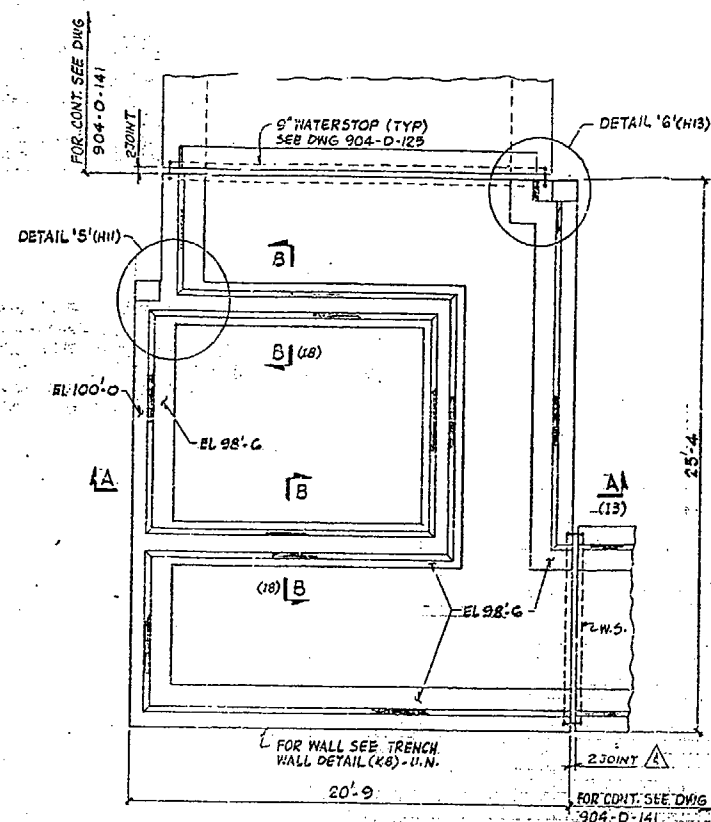
904-D-128



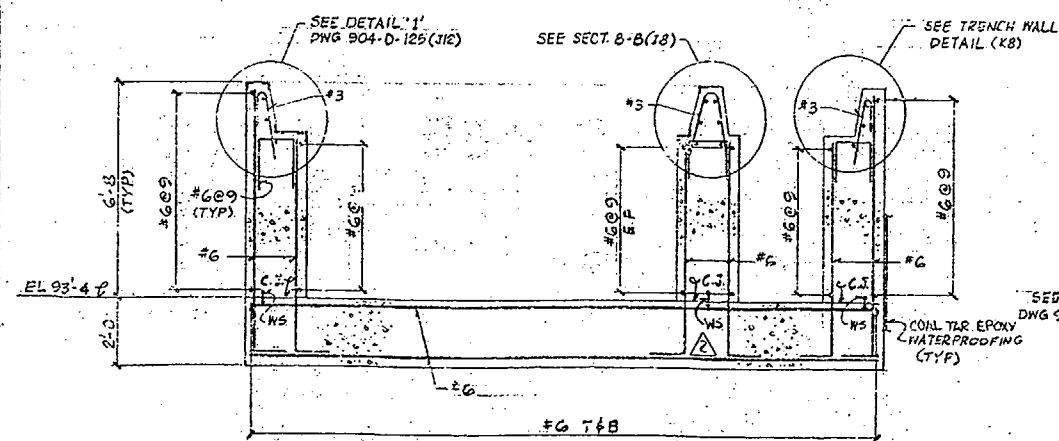
FOUNDATION PLAN
(MASONRY)
1/4" = 1'-0"



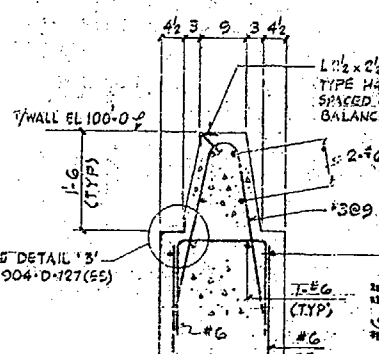
FOUNDATION PLAN
(FDN REINF. & DOWELS)
4'-1-0



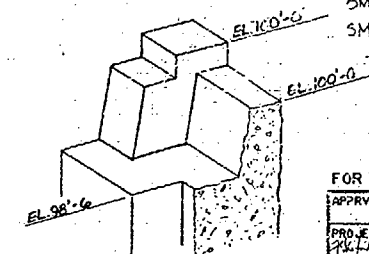
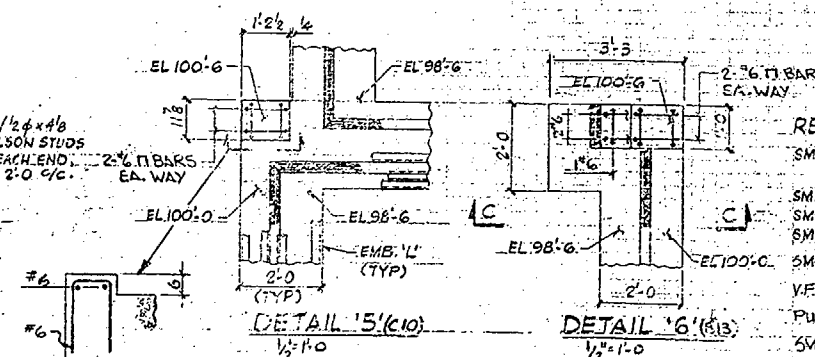
PLAN
(TOP OF WALLS)
1/4" = 1'-0"



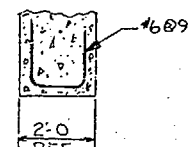
SECTION A-A (D1, D8, D13)
3/8" = 1'-0"




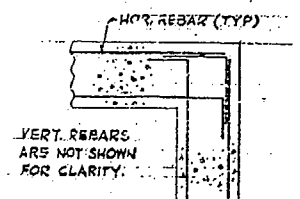
SECTION B-B (CH, DII, G4)
 $34^{\circ} = 1:0$



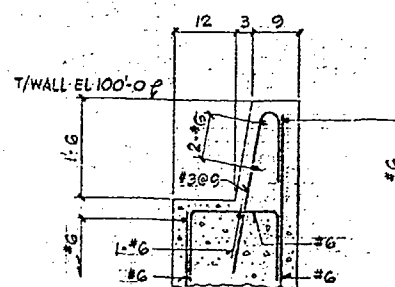
ISOMETRIC - DETAIL



DETAIL 7 (B4, E4)
SCALE: NTS 



TYP. WALL CORNER DETAIL
(REIN.)



TRENCH WALL DETAIL
3/4" = 1'-0"

REV NO	DATE	REVISION	DR	CH	APPROVED
C	1-26-90	REVISED PER EBAR NC/575A REVISED & REDRAWN	VS	L	W.C. W.C. JAL 1/1/95
O	2/12/90	ER 1775			W.C.
1	2-16-90	REV. PER ECN 3475	GM	DJS	W.C.
2	2-22-90	REV. PER ECN 3483	CGR	DJS	W.C.
3	10-11-90	REV. PER ECN 3636	CJR	HAB	W.C.
4	11-13-90	PER FCN VF-2A-064	ILH	DJS	W.C.
5	4/4/91	PER FCN VF-2A-203	ILH	HAB	W.C.

NOTES:

1. FOR GENERAL NOTES SEE DRAWING 905-D-710.
2. SEE DWG 904D-140 FOR KEY PLAN
3. FOR LINER EMBED: LOCATIONS SEE DWG. 904D-132.FRM-704-01 314
4. FOR LINER SUPPORT SECTION & DETAILS SEE DWG 904-D-133.
5. FOR WALL PENETRATIONS SEE DRAWING PLAN - 704-04.
6. FOR COVERS SEE DRAWINGS 904-D-150 & 151.

REFERENCE DRAWINGS:

- | | |
|---|-----------------|
| SMS - 8" - 1" PUMP PIT PLANS & SECTIONS - M&R | 904-D-125 |
| SMS - TRENCH PLAN & DETAILS - SH I | 904-D-141 |
| SMS - 8" - 4" PUMP PIT PLANS & SECTIONS - M&R | 904-D-127 |
| SMS - 8" - 5" UTILITY PIT PLAN & SECTIONS - M&R | 904-D-2864 |
| SMS - H.W. TRANSFER PIPING SUPPORT LOCATIONS | 904-D-5600 |
| V.F. GENERAL NOTES AND REFERENCE DWGS. | 905-D-710 |
| PUMP PIT LINER LAYOUT 8" - 5" | PNL - 704-04 |
| SMS 8" - 5" PUMP PIT LINER PLAN & SECTION | 904-D-152 |
| SMS PIT LINER SUPPORT TYPE SECT. & DET. | 904-D-153 |
| SMS PIT COVER M&R PLAN & SECT. SH I & 2 | 904-D-150 & 151 |
| SMS. KEY PLAN | 904D-140 |

FOR DRAWING INDEX SEE DRAWING NO.

APPROV WMS CO.		EBASCO SERVICES INCORPORATED					
		A/E C.F.S. NO. 2385			TASK ORDER 015		
PROJECT MGR J.H. H. 9/6/79		FOR WEST VALLEY NUCLEAR SERVICES COMPANY, INC. WEST VALLEY, NEW YORK					
ENGINEER SURV W.C.H.		WEST VALLEY DEMONSTRATION PROJECT					
LEAD DESIG ENGR W.C.H.		SLUDGE MOBILIZATION SYSTEM					
DESIGN W.C.H.		BQ-5 DIVERSION PIT & R					
CHECKED S.G.B.		PLANS & SECTIONS					
DATE 1-18-90		DRAWING NO.		REV.			
DE ACOT-BISE44:39		904D-I28		5			
PROJECT NO.		904-D-128		C			
19-CIV-02275							
SUBCONTRACT NO.							
ISSUED FOR CONSTRUCTION		SCALE		SPEC CODES			
		NONE					

904-D-140

CUT TRENCH COVER
BAR COVER BARS AT
OPENING AS REQ.

TYPICAL ADDITIONAL REINF.
AT TRENCH COVER OPENINGS
DETAIL 'H'

NTS

EXISTING PUMP SUPPORT
FOUNDATIONS (TYP)

PNEUMATIC TRANSFER SYSTEM
PRECAST CONCRETE FOUNDATION-EXTRA
CONCRETE PLACED AT BASE DURING
CONSTRUCTION REMAINS IN PLACE.

DETAIL 'F'

SECTION A-A (110)

3/4" = 1'-0"

SECTION B-B (110)

DETAIL 'B' (113)

3/4" = 1'-0"

DETAIL 'C'

3/4" = 1'-0"

DETAIL 'D'

3/4" = 1'-0"

DETAIL 'E'

3/4" = 1'-0"

NEOPRENE PAD & CAULKING DETAIL

RAIN GUARD DETAIL

TYP TRENCH COVER DETAILS

NO	DATE	REVISION	BY	CH	APPROV
B	10-13-84	GENERAL REVISION	V.S.	SC	W.V.
C	2-2-90	REVISED PER EBAR NO. 1338A	V.S.	SC	W.V.
D	2/12/90	ER 1775			
1	2-16-90	GEN REV PER ECN 3474	GW	DES	W.V.
2	4-9-90	REV PER ECN 3563	JAW	DES	W.V.
3	10-15-90	REV PER ECN 3636 (FCH VF-2A-004)	CGR	HAB	W.V.
4	10-31-90	REV PER ECN VF-2A-010	LH	HAB	W.V.
5	11-8-90	REV PER ECN VF-2A-032	DAK	DES	W.V.
6	2-4-91	REV PER ECN VF-2A-111	DAK	HAB	W.V.
7	2-19-91	REV PER ECN VF-2A-283 & VF-2A-288	GM	HAB	W.V.
8	12-26-91	ECN 4766	PD	HAB	W.V.
9	1-3-92	GEN REV PER ECN 5197	HAB	DES	W.V.
10	1-2-93	REV PER ECN 6279	GW	HAB	W.V.
11	9-16-94	REV PER ECN VF-2B-3588	W.V.	DES	W.V.

* NOTE: 2" CAPED 60140 PVC PIPE
INSTALLED UNDER MUDMAT FOR
FUTURE ACCESS UNDER TRENCH

GENERAL NOTES:

- FOR GENERAL NOTES EXCEPT AS SHOWN BELOW
SEE DRAWING 905-D-710
 - FOR W.P. GEOMETRY SEE DRAWING 900D-2960
 - WORK THIS DRAWING WITH DRAWINGS 904-D-141
THRU 904-D-146 AND DWG 900D-2960
 - ALL CARBON STEEL EMBEDS TO BE GALVANIZED
AFTER WELDING PRIOR TO INSTALLATION.
 - UNLESS OTHERWISE NOTED: PRECAST CONCRETE COVERS
SHALL HAVE ONLY 2 BEARING SURFACES WHICH SHALL BE
EITHER THE TRENCH WALLS OR A SUPPORT BEAM, AND
THE BEARING SURFACES SHALL BE OPPOSITE EACH
OTHER. REDUCE THE THICKNESS OF THE COVER BY
1/4 INCH AT THE NON-BEARING CONTACT AREA.
- ALL BEARING SURFACES SHALL HAVE A 1/2" NEOPRENE
(40 DUROMETER) BEARING PAD, CONTINUOUS FOR THE
ENTIRE BEARING SURFACE. THE PAD THICKNESS
HAS NOT BEEN INCORPORATED INTO THE COVER
ELEVATIONS.

GENERAL NOTES CONTINUED BELOW.

REFERENCE DRAWING	
VITRIFICATION FACILITY GENERAL NOTES AND REFERENCE DRAWINGS	905D-710
VIT. FAC. ARCHITECTURAL ELEVATION	905D-731 SH.1
VIT. FAC. ARCHITECTURAL GROUND FLOOR EL. 100 FT O	905D-733
SMS TRENCH PLAN & DET M&R SH. 1-4	904D-141 THRU 904D-144
SMS TRENCH COVER SCHEDULE SH. 1&2	904D-145 THRU 904D-146
SMS TRENCH	900D-2960
STS 50N SAMPLE PNEUMATIC TRANSFER SYSTEM	900D-1211

WVNS APPROVAL

COG. MGR. W.V.
COG. ENGR. W.V.
DRFT. SUPR. W.V.
O.A. MGR. W.V.
R & S MGR. W.V.
PROJ. MGR. W.V.

GENERAL NOTES (CONTINUED FROM ABOVE)
SEALING BETWEEN TRENCH COVERS TO BE 1/2 INCH
A TOLERANCE OF MINUS 1/16" TO PLUS 1/8" IS
ALLOWABLE TO PERMIT FIT UP ONLY. WVNS
ENGINEERS TO BE NOTIFIED OF ANY DISCREPANCIES

FOR DRAWING INDEX SEE DRAWING NO.

APPROV WVNS CO.	EBASCO SERVICES INCORPORATED
PROJECT MGR. <u>W.V.</u>	A/E O.F.S. NO. 2338 TASK ORDER 015
ENGINEER SUPV. <u>W.V.</u>	FOR WEST VALLEY NUCLEAR SERVICES COMPANY, INC WEST VALLEY, NEW YORK
LEAD DES. ENGR. <u>W.V.</u>	WEST VALLEY DEMONSTRATION PROJECT
DESIGN <u>W.V.</u>	SLUDGE MOBILIZATION SYSTEM KEY PLAN
CHECKED <u>W.V.</u>	
DRAWN <u>W.V.</u>	
DE-ACOT-81NE44133	SIZE INDEX CODE NUMBER
PROJECT NO.	AREA OR TYP. CL. OR TC
18-CW-02275	DRAWING NO. 904D-140
SUBCONTRACT NO.	REV. 11
ISSUED FOR CONSTRUCTION	SCALE 1/16" = 1'-0"
	SPEC. CODES
	A/E SHEET NO. 904-D-140

904-D-141

* NOTE: 6" CAPED SCH 40 PVC PIPE INSTALLED UNDER
MUD MAT FOR FUTURE ACCESS UNDER TRENCH

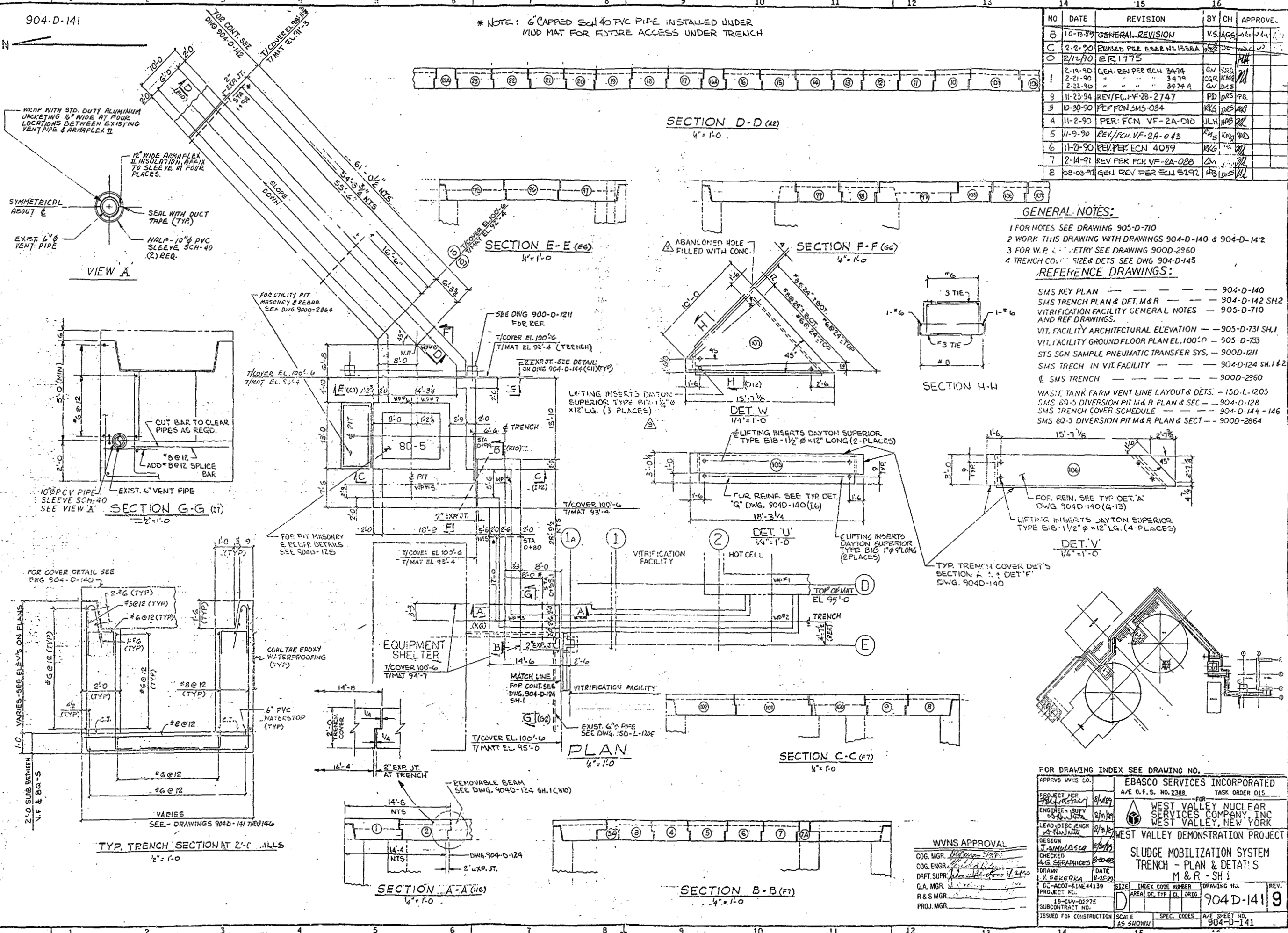
NO	DATE	REVISION	BY	CH	APPROVE
B	10-13-89	GENERAL REVISION	VS	AGS	AS
C	2-2-90	REVISED PER EBAR N1338A	VS	AGS	AS
O	2/12/90	ER 1775	VS	AGS	AS
1	2-19-90	GEN. REV PER ECU 3474	VS	AGS	AS
2	2-21-90	" " " " 3479	VS	AGS	AS
3	2-22-90	" " " " 3474 A	VS	AGS	AS
9	11-23-94	REV/FCN VF-28-2747	PD	DES	PS
3	10-30-90	PER FCN SMS-084	RK	DES	AB
4	11-2-90	PER FCN VF-2A-D10	JLH	HAB	PS
5	11-9-90	REV/FCN VF-2A-043	RH	S	MS
6	11-2-90	REV PER ECU 4059	RK	S	MS
7	2-14-91	REV PER FCN VF-2A-088	DM	S	MS
8	08-03-91	GEN REV PER ECU 5192	AB	S	MS

GENERAL NOTES:

- 1 FOR NOTES SEE DRAWING 905-D-710
- 2 WORK THIS DRAWING WITH DRAWINGS 904-D-140 & 904-D-142
- 3 FOR W.P. ENTRY SEE DRAWING 900D-2960
- 4 TRENCH COVER SIZE & DETS SEE DWG 904-D-145

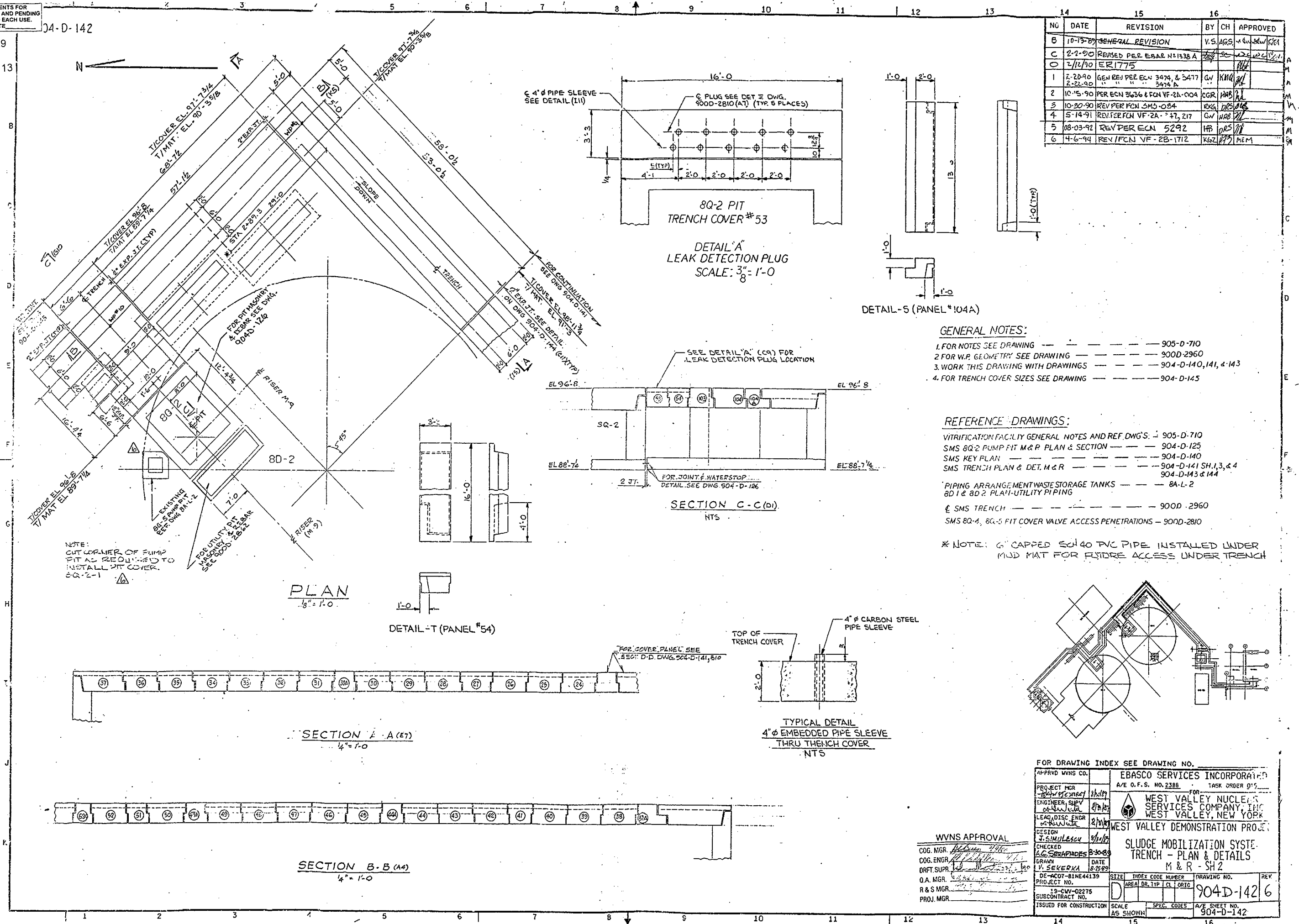
REFERENCE DRAWINGS:

- SMS KEY PLAN — 904-D-140
- SMS TRENCH PLAN & DET. M&R — 904-D-142 SH2
- VITRIFICATION FACILITY GENERAL NOTES — 905-D-710
- AND REF. DRAWINGS.
- VIT. FACILITY ARCHITECTURAL ELEVATION — 905-D-731 SH.1
- VIT. FACILITY GROUND FLOOR PLAN EL. 100'-0" — 905-D-733
- STS SGN SAMPLE PNEUMATIC TRANSFER SYS. — 900D-1211
- SMS TRENCH IN VIT. FACILITY — 904-D-124 SH.1 & 2
- Q SMS TRENCH — 900D-2960
- WASIE TANK FARM VENT LINE LAYOUT & DETS. — 150-L-1205
- SMS 80-5 DIVERSION PIT M&R PLAN & SEC. — 904-D-128
- SMS TRENCH COVER SCHEDULE — 904-D-144 - 146
- SMS 80-5 DIVERSION PIT M&R PLAN & SECT — 900D-2864



FOR DRAWING INDEX SEE DRAWING NO.		EBASCO SERVICES INCORPORATED	
APPROVED WWS CO.	PROJECT MGR. <i>[Signature]</i>	A/E O.F.S. NO. 2388	TASK ORDER 015
ENGINEER (SUPPLY)	ENGINEER (DESIGN)	WEST VALLEY NUCLEAR SERVICES COMPANY, INC.	
LEAD DISC. ENGR.	DESIGN	WEST VALLEY DEMONSTRATION PROJECT	
CHECKED	DESIGN	SLUDGE MOBILIZATION SYSTEM	
DRAWN	DATE	TRENCH - PLAN & DETAILS	
PROJECT NO.	DATE	M & R - SH 1	
ISSUED FOR CONSTRUCTION	SCALE	INDEX CODE NUMBER	DRAWING NO.
AS SHOWN	AS SHOWN	904-D-141	9

104-D-142



NO	DATE	REVISION	BY	CH	APPROVED
B	10-13-89	GENERAL REVISION	V.S.	AGS	✓ G. W. B. W. / G. K. A.
C	2-2-90	REVISED PER EBAR N°1338 A	AGS	SC	W. C. / W. C. / P. C. 1
O	2/12/90	ER1775			W. C.
1	2-20-90 2-22-90	GEN REV PER EGN 3474, & 3477 " " " " 3474 A	GW	KMG	W. C.
2	10-15-90	PER EGN 3636 & FCN VF-2A-004	CGR	HAB	W. C.
3	10-20-90	REV PER FCN 5M3-034	RKG	DOS	W. C.
4	5-14-91	REV PER FCN VF-2A-037, 217	GW	HAB	W. C.
5	08-03-92	REV PER EGN 5292	HAB	DOS	W. C.
6	4-6-94	REV / FCN VF-2B-1712	KGZ	APB	MEM

GENERAL NOTES:

1. FOR NOTES SEE DRAWING --- --- --- 905-D-710
2. FOR W.P. GEOMETRY SEE DRAWING --- --- --- 900D-2960
3. WORK THIS DRAWING WITH DRAWINGS --- --- --- 904-D-140, 141, & 143
4. FOR TRENCH COVER SIZES SEE DRAWING --- --- --- 904-D-145

REFERENCE DRAWINGS:

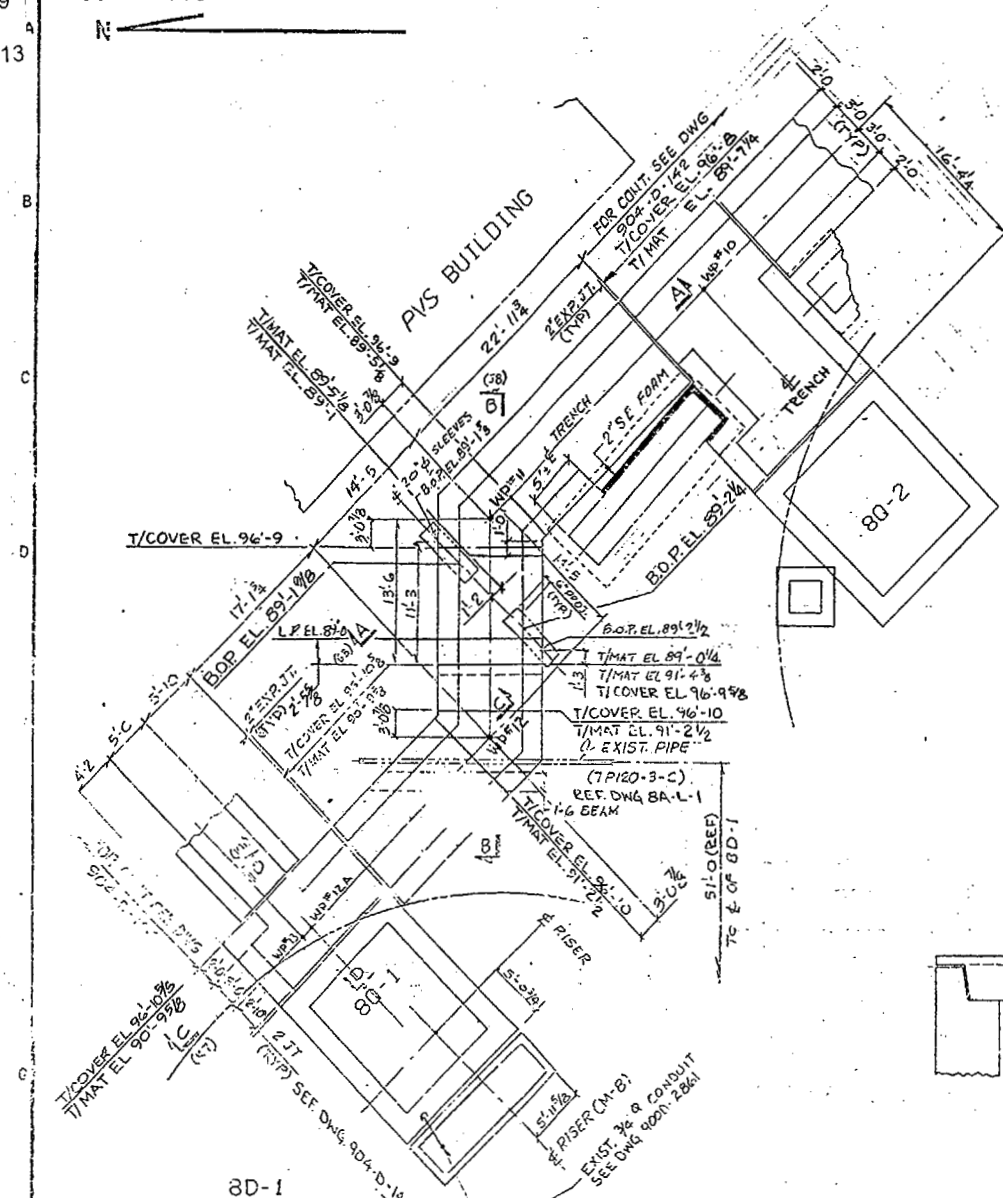
VITRIFICATION FACILITY GENERAL NOTES AND REF. DWGS: - 905-D-710
 SMS 8Q-2 PUMP FIT M&P PLAN & SECTION — — — 904-D-125
 SMS KEY PLAN — — — — — 904-D-140
 SMS TRENCH PLAN & DET. M&R — — — — — 904-D-141 SH.1,3,&4
 904-D-143 & 144
 PIPING ARRANGEMENT WASTE STORAGE TANKS — — — 8A-L-2
 8D1 & 8D2 PLANT-UTILITY PIPING
 & SMS TRENCH — — — — — 900D-2960
 SMS 8Q-4, 8Q-5 FIT COVER VALVE ACCESS PENETRATIONS — 900D-2810

* NOTE: 6" CAPPED SCH 40 PVC PIPE INSTALLED UNDER MUD MAT FOR FUTURE ACCESS UNDER TRENCH

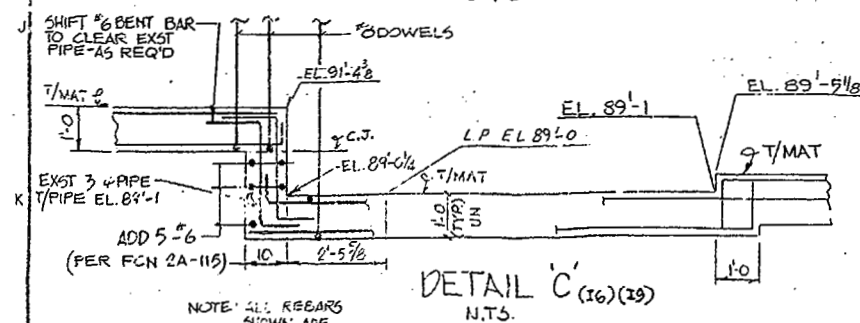
FOR DRAWING INDEX SEE DRAWING NO. _____

FOR DRAWING INDEX SEE DRAWING NO.		EASCO SERVICES INCORPORATED	
APPROV WWS CO.		A/E O.F.S. NO. <u>2388</u> TASK ORDER 015	
PROJECT MGR <i>W. J. HENNING</i>	<i>3/10/87</i>	FOR	
ENGINEER, SHEET <i>OF 11</i>	<i>2/10/87</i>	WEST VALLEY NUCLEAR SERVICES COMPANY, INC. WEST VALLEY, NEW YORK	
LEAD DISC ENGR <i>OF 11</i>	<i>2/10/87</i>	WEST VALLEY DEMONSTRATION PROJECT	
DESIGN <i>J. S. MULESCU</i>	<i>2/10/87</i>	SLUDGE MOBILIZATION SYSTEM TRENCH - PLAN & DETAILS M & R - SH 2	
CHECKED <i>A. G. SERAPHIMOS</i>	<i>2-30-88</i>		
DRAWN <i>V. SEKERKA</i>	DATE <i>8-23-89</i>		
DE-ACOT-81NE44139	SIZE INDEX CODE NUMBER	DRAWING NO.	REV
PROJECT NO.	<input type="checkbox"/> AREA <input type="checkbox"/> DR. <input type="checkbox"/> TYP <input type="checkbox"/> CL <input type="checkbox"/> ORIG	904D-1426	
13-CW-02275			
SUBCONTRACT NO.			
ISSUED FOR CONSTRUCTION	SCALE AS SHOWN	SPEC. CODES	A/E SHEET NO. 904D-142

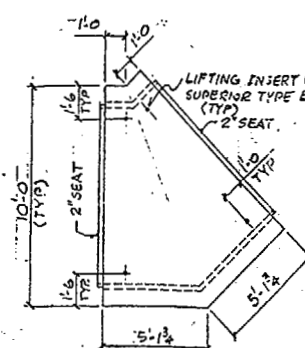
904-D-143



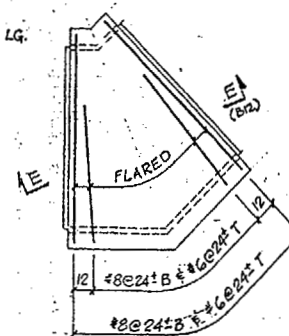
PLAN
1/2" = 1'-0"



DETAIL 'C' (I6)(I9)
N.T.S.

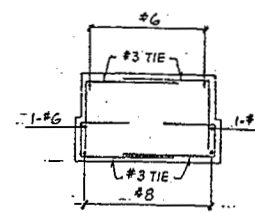


PLAN - MAS.

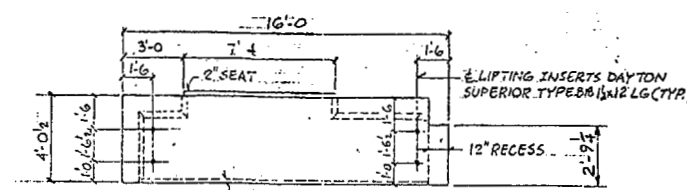


PLAN - REINF

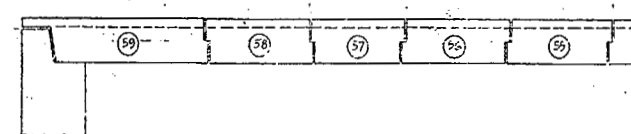
DETAIL 'A' - COVER PANELS 59 & 63



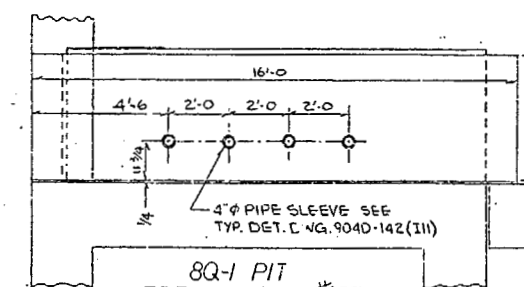
SECTION E-E (A10)



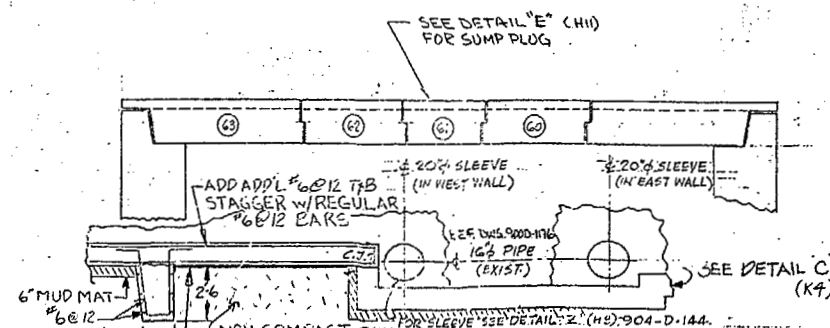
DETAIL 'B' - COVER PANEL 68



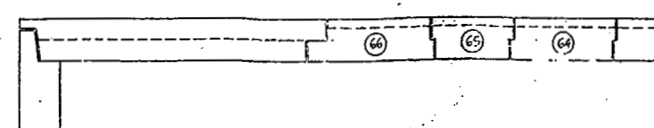
SECTION A - A (02)
1/2/0



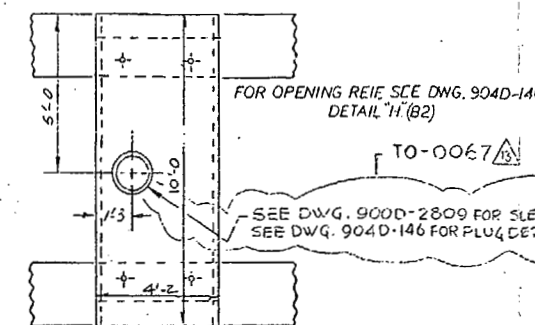
8Q-1 PIT
TRENCH COVER #67
DETAIL "D"
LEAK DETECTION PLUG



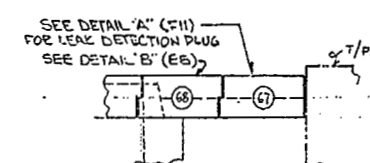
SECTION B-B (c3)



SECTION C-C (G1)
1/4" = 1'-0"



TRENCH COVER #61
DETAIL "E"
TRENCH SUMP PLUG



SECTION D-D (FI)

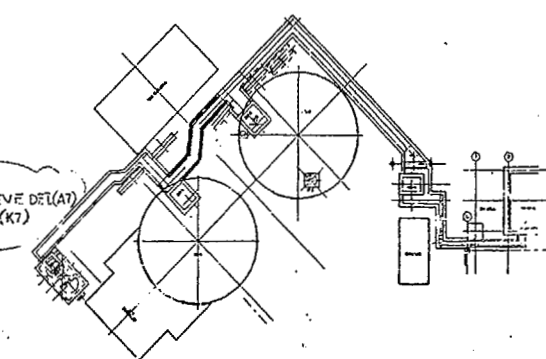
14		15		16	
NO	DATE	REVISION	BY	CH	APPROV
B	10-15-89	GENERAL REVISION	W.S.	SC	W.S. SC
C		REVISED PER EBAR No. 1338A	W.S.	SC	W.S. SC
O	2/12/90	ER 1775			
I	2-19-90	GEN REV PER ECM 3474 & 3477 3474 A	GW	KMB	W.S.
2	10-16-90	PER ECM 3636 & FCN YF-2A-004	CGR	HAB	W.S.
3	10-30-90	REV PER FCN 5MS-034	WKG	PLS	W.S.
4	11-8-90	REV PER FCN VF-2A-032	DAK	DRS	W.S.
5	11-16-90	REV PER FCN VF-2A-050	WKG	KMB	W.S.
6	11-26-90	REV PER FCN VF-2A-067	JCH	WDB	W.S.
7	11-28-90	REV PER ECM 4059	WKG	HAB	W.S.
8	1-31-91	REV/FCN VF-2A-069	W.S.	HAB	W.S.
9	2-6-91	REV/FCN VF-2A-133	W.S.	HAB	W.S.
10	2-14-91	REV PER FCN VF-2A-126	LM	HAB	W.S.
11	3-7-91	REV PER FCN VF-2A-027 VF-2A-115	W.S.	HAB	W.S.
12	5-15-91	REV PER FCN VF-2A-247, VF-2A-258, VF-2A-217	GW	HAB	W.S.
13	3-3-95	REV/FCN-TM-0028	PD	CLS	W.S.

GENERAL NOTES:

- 1 FOR NOTES SEE DRAWING — — — 905-D-710
2 FOR W.P. GEOMETRY SEE DRAWING — — 900D-2960
3 WORK THIS DRAWING WITH DRAWINGS — 904-D-140, 141, 142 & 144
4 FOR TRENCH COVER SIZES & DETS. SEE 904-D-145

REFERENCE DRAWINGS:

- VITRIFICATION FACILITY GENERAL NOTES — 905-D-710
AND REFERENCE DRAWINGS
- SMS KEY PLAN — — — — — 904-D-140
- ☒ SMS TRENCH — — — — — 900D-2960
- SMS TRENCH PLAN & DET. M&R — — — — 904-D-141 SH. 1-4, 142, & 144
- TANK FARM VENTILATION & AS KS 8D-1 & 8D-2 — 900D-1176
- VENTILATION PIPING & SERVICE BUILDING
- PIPING ARRANGEMENT WASTE STORAGE — 8A-L-1
- TANK 8D-1 & 8D-2 PLAN - PROCESS PIPING
- SMS 8Q-4, 8Q-5 PIT COVER ACCESS PENETRATIONS — — 900D-2810

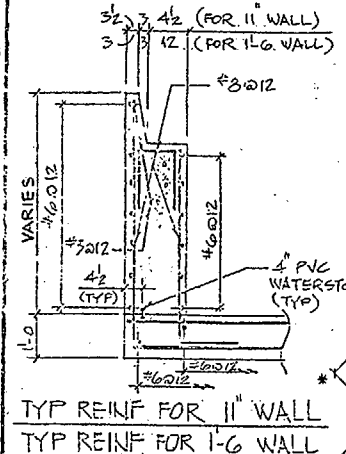


FOR DRAWING INDEX SEE DRAWING NO.		EBCSO SERVICES INCORPORATED	
ACFRD NO. CO.		A/E O.F.S. NO. <u>2388</u>	TACK ORDER CLS
PROJECT NO. <u>1-2388</u>	DATE <u>2/1/79</u>	FOR	
ENGINEER SUPERVISOR <u>OXLEY</u>	DATE <u>2/1/79</u>	WEST VALLEY NUCLEAR SERVICES COMPANY, INC	
LEAD DTC ENGR <u>OXLEY</u>	DATE <u>2/1/79</u>	WEST VALLEY, NEW YORK	
DESIGN <u>J.SIMULESCU</u>	DATE <u>2/1/79</u>	WEST VALLEY DEMONSTRATION PROJECT	
CHECKED <u>S. CASANOVA</u>	DATE <u>8-30-80</u>	SLUDGE MOBILIZATION SYSTEM TRENCH - PLAN & DETAILS	
DRAWN <u>V. SEKERKHA</u>	DATE <u>8-25-80</u>	M & R - SH3	
DC-M007-B1NE44139		SIZE	INDEX CODE NUMBER
PROJECT NO. 19-CW-02275		DRAWN	DR. TYP
SUB CONTRACT NO.		CL	ORIG
ISSUED FOR CONSTRUCTION	SCALE 1/8"=1' 0"	SPEC. CODES	
		A/E SHEET NO. 904D-143	

904-D-144

NOTE: VERT. BARS
NOT SHOWN FOR CLARITY

TYPICAL REBAR DETAIL
AT WALL WITH VARYING THICKNESS
NTS



TYP REINF FOR 11" WALL
TYP REINF FOR 1-6" WALL

NO	DATE	REVISION	BY	CH	APPROVED
14	8-6-92	REV/ECN 5	PD	MS	ML
15	8-24-92	REV/ECN 5456	MS	MS	ML
16	9-10-92	REV/ECN 5495	PD	MS	ML
17	3-10-93	REV/FCN VF-2B 0458	PD	MS	ML
18	1-5-94	REV PER FCN VF-2B-1070	KZ	MS	ML

NO	DATE	REVISION	BY	CH	APPROVED
3	3-7-91	REV PER FCN VF-2A-027	GN	MS	ML
9	4-4-91	PER FCN VF-2A-177	GN	MS	ML
10	5-15-91	REV PER FCN VF-2A-180, VF-2A-217 & VF-2A-247	GN	MS	ML
11	8-2-91	REV PER ECN 4443	GN	MS	ML
12	6-1-92	REV PER ECN 5155	PAK	MS	ML
13	08-03-92	REV PER ECN 5297	MS	MS	ML

NO	DATE	REVISION	BY	CH	APPROVED
8	10-19-89	GENERAL REVISION	VS	SC	ML
C		REVISED PER ECR 1338-A	DS	SC	ML
O	2-12-90	ER 1775	DS	SC	ML
19	1-24-94	REV PER FCN VF-2B-1595	GN	MS	ML
20	3-3-95	REV/FCN-TM-0028	PT	MS	ML

REFERENCE DRAWINGS:

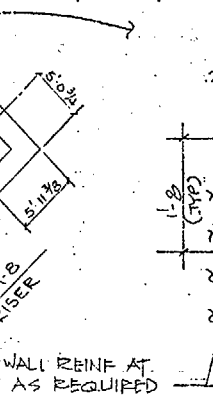
SMS 8Q-4, 8Q-5 PIT COVER VALVE PENETRATIONS 900D-2810 & SMS TRENCH — 900D-2960
 PIPING ARRANGEMENT WASTE STORAGE — 8A-L-2
 TANKS 8D-1 & 8D-2 PLAN UTILITY PIPING
 VITRIFICATION FACILITY GEN. NOTES AND — 905-D-710
 REF DWGS.
 SMS KEY PLAN — 904-D-140
 SMS TRENCH PLAN & DET. M&R — 904-D-143
 SMS 8Q-1 PUMP PIT M&R PLAN & SECT. — 904-D-125
 SMS TRENCH INVF. — 904-D-124

THIS DRAWING IS PART OF
CS-194 EXCEPT AS NOTED
BELOW

SEE DETAIL 'A' (15)
FOR LEAK DETECTION
AND SUMP PLUG

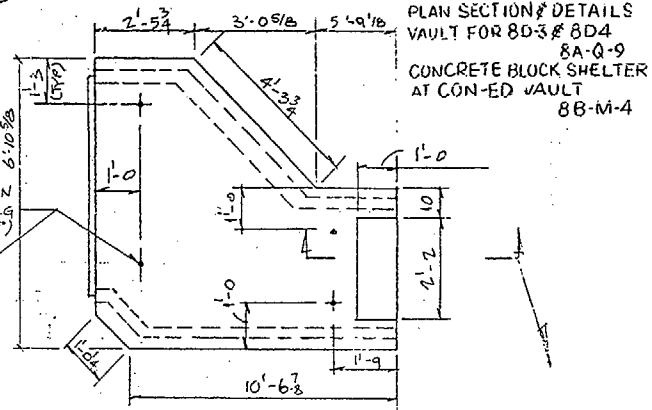
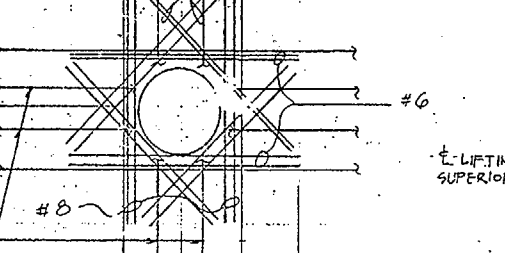
SECTION C-C (E1)

1/4" = 1'-0"



10'2" EXP. JOINT DETAIL

CS-139, ZONE F3,F4,I2



DET Y (PANEL 85)

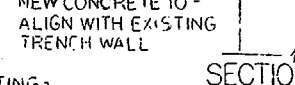
NTS

GENERAL NOTES:

1. FOR NOTES SEE DRAWING — 905-D-710
2. FOR W.R. GEOMETRY SEE DRAWING — 900D-2960
3. WORK THIS DRAWING WITH DRAWINGS — 904-D-140, & 143
4. FOR TRENCH COVER SIZES & DETS. SEE — 904-D-145

DET X (PANEL 79)

NTS



SECTION H-H (F2)

NEW CONCRETE TO ALIGN WITH EXISTING TRENCH WALL

SLOPE

LEVEL

NEW CONCRETE

ROUGHEN EXISTING CONCRETE SURFACES

DRILL HOLES IN EXISTING CONCRETE AND GROUT * BARS IN PLACE (TYP)

* HILTI HIT-100 SYSTEM - PER MFG SPECS

SECTION G-G (F2)

3#5 BARS
2#6 BARS

6" MUD MAT

TRENCH COVER BEARING SURFACE

SLOPE VARIES TO CLEAR DUCT BANK

NON COMPACT SOIL

EXIST. ELEC. DUCT BANK

6" MUD MAT

ELEVATION A-A

20" DIA. SLEEVE

EXIST. 16" DIA. PIPE

WP #13

6" MUD MAT

25' (TYP)

6" MUD MAT

6" MUD MAT

SECTION B-B (B6)

1/2" = 1'-0"

* NOTE: 6" CAPED SCH 40 PVC PIPE INSTALLED UNDER MUD MAT FOR FUTURE ACCESS UNDER TRENCH

6" MUD MAT

6" MUD MAT

6" MUD MAT

SECTION D-D (F9)

TO-0067

SEE DWG. 900D-2800 FOR SLEEVE DET. (A7)

SEE DWG. 904-146 FOR PLUG DET. (K7)

SEE TYP. REINF. DET. FOR 11" WALL (D1)

12" x 5/8" HAL NELSON STUD TYP (S)

4" PIPE SLEEVE SEE TYP. DET. DWG. 904D-142 (I11)

ACCESS SLEEVE & PLUG SEE DWG. 900D-2800 DET. II (A7)

WELD W/ WIRE ACCESSIBLE AT BOTH ENDS TYP

10" SLEEVE TYP (2)

CS-139

SECTION F-F (F2)

CS-139

SECTION G-G (F2)

SECTION H-H (F2)

SECTION I-I (F2)

SECTION J-J (J5)

SECTION K-K (J5)

SECTION L-L (J5)

8Q-4 PIT
TRENCH COVER #94
LEAK DETECTION PLUG &
TRENCH SUMP PLUG

NTS

NOTE: VERT. BARS NOT SHOWN FOR CLARITY

TYP WALL CORNER REINF DETAIL

NTS

NOTE: VERT. BARS NOT SHOWN FOR CLARITY

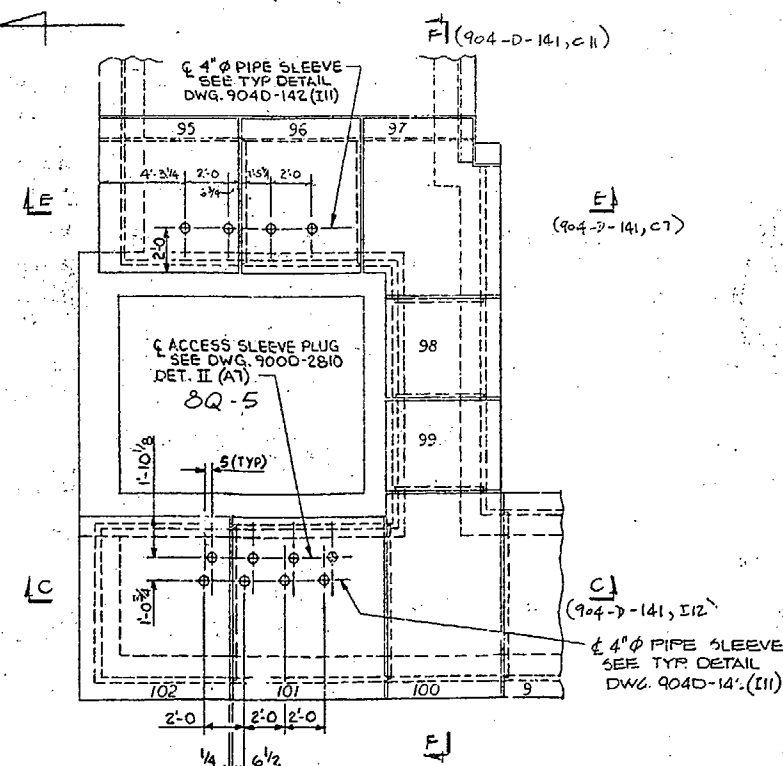
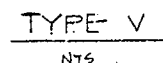
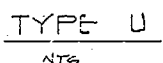
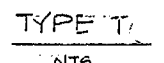
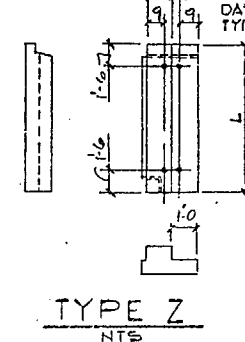
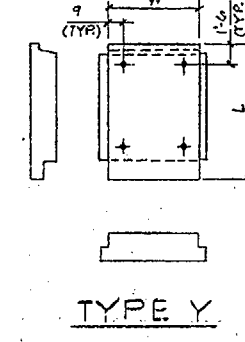
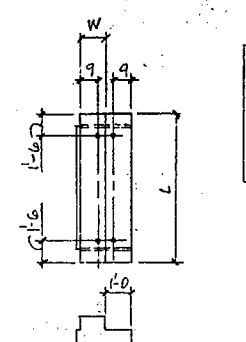
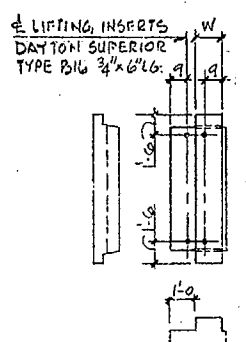
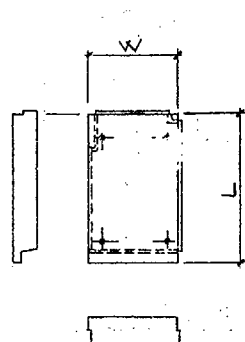
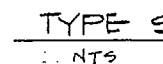
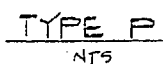
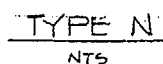
FOR DRAWING INDEX SEE DRAWING NO.	
APPROV WWS CO.	EBASCO SERVICES INCORPORATED
PROJECT MGR	A/E O.F.S. NO. 2388
ENGINEER SUPV	FOR TASK ORDER 015
LEAD DES ENGR	WEST VALLEY NUCLEAR SERVICES COMPANY, INC
DESIGN	WEST VALLEY, NEW YORK
CHECKED	WEST VALLEY DEMONSTRATION PROJECT
DRAWN	SLUDGE MOBILIZATION SYSTEM
DATE	TRENCH - PLAN & DETAILS
PROJECT NO.	M & R - SH 4
SUBCONTRACT NO.	DRAWING NO.
ISSUED FOR CONSTRUCTION	904D-144 20
SCALE	AS SHOWN
SPEC. CODES	AVE SHEET NO. 904-D-144

LIFTING INSERTS
 DAYTON SUPERIOR
 TYPE B 8x12 I-BEAM
 (TYP. UNLESS NOTED)

SEE DET. "D"
 DWG 904-D-140
 (K10) (TYP.
 UNLESS NOTED)

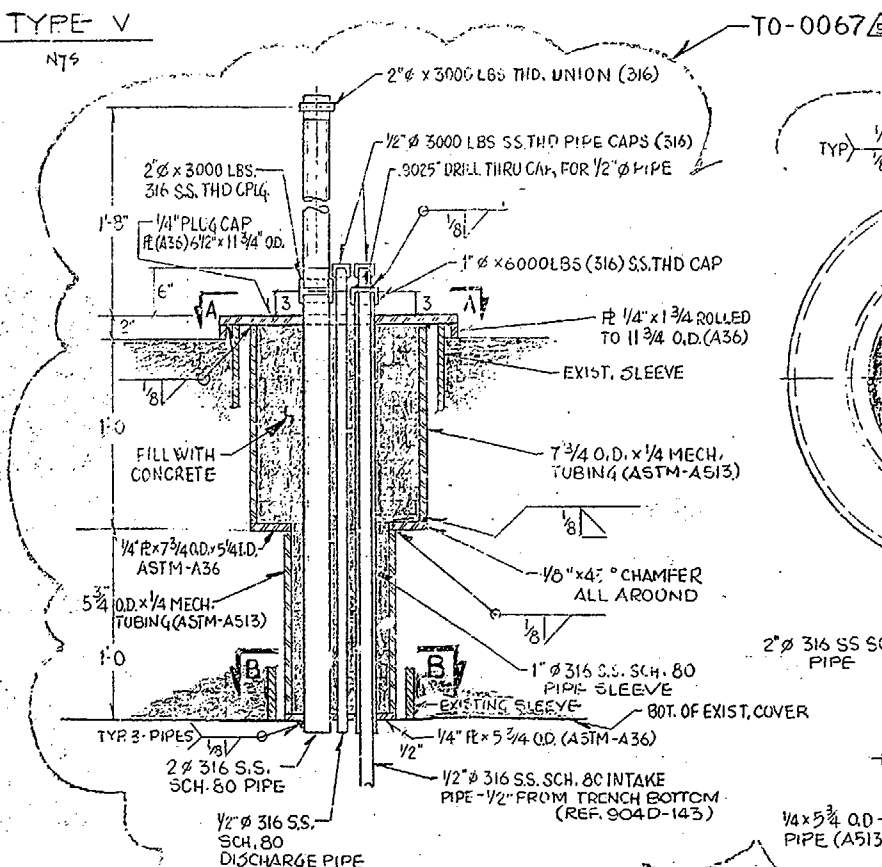
SEE DET. "C"
 DWG 904-D-140
 (K7)

SEE DET. "F"
 DWG 904-D-140 (C11)
 (TYP. UNLESS NOTED)



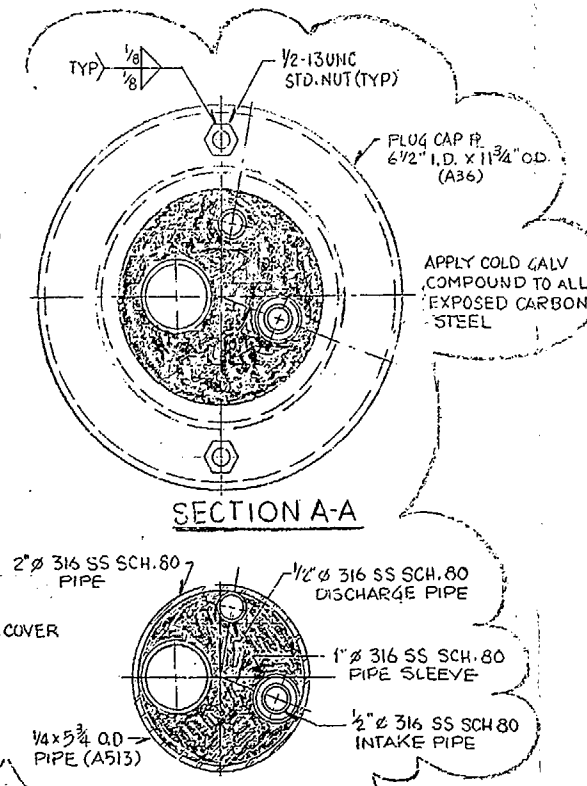
PART PLAN (TRENCH COVER PLAN)

NOTE: FOR INFO. NOT SHOWN SEE
DWG 004-D-141 (E5)



SLEEVE PLUG FOR SMS
TRENCH COVERS T1 & T50

NOT TO SCALE



SECTION B-E

REV NO	DATE	REVISION	DR	CH	APPROVED
0	2-2-90	REVISED PER EECR 44-1975	W	SC	W.C. W.C. W.C.
0	2/12/90	ER175			W.C.
1	2-21-90	REV PER ECH 3479	W	KMO	W.C.
2	2-23-90	REV ECH 3479A	CGR	KMB	W.C.
2	10-17-90	PER FCN 36361 FCN VF24-008	CGR	HAB	W.C.
3	2-14-91	REV PER FCN VF24-008	CN	HAB	W.C.
4	9-14-94	REV PER FCN VF24-2551	MJC	W.C.	W.C.
5	3-3-95	REV/FCN-TM-0028	PD	W.C.	W.C.


1. FOR GENERAL NOTES SEE DRAWING -- 90SD-710
2. WORK THIS DRAWING WITH DRAWINGS -- 90SD-140 THRU 144
3. AFTER TRENCH COVERS & PIT COVER ARE INSTALLED IN PLACE, ALL COIL & INSERT HOLES ARE TO BE DRIED & CLEANED OF ANY LOOSE MATERIAL. COAT ENTIRE HOLE WITH CHEVRON DURA-LITH GREASE - NLG #2. PLUG EACH HOLE WITH DAYTON-SUPERIOR "T7-SLOTTED SETTING PLUGS" ALSO TO BE COATED WITH DURA-LITH GREASE. PLUG TO BE SET FLUSH WITH COIL INSERT APPROXIMATELY $\frac{1}{2}$ " BELOW CONCRETE SURFACE. FILL REMAINING VOID WITH SIKAFLEX-2K NSF/SL SEALANT.

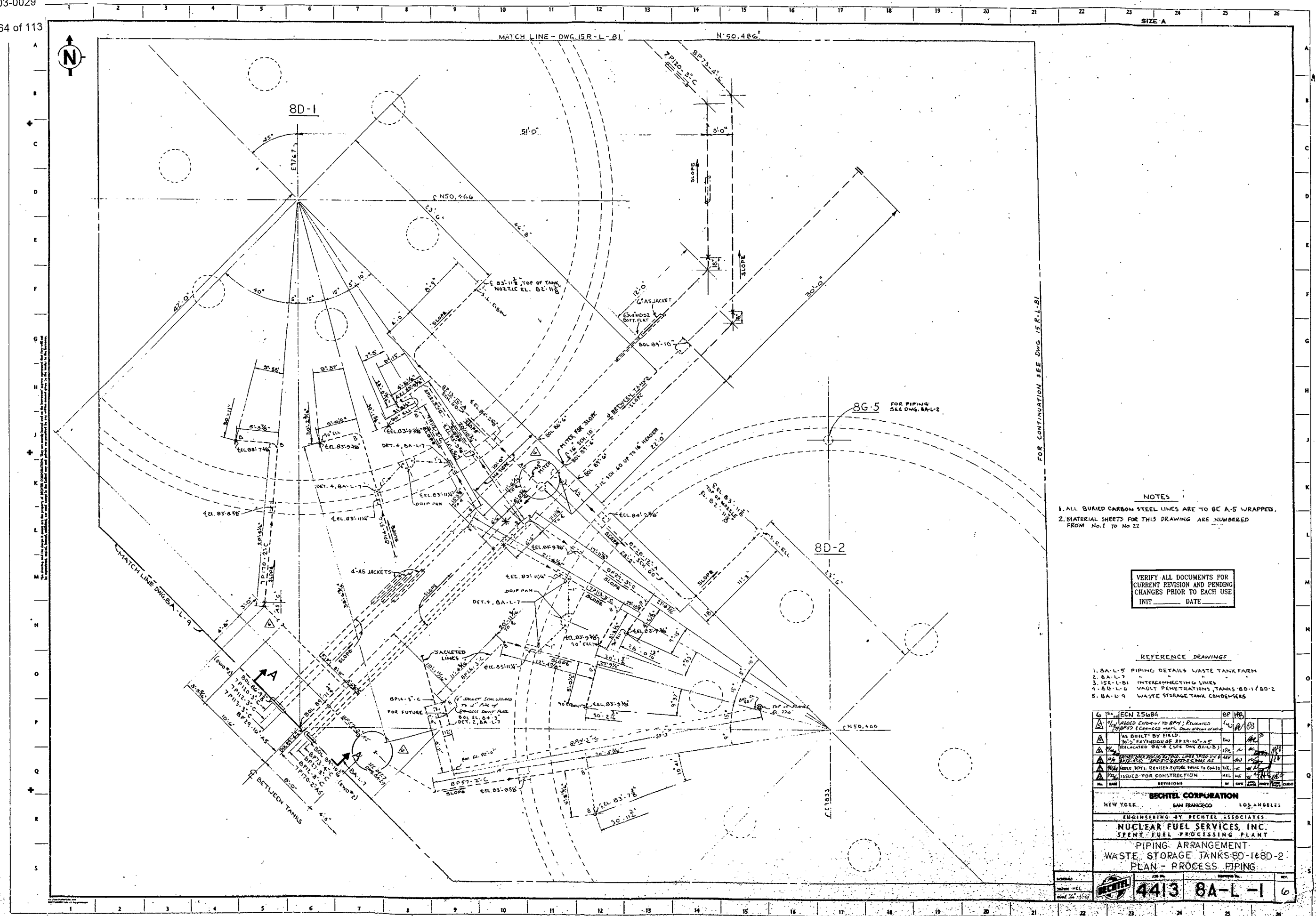
SMS KEY PLAN — — — — 904D-140
SMS TRENCH PLAN & DETS. M&R-904D-141 SH 1
VIT. FAC. GENERAL NOTES & REF DWG-905D-710
8Q-4 & 8Q-5 PIT COVER VALVE — — 900D-2810
ACCESS PENETRATIONS

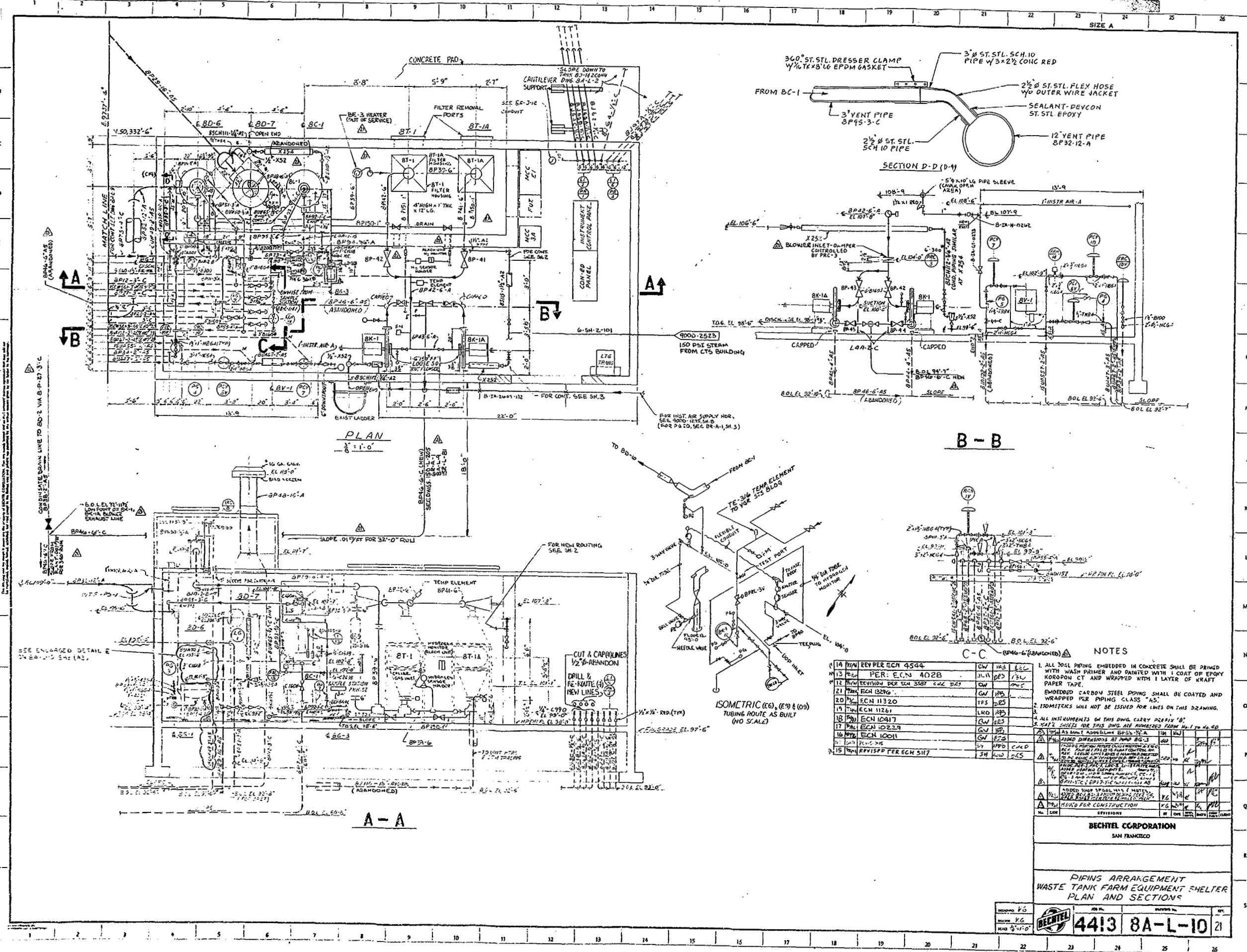
COG. MGR. *WCF* *2/14/80*
COG. ENGR. *WCF* *2/14/80*
DRAFT SUPR. *WCF* *2/14/80*
O.A. MGR. *WCF* *2/14/80*
R & S MGR. *WCF* *2/14/80*
PROJ. MGR. *WCF* *2/14/80*

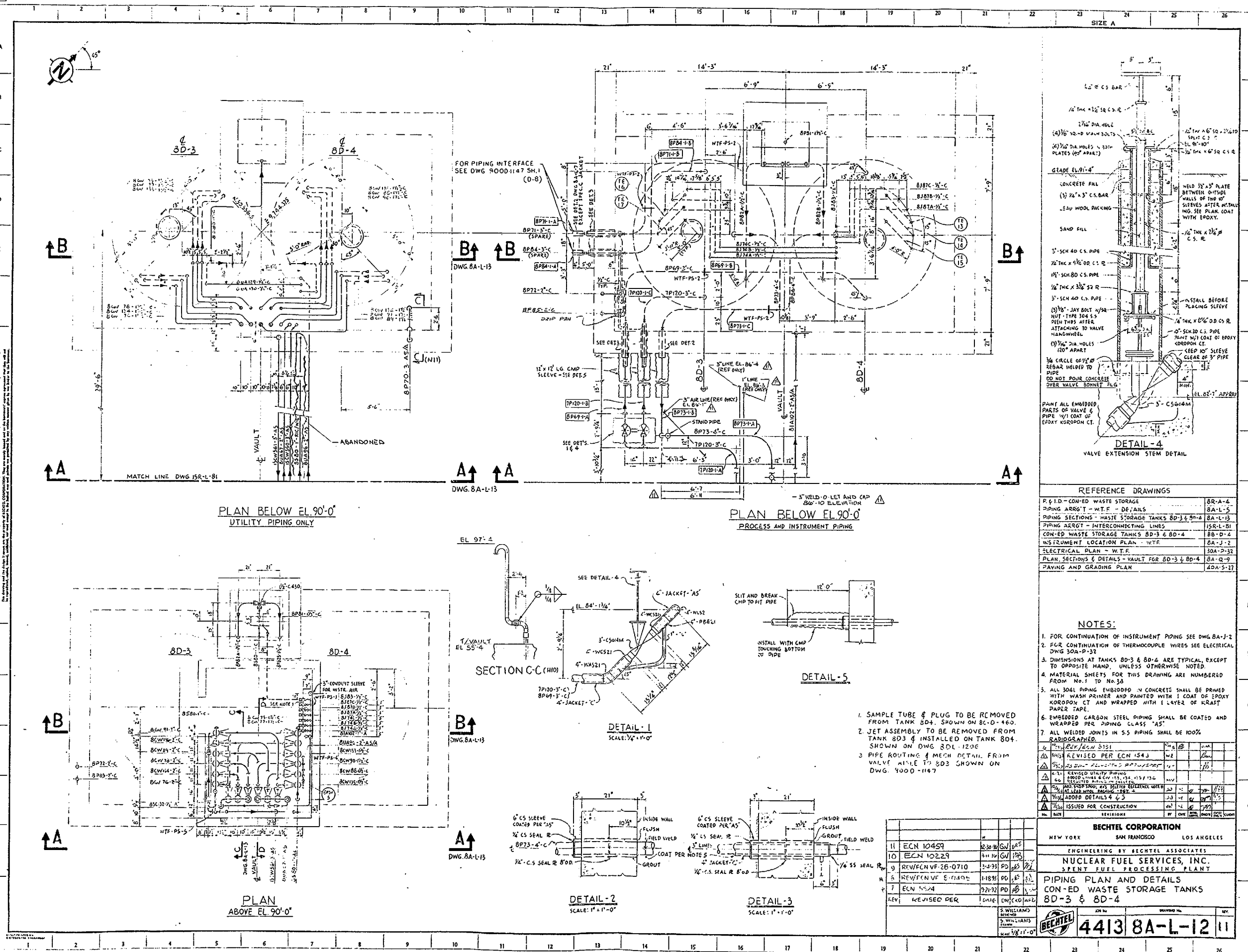
WORK THIS DWG WITH DWG'S 905-D-140 THRU 144

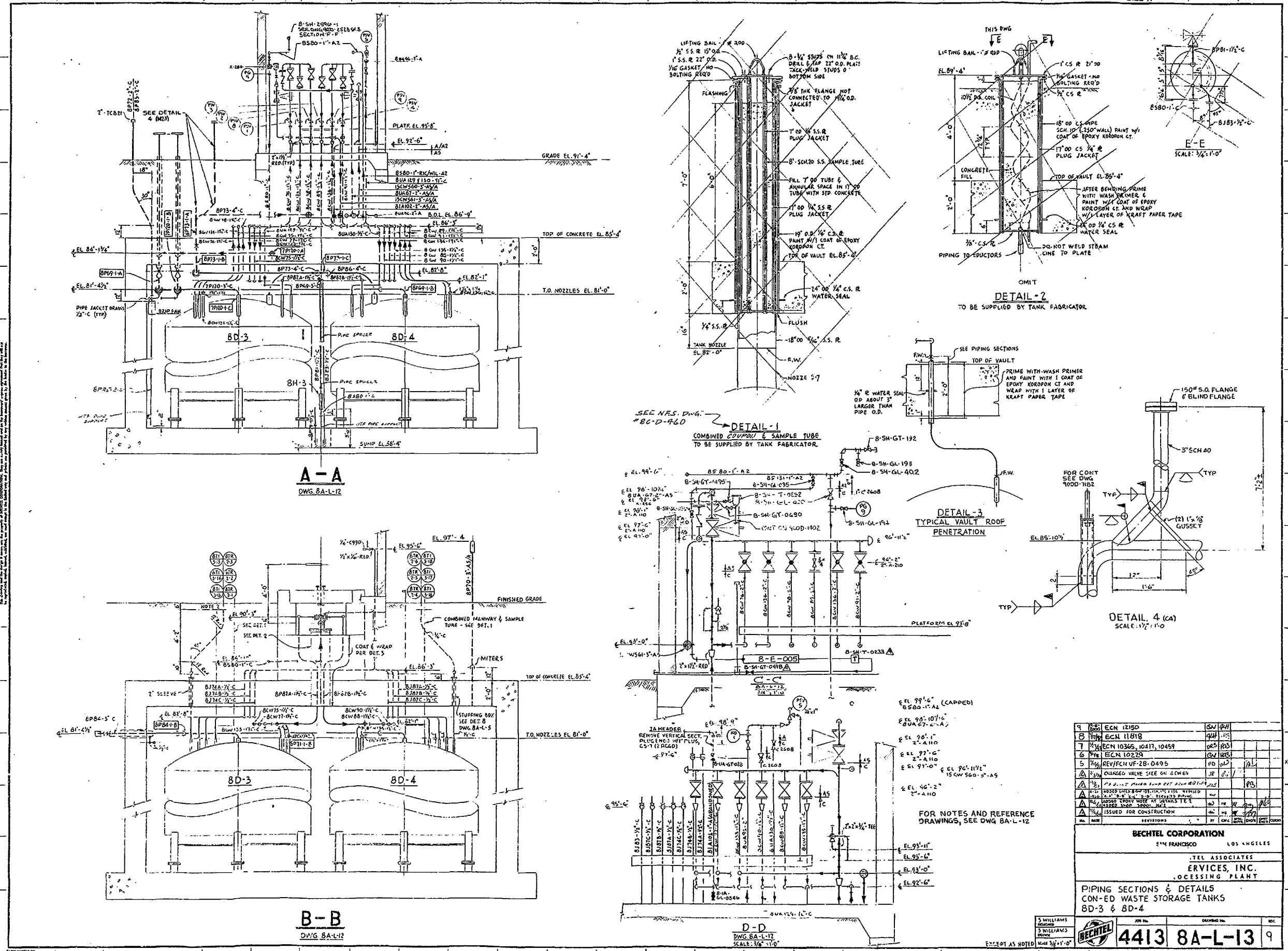
FOR DRAWING INDEX SEE DRAWING NO.

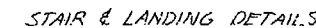
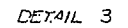
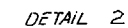
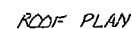
APPRVD WYNS CO.		E BASCO SERVICES INCORPORATED		TASK ORDER <u>15</u>	
PROJECT MGR <u>W. C. Lewis</u>	<u>1/4/90</u>	A/E O. F. S. NO. <u>2308</u>		FOR	
ENGINEER/SUPV <u>W. C. Lewis</u>	<u>1/10/90</u>		WEST VALLEY NUCLEAR SERVICES COMPANY, INC WEST VALLEY, NEW YORK		
LEAD DISC ENGR <u>W. C. Lewis</u>	<u>1/10/90</u>		WEST VALLEY DEMONSTRATION PROJECT		
DESIGN <u>J. Calabrese</u>	<u>1-9-90</u>	SLUDGE MOBILIZATION SYSTEM			
CHECKED <u>J. Calabrese</u>	<u>1-9-90</u>	TRENCH COVER SCHEDULE			
DRAWN <u>J. Calabrese</u>	DATE <u>1/8/90</u>	SH 2.			
DE-ACOT-81NE44139 PROJECT NO.	SIZE	INDEX CODE NUMBER	DRAWING NO.	REV.	
19-CW-02275 SUBCONTRACT NO.	D	AREA DR. TYP. CL. ORIG.	904D-146	5	
ISSUED FOR CONSTRUCTION	SCALE	SPEC. CODES	A/E SHEET NO. <u>904-D-146 B</u>		











NOTES :

1. FOR CONSTRUCTION & WORKMANSHIP OF THE CONE BLOCK WALL SEE SPECIFICATION NO. R-19. ALL SURFACES SHALL BE LAID UP IN STACK BOND UNLESS NOTED OTHERWISE.
2. FOR WELDING JOINT DECK TO SUPPORTING MEMBERS FOLLOW MANUFACTURER'S SPECIFICATION & RECOMMENDATION.
3. FOR LOCATION OF SHELTER SEE DWG. 8A-Q-9
4. FOR PENETRATIONS IN FLOOR SLAB SEE DWG. 8A-L-12

REFERENCE DRAWING 3		
PLAN, SECTION & DETAIL - VAULT FOR 80-3 & 80-4		BA-Q-1
HANDRAIL DETAILS		157A-M-10
STEEL ROOF DECK	SPEC.	1413-R-1
MASONRY	SPEC.	1413-R-1
PIPING PLAN AT CONED VAULT		BA-L-12
PLATFORM AT CONED VAULT		8C-M-3

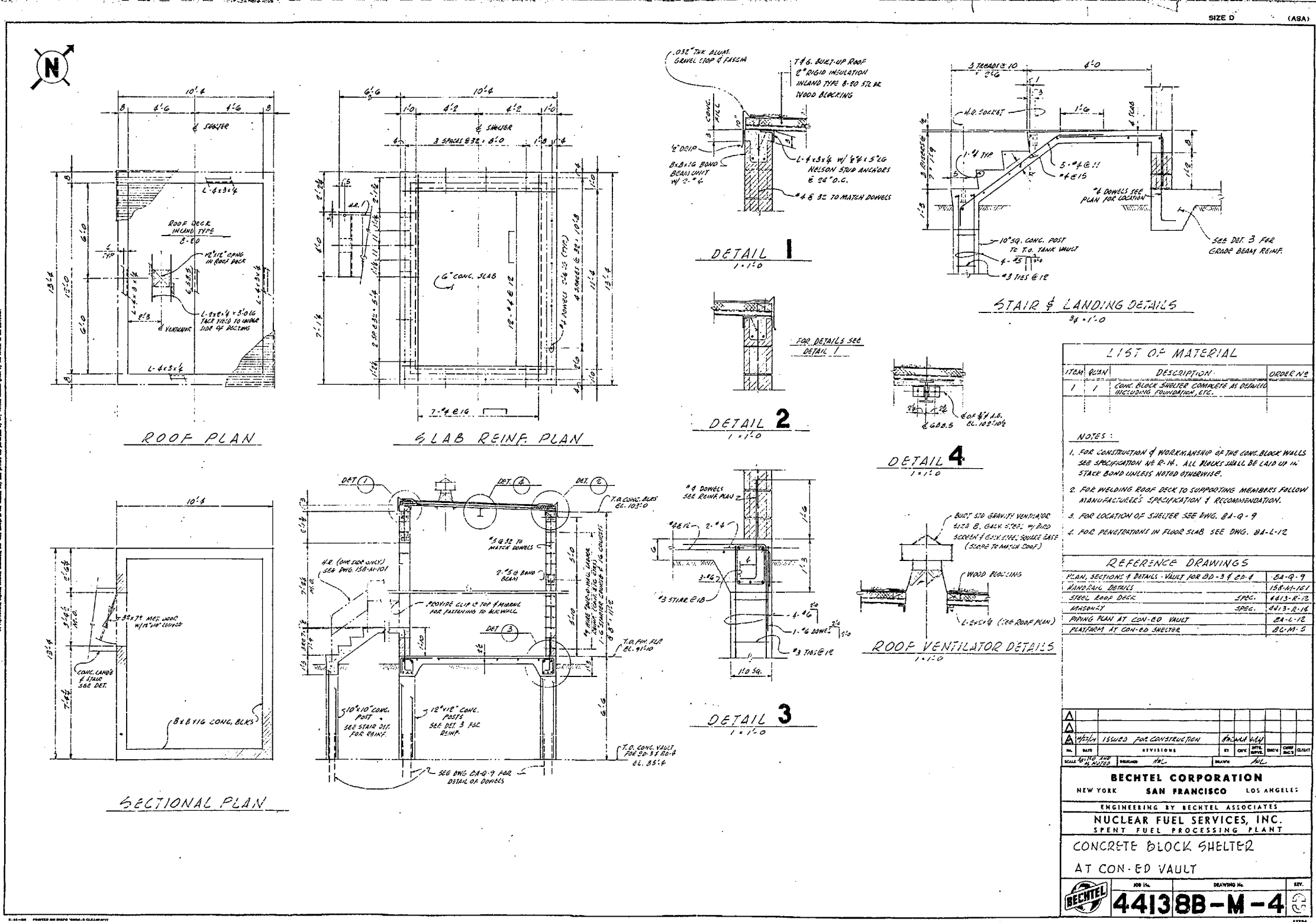
[illegible]

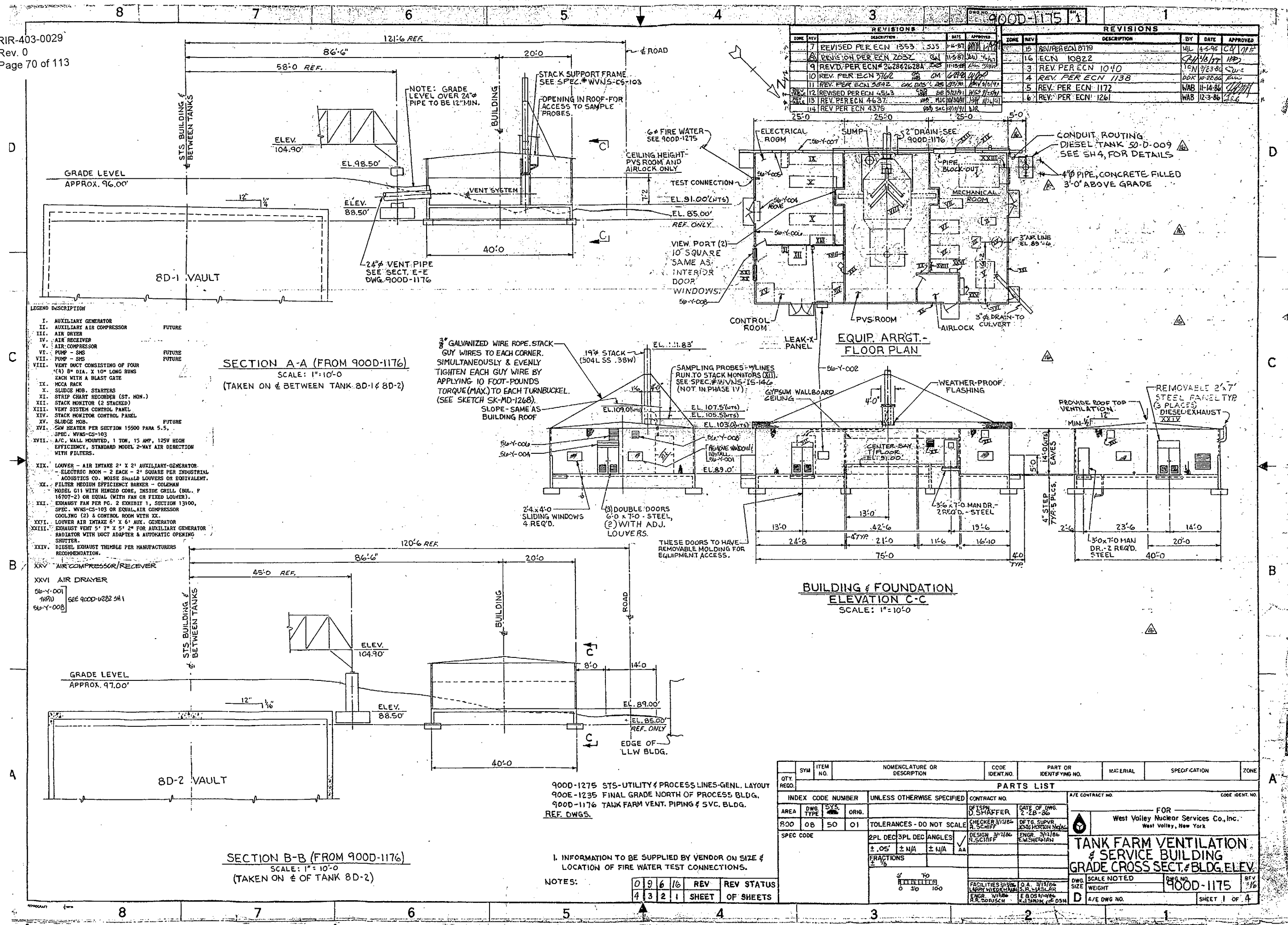
NUCLEAR FUEL SERVICES, INC.
SUBSIDIARY OF W. R. GRACE & CO.
WEST VALLEY, NEW YORK

CONCRETE BLOCK SHELTER AT CON-ED VAULT
REDRAWN FROM RECHTEL DWG 88-A'-4

PROJECT NO.	DRAWING NO.	REV. NO.
	8B-M-571	0

8B-M-4





Appendix B

MicroShield™ Modeling Results for HLW Transfer Trench Piping

Component or area: Lines 55-PH-2-034, 55-PH-2-038, 55-PH-3-003 and 55-PH-3-021

Model geometry used: Cylinder Surface - External Dose Point

Given/Facts:

1. Unshielded radiation probe readings were taken inside the transfer trench at CS-271. The highest reading measured was 9.8 mR/hr.
2. Lines 55-PH-2-034 and 55-PH-2-038, are 2" diameter lines and are enclosed in 4" lines for double containment. These lines are constructed of Schedule 40 stainless steel.
3. Lines 55-PH-3-021 and 55-PH-3-003, are 3" diameter lines and are enclosed in 6" lines for double containment. These lines are constructed of Schedule 40 stainless steel.

Assumptions:

1. The transfer trench was modeled conservatively by using the highest dose reading measured in the trench. The dose point used was at a distance of the longest distance in the trench, or a cross sectional diagonal of the trench. (In other words, it is assumed that the dose point was taken at one corner of the trench, with the source as each individual pipe running through the other corner of the trench.)
2. All radiation is assumed to be coming from each individual line.
3. The internal surfaces of the lines are assumed to be uniformly contaminated with Cs-137.
4. Each line is assumed to be 5' long. In order to get the total curie content of each line, the results will have to be scaled to the entire length of piping.

Input into the model

Distance of the detector to the source: Trench depth = 6' 0.5" (from Drawing 904D-0142)
Trench width = 6' (from Drawing 904D-060)

$$\text{Detector distance} = \sqrt{(72'')^2 + (72.5'')^2} = 102.2''$$

Dimensions of the lines: 2.375" O.D., 0.154" wall thickness* x 5' length
3.5" O.D., 0.216" wall thickness* x 5' length
4.5" O.D., 0.237" wall thickness* x 5' length
6.625" O.D., 0.280" wall thickness* x 5' length

Reading modeled: 9.8 mR/hr

Drawings/References: Drawing 904D-0142, Drawing 904D-060, "Sludge Mobilization System Piping Line List," WVNS-UPLL-010, Revision 10

Work Documents/Surveys: Radiation and Contamination Survey Report 123224, Work Instruction SMTS-994356

*Wall thicknesses and radii of the lines are based on information from "Pocket Ref," Thomas J. Glover, Sequoia Publishing, Inc.

Model prepared by: E. Lauber E. Lauber 2/3/04
Signature/Print name/Date

Model peer reviewed by: E. Y. Lauber E. Y. LAUBER 3 Feb 04
Signature/Print name/Date

MicroShield v6.02 (6.02-0000)
Grove Engineering

Page : 1
DOS File : Lines 55-PH-2-034 and 038.ms6
Run Date: February 3, 2004
Run Time: 10:01:05 AM
Duration : 00:00:00

File Ref: N/A
Date: 2/3/04
By: SL
Checked: SL

Case Title: Lines at CS-271
Description: Lines 55-PH-2-034 and 038, based on 9.8 mR/hr
Geometry: 10 - Cylinder Surface - External Dose Point

Source Dimensions

Height	152.4 cm	5 ft 0.0 in
Radius	2.625 cm	1.0 in

Dose Points

	<u>X</u>	<u>Y</u>	<u>Z</u>
# 1	265.303 cm 8 ft 8.5 in	76.2 cm 2 ft 6.0 in	0 cm 0.0 in

Shields

<u>Shield Name</u>	<u>Dimension</u>	<u>Material</u>	<u>Density</u>
Cyl. Radius	2.625 in	Air	0.00122
Transition	.826 in	Air	0.00122
Shield 2	.237 in	Iron	7.86
Air Gap		Air	0.00122
Wall Clad	.154 in	Iron	7.86

Source Input

Grouping Method : Actual Photon Energies

<u>Nuclide</u>	<u>curies</u>	<u>becquerels</u>	<u>μCi/cm²</u>	<u>Bq/cm²</u>
Ba-137m	2.6296e-001	9.7296e+009	1.0461e+002	3.8707e+006
Cs-137	2.7797e-001	1.0285e+010	1.1058e+002	4.0916e+006

Buildup

The material reference is : Shield 2

Integration Parameters

Y Direction (axial)	20
Circumferential	20

Results

<u>Energy</u> <u>MeV</u>	<u>Activity</u> <u>photons/sec</u>	<u>Fluence Rate</u> <u>MeV/cm²/sec</u> <u>No Buildup</u>	<u>Fluence Rate</u> <u>MeV/cm²/sec</u> <u>With Buildup</u>	<u>Exposure Rate</u> <u>mR/hr</u> <u>No Buildup</u>	<u>Exposure Rate</u> <u>mR/hr</u> <u>With Buildup</u>
0.0045	1.010e+08	1.337e-194	4.396e-27	9.161e-195	3.014e-27
0.0318	2.014e+08	1.343e-23	1.489e-23	1.119e-25	1.240e-25
0.0322	3.716e+08	1.473e-22	1.637e-22	1.185e-24	1.317e-24
0.0364	1.352e+08	2.697e-16	3.115e-16	1.533e-18	1.770e-18
0.6616	8.755e+09	3.038e+03	5.055e+03	5.889e+00	9.800e+00
TOTALS:	9.564e+09	3.038e+03	5.055e+03	5.889e+00	9.800e+00

Page : 1
DOS File : Lines 55-PH-3-003 and 021.ms6
Run Date: February 3, 2004
Run Time: 10:08:02 AM
Duration : 00:00:00

File Ref: N/A
Date: 2/3/04
By: EL
Checked: EL

Case Title: Lines at CS-271
Description: Lines 55-PH-3-003 and 021, based on 9.8 mR/hr
Geometry: 10 - Cylinder Surface - External Dose Point



Source Dimensions
Height 152.4 cm 5 ft 0.0 in
Radius 3.896 cm 1.5 in

Dose Points
1 X 2.68e+02 cm 76.2 cm Z 0 cm
8 ft 9.5 in 2 ft 6.0 in 0.0 in

Shields

Shield Name	Dimension	Material	Density
Cyl. Radius	3.896 in	Air	0.00122
Transition	1.283 in	Air	0.00122
Shield 2	.28 in	Iron	7.86
Air Gap		Air	0.00122
Wall Clad	.216 in	Iron	7.86

Source Input
Grouping Method : Actual Photon Energies

Nuclide	curies	becquerels	μCi/cm ²	Bq/cm ²
Ba-137m	2.9513e-001	1.0920e+010	7.9102e+001	2.9268e+006
Cs-137	3.1198e-001	1.1543e+010	8.3618e+001	3.0939e+006

Buildup
The material reference is : Shield 2

Integration Parameters
Y Direction (axial) 20
Circumferential 20

Results

Energy MeV	Activity photons/sec	Fluence Rate		Exposure Rate	
		No Buildup MeV/cm ² /sec	With Buildup MeV/cm ² /sec	No Buildup mR/hr	With Buildup mR/hr
0.0045	1.134e+08	4.544e-246	4.838e-27	3.114e-246	3.316e-27
0.0318	2.261e+08	8.903e-30	7.509e-26	7.416e-32	6.254e-28
0.0322	4.171e+08	1.563e-28	1.408e-25	1.258e-30	1.133e-27
0.0364	1.518e+08	1.666e-20	1.945e-20	9.468e-23	1.105e-22
0.6616	9.826e+09	2.720e+03	5.053e+03	5.273e+00	9.797e+00
TOTALS:	1.073e+10	2.720e+03	5.053e+03	5.273e+00	9.797e+00

Component or area: Lines 55-PH-2-004, 55-PH-2-005 and 55-PH-2-008

Model geometry used: Cylinder Surface - External Dose Point

Given/Facts:

1. Unshielded radiation probe readings were taken inside the transfer trench at CS-138. The highest reading measured was 2.9 mR/hr.
2. These lines are 2" diameter lines and are enclosed in 4" lines for double containment. These lines are constructed of Schedule 40 stainless steel.

Assumptions:

1. The transfer trench was modeled conservatively by using the highest dose reading measured in the trench. The dose point chosen was set at the longest possible distance of any line from the dose point. This was determined from Drawing 900D-2826, Sheet 1. The lines are contained to a cross sectional area of 22.5" x 118.5". The longest distance would be a diagonal line across this rectangular area.
2. All radiation is assumed to be coming from each individual line.
3. The internal surfaces of the lines are assumed to be uniformly contaminated with Cs-137.
4. Each line is assumed to be 5' long. In order to get the total curie content of each line, the results will have to be scaled to the entire length of piping.

Input into the model

Distance of the detector to the source:

$$\text{Detector distance} = \sqrt{(22.5")^2 + (118.5")^2} = 120.6"$$

Dimensions of the lines: 2.375" O.D., 0.154" wall thickness* x 5' length
4.5" O.D., 0.237" wall thickness* x 5' length

Reading modeled: 2.9 mR/hr

Drawings/References: Drawing 900D-2826, Sheet 1, Drawing 904D-060, "Sludge Mobilization System Piping Line List," WVNS-UPLL-010, Revision 10

Work Documents/Surveys: Radiation and Contamination Survey Report 123224, Work Instruction SMTS-994356

*Wall thicknesses and radii of the lines are based on information from "Pocket Ref," Thomas J. Glover, Sequoia Publishing, Inc.

Model prepared by: E. Lachapelle E. Lachapelle 2/3/04
Signature/Print name/Date

Model peer reviewed by: E. Y. LAUBER E. Y. LAUBER 3 Feb 04
Signature/Print name/Date

Page : 1
DOS File : Lines 55-PH-2-034, 005 and 008.ms6
Run Date: February 3, 2004
Run Time: 9:58:27 AM
Duration : 00:00:00

File Ref: N/A
Date: 2/3/04
By: EL
Checked: EL

Case Title: Lines at CS-271
Description: Lines 55-PH-2-004, 005 and 008, based on 2.9 mR/hr
Geometry: 10 - Cylinder Surface - External Dose Point



Source Dimensions
Height 152.4 cm 5 ft 0.0 in
Radius 2.625 cm 1.0 in

Dose Points

	X	Y	Z
# 1	312.039 cm 10 ft 2.8 in	76.2 cm 2 ft 6.0 in	0 cm 0.0 in

Shields

Shield Name	Dimension	Material	Density
Cyl. Radius	2.625 in	Air	0.00122
Transition	.826 in	Air	0.00122
Shield 2	.237 in	Iron	7.86
Air Gap		Air	0.00122
Wall Clad	.154 in	Iron	7.86

Source Input

Grouping Method : Actual Photon Energies

Nuclide	curies	becquerels	$\mu\text{Ci/cm}^2$	Bq/cm ²
Ba-137m	1.0670e-001	3.9479e+009	4.2448e+001	1.5706e+006
Cs-137	1.1279e-001	4.1733e+009	4.4871e+001	1.6602e+006

Buildup

The material reference is : Shield 2

Integration Parameters

Y Direction (axial)	20
Circumferential	20

Results

Energy MeV	Activity photons/sec	Fluence Rate		Exposure Rate	
		No Buildup MeV/cm ² /sec	With Buildup MeV/cm ² /sec	No Buildup mR/hr	With Buildup mR/hr
0.0045	4.098e+07	4.394e-195	1.299e-27	3.012e-195	8.903e-28
0.0318	8.173e+07	4.417e-24	4.895e-24	3.679e-26	4.078e-26
0.0322	1.508e+08	4.833e-23	5.371e-23	3.890e-25	4.323e-25
0.0364	5.488e+07	8.665e-17	1.001e-16	4.923e-19	5.685e-19
0.6616	3.552e+09	8.991e+02	1.496e+03	1.743e+00	2.900e+00
TOTALS:	3.881e+09	8.991e+02	1.496e+03	1.743e+00	2.900e+00

Appendix C

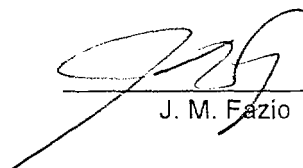
Peer Reviewed Batch 10 Vitrification Run Scaling Factors for
HLW Trench Piping and Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5

**Batch 10 Vitrification Run Scaling Factors for
HLW Trench Piping and Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5**

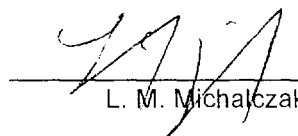
Project Isotope	Batch 10 Radionuclide Distribution Analysis Date May 15, 1997 ($\mu\text{Ci/g}$)	Batch 10 Radionuclide Distribution Analysis Decayed/Ingrown to September 30, 2004 ($\mu\text{Ci/g}$)	Batch 10 Scaling Factor Decayed/Ingrown to September 30, 2004
C-14	4.90e-04	4.90e-04	2.03e-07
Tc-99	8.45e-02	8.45e-02	3.51e-05
I-129	3.90e-07	3.90e-07	1.62e-10
U-232*	9.97e-03	9.29e-03	3.85e-06
U-233	3.60e-03	3.60e-03	1.49e-06
U-234	1.30e-03	1.38e-03	5.73e-07
U-235	3.80e-05	3.80e-05	1.58e-08
Np-237	2.00e-02	2.00e-02	8.30e-06
U-238	3.40e-04	3.40e-04	1.41e-07
Pu-238	3.96e+00	3.74e+00	1.55e-03
Pu-239	1.09e+00	1.09e+00	4.52e-04
Pu-240	7.70e-01	7.74e-01	3.21e-04
Pu-241	3.43e+01	2.40e+01	9.96e-03
Am-241	3.21e+01	3.21e+01	1.33e-02
Cm-243	2.58e-01	2.16e-01	8.96e-05
Cm-244	6.72e+00	5.07e+00	2.10e-03
Cs-137	2.85e+03	2.41e+03	1.00e+00
Sr-90	2.75e+03	2.30e+03	9.54e-01

* U-232 was not analyzed for in the Batch 10 sample. A conservative scaling factor was developed by taking the highest ratio for U-232:U-233, U-232:U-234, and U-232:U-238 using the isotopic distributions developed in the ORIGEN-based spent nuclear fuel distribution (Memorandum FI:2002:0003 (Reissue), J. L. Mahoney to Distribution, "Bounding Isotope Ratios for NFS Spent Fuels," dated February 19, 2002) and then using that ratio's value for U-232 above. The U-232:U-234 ratio resulted in a bounding value of 9.97e-03 which resulted in a corrected scaling factor of 3.69e-06 for U-232.

Prepared By:

 2/13/04 2/13/04
J. M. Fazio

Peer Reviewed By:

 2/13/04
L. M. Michalczak

Appendix D

MicroShield™ Modeling Results for Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5

Component or area: 8Q-1 Pit

Model geometry used: Rectangular Volume

Given/Facts:

1. Unshielded probe readings were taken inside the 8Q-1 pit at 1 foot intervals. The highest reading measured was 53.4 mR/hr.
2. There is approximately 382 lbs of piping/equipment within the 8Q-1 pit. (WO 9400911)

Assumptions:

1. The pit was modeled using a conservative approach by obtaining the highest dose reading measured in the pit and moving the dose point to the outside of the volume and the density of the source was determined by using the weight of the equipment inside the pit.
2. All contamination was assumed to be exclusively Cs-137.
3. Material in the pit was assumed to be iron.

Calculation:

Input into the model

Detector position: Flush with top of pit area; centered geometrically over the pit at a distance of 2" from the surface of the volume.

Source dimensions: 5"10.75" by 11' by 13'

Reading modeled: 53.4 mR/hr

Source material: Combination of air, piping and components (382 lbs)

Drawings: 904D-125, Rev.6

Work Documents/Surveys: Radiation Protection Survey #122979, WO 9400911

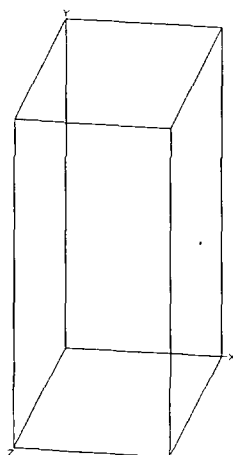
Model prepared by: E.Y. Lauber E.Y. Lauber 13 Jan 04
Signature/Print name/Date

Model peer reviewed by: E.B. Lachapelle E.B. Lachapelle 1/13/04
Signature/Print name/Date

Page : 1
DOS File : 8Q1PitCharacterization_03Dec30EYL.ms6
Run Date: January 12, 2004
Run Time: 7:53:07 AM
Duration : 00:00:01

File Ref: _____
Date: Jan 04
By: Em J. Lankford
Checked: EL

Case Title: 8Q-1 Pit
Description: WTF Characterization
Geometry: 13 - Rectangular Volume



Source Dimensions			
Length	179.705 cm	5 ft 10.8 in	
Width	335.28 cm	11 ft	
Height	396.24 cm	13 ft 0.0 in	

Dose Points			
	X	Y	Z
# 1	184.785 cm 6 ft 0.7 in	198.12 cm 6 ft 6.0 in	167.64 cm 5 ft 6.0 in

Shields			
Shield Name	Dimension	Material	Density
Source	2.39e+07 cm ³	Carbon	0.00725
Air Gap		Air	0.00122

Source Input				
Grouping Method : Actual Photon Energies				
Nuclide	curies	becquerels	μCi/cm ³	Bq/cm ³
Ba-137m	2.9546e-001	1.0932e+010	1.2376e-002	4.5791e+002
Cs-137	3.1233e-001	1.1556e+010	1.3082e-002	4.8405e+002

Buildup
The material reference is : Source

Integration Parameters	
X Direction	10
Y Direction	20
Z Direction	20

Results					
Energy MeV	Activity photons/sec	Fluence Rate MeV/cm ² /sec No Buildup	Fluence Rate MeV/cm ² /sec With Buildup	Exposure Rate mR/hr No Buildup	Exposure Rate mR/hr With Buildup
0.0318	2.263e+08	2.523e+01	3.413e+01	2.102e-01	2.843e-01
0.0322	4.176e+08	4.718e+01	6.385e+01	3.797e-01	5.139e-01
0.0364	1.520e+08	1.967e+01	2.679e+01	1.118e-01	1.522e-01
0.6616	9.837e+09	2.557e+04	2.705e+04	4.956e+01	5.245e+01
TOTALS:	1.063e+10	2.566e+04	2.718e+04	5.027e+01	5.340e+01

Component or area: 8Q-2 Pit

Model geometry used: Rectangular Volume

Given/Facts:

1. Unshielded probe readings were taken inside the 8Q-2 pit at 1 foot intervals. The highest reading measured was 33.5 R/hr.
2. There is approximately 417 lbs of piping/equipment within the 8Q-2 pit. (WO 9400911)

Assumptions:

1. The pit was modeled using a conservative approach by obtaining the highest dose reading measured in the pit and moving the dose point to the outside of the volume. The density of the source was determined by using the weight of the equipment inside the pit.
2. All contamination was assumed to be exclusively Cs-137.
3. Material in the pit was assumed to be iron.

Calculation:

Input into the model

Detector position: Flush with top of pit area; centered geometrically over the pit at a distance of 2" from the surface of the volume.

Source dimensions: 6'5" by 12' by 13' 6"

Reading modeled: 33.5 R/hr

Source material: Combination of air, piping and components (417 lbs. at a density of .00683 gm/cm³)

Drawings: 904D-125, Rev.6, 904D-126 Rev. 5

Work Documents/Surveys: Radiation Protection Survey #122979, WO 9400911

Model prepared by: E.Y. Lauber E.Y. Lauber 19 Jan 04
Signature/Print name/Date

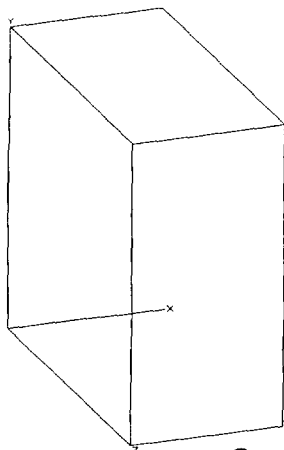
Model peer reviewed by: E.B. Lachapelle E.B. Lachapelle 1/19/04
Signature/Print name/Date

MicroShield v6.02 (6.02-0000)
Grove Engineering

Page : 1
DOS File : 8Q2PitCharacterization_04Jan11EYL.ms6
Run Date: January 12, 2004
Run Time: 8:15:12 AM
Duration : 00:00:01

File Ref: _____
Date: 19 Jan 04
By: Em J. Haden
Checked: EL

Case Title: 8Q-2 Pump Pit
Description: WTF Characterization of 8Q-2 Pump Pit based on 33.5 R/hr
Geometry: 13 - Rectangular Volume



Source Dimensions		
Length	184.15 cm	6 ft 0.5 in
Width	411.48 cm	13 ft 6.0 in
Height	365.76 cm	12 ft

Dose Points			
#	X	Y	Z
# 1	189.23 cm 6 ft 2.5 in	182.88 cm 6 ft	205.74 cm 6 ft 9.0 in

Shields			
Shield Name	Dimension	Material	Density
Source	2.77e+07 cm ³	Iron	0.00683
Air Gap		Air	0.00122

Source Input				
Grouping Method : Actual Photon Energies				
Nuclide	curies	becquerels	μCi/cm ³	Bq/cm ³
Ba-137m	2.0922e+002	7.7410e+012	7.5489e+000	2.7931e+005
Cs-137	2.2116e+002	8.1829e+012	7.9798e+000	2.9525e+005

Buildup
The material reference is : Source

Integration Parameters	
X Direction	10
Y Direction	20
Z Direction	20

Results					
Energy MeV	Activity photons/sec	Fluence Rate MeV/cm ² /sec No Buildup	Fluence Rate MeV/cm ² /sec With Buildup	Exposure Rate mR/hr No Buildup	Exposure Rate mR/hr With Buildup
0.0318	1.603e+11	1.897e+03	1.951e+03	1.580e+01	1.625e+01
0.0322	2.957e+11	3.669e+03	3.776e+03	2.953e+01	3.039e+01
0.0364	1.076e+11	2.164e+03	2.248e+03	1.230e+01	1.277e+01
0.6616	6.965e+12	1.654e+07	1.725e+07	3.207e+04	3.344e+04
TOTALS:	7.529e+12	1.655e+07	1.726e+07	3.212e+04	3.350e+04

Component or area: 8Q-4 Pit

Model geometry used: Rectangular Volume

Given/Facts:

1. Unshielded probe readings were taken inside the 8Q-4 pit at 1 foot intervals. The highest reading measured was 16.2 mR/hr.
2. There is approximately 927 lbs of piping/equipment within the 8Q-4 pit. (WO 9400911)

Assumptions:

1. The pit was modeled using a conservative approach by obtaining the highest dose reading measured in the pit and moving the dose point to the outside of the volume and the density of the source was determined by using the weight of the equipment inside the pit.
2. All contamination was assumed to be exclusively Cs-137.
3. Material in the pit was assumed to be iron.

Calculation:

Input into the model

Detector position: Flush with top of pit area; centered geometrically over the pit at a distance of 2" from the surface of the volume.

Source dimensions: 6' by 7' by 6'

Reading modeled: 16.2 mR/hr

Source material: Combination of air, piping and components (927 lbs)

Drawings: 904D-127, Rev.12

Work Documents/Surveys: Radiation Protection Survey #122979, WO 9400911

Model prepared by: E.Y. Lauber E.Y. Lauber 20 Jan 04
Signature/Print name/Date

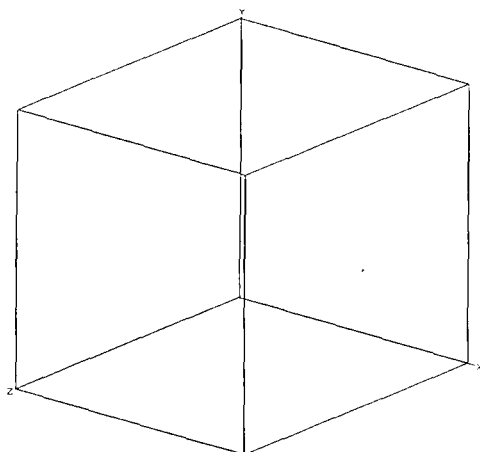
Model peer reviewed by: E.B. Lachapelle E.B. Lachapelle 1/20/04
Signature/Print name/Date

MicroShield v6.02 (6.02-0000)
Grove Engineering

Page : 1
DOS File : 8Q4PitCharacterization_03Dec29EYL.ms6
Run Date: January 12, 2004
Run Time: 8:35:10 AM
Duration : 00:00:01

File Ref: _____
Date: 20 Jan 04
By: Greg Landrum
Checked: EL

Case Title: 8Q-4 Pit
Description: WTF Characterization of 8Q-4 pit at 16.2 mR/hr
Geometry: 13 - Rectangular Volume



Source Dimensions

Length	182.88 cm	6 ft
Width	213.36 cm	7 ft 0.0 in
Height	182.88 cm	6 ft

Dose Points

	<u>X</u>	<u>Y</u>	<u>Z</u>
# 1	187.96 cm 6 ft 2.0 in	91.44 cm 3 ft	106.68 cm 3 ft 6.0 in

Shields

<u>Shield Name</u>	<u>Dimension</u>	<u>Material</u>	<u>Density</u>
Source	7.14e+06 cm ³	Iron	0.05894
Air Gap		Air	0.00122

Source Input

Grouping Method : Actual Photon Energies

<u>Nuclide</u>	<u>curies</u>	<u>becquerels</u>	<u>μCi/cm³</u>	<u>Bq/cm³</u>
Ba-137m	4.8265e-002	1.7858e+009	6.7637e-003	2.5026e+002
Cs-137	5.1020e-002	1.8877e+009	7.1498e-003	2.6454e+002

Buildup

The material reference is : Source

Integration Parameters

X Direction	10
Y Direction	20
Z Direction	20

Results

<u>Energy</u> <u>MeV</u>	<u>Activity</u> <u>photons/sec</u>	<u>Fluence Rate</u> <u>MeV/cm²/sec</u> <u>No Buildup</u>	<u>Fluence Rate</u> <u>MeV/cm²/sec</u> <u>With Buildup</u>	<u>Exposure Rate</u> <u>mR/hr</u> <u>No Buildup</u>	<u>Exposure Rate</u> <u>mR/hr</u> <u>With Buildup</u>
0.0318	3.697e+07	1.224e-01	1.275e-01	1.019e-03	1.062e-03
0.0322	6.821e+07	2.416e-01	2.518e-01	1.944e-03	2.027e-03
0.0364	2.482e+07	1.687e-01	1.774e-01	9.585e-04	1.008e-03
0.6616	1.607e+09	6.780e+03	8.355e+03	1.314e+01	1.620e+01
TOTALS:	1.737e+09	6.781e+03	8.355e+03	1.315e+01	1.620e+01

Component or area: 8Q-5 Pit

Model geometry used: Rectangular Volume

Given/Facts:

1. Unshielded probe readings were taken inside the 8Q-5 pit at 1 foot intervals. The highest reading measured was 6 mR/hr.

Assumptions:

1. The pit was modeled using a conservative approach by obtaining the highest dose reading measured in the pit and moving the dose point to the outside of the volume and the density of the source was conservatively assumed to be 1/2 the volume of the pit. (density of 3.93 versus 7.86 g/cm³).
2. All contamination was assumed to be exclusively Cs-137.
3. Material in the pit was assumed to be iron.

Calculation:

Input into the model

Detector position: Flush with top of pit area; centered geometrically over the pit at a distance of 2" from the surface of the volume.

Source dimensions: 5'1.5" by 9' by 12'

Reading modeled: 6 mR/hr

Source material: Combination of air, piping and components (iron assumed to be 1/2 volume of pit at density of 3.93 g/cm³)

Drawings: 904D-128, Rev.5, 904D-125 Rev. 6

Work Documents/Surveys: Radiation Protection Survey #122979, WO 9400911

Model prepared by: *E.Y. Lauber* E.Y. Lauber 19 Jan 04
Signature/Print name/Date

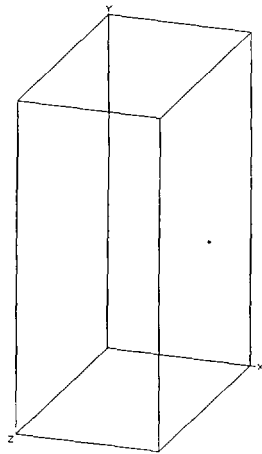
Model peer reviewed by: *E.B. Lachapelle* E.B. Lachapelle 1/19/04
Signature/Print name/Date

MicroShield v6.02 (6.02-0000)
Grove Engineering

Page : 1
DOS File : 8Q5PitCharacterization_04Jan11EYL.ms6
Run Date: January 12, 2004
Run Time: 9:02:34 AM
Duration : 00:00:01

File Ref: _____
Date: 12 Jan 04
By: E. J. L. L.
Checked: EJ

Case Title: 8Q-5 Pit
Description: WTF Characterization of 8Q-5 Pit based on 6 mR/hr
Geometry: 13 - Rectangular Volume



Source Dimensions			
Length	156.21 cm	5 ft 1.5 in	
Width	274.32 cm	9 ft	
Height	365.76 cm	12 ft	

Dose Points			
	<u>X</u>	<u>Y</u>	<u>Z</u>
# 1	161.29 cm 5 ft 3.5 in	182.88 cm 6 ft	137.16 cm 4 ft 6.0 in

Shields			
Shield Name	Dimension	Material	Density
Source	9.56e+05 in ³	Iron	3.93
Air Gap		Air	0.00122

Source Input				
Grouping Method : Actual Photon Energies				
Nuclide	curies	becquerels	$\mu\text{Ci}/\text{cm}^3$	Bq/cm^3
Ba-137m	7.1189e-001	2.6340e+010	4.5421e-002	1.6806e+003
Cs-137	7.5253e-001	2.7844e+010	4.8013e-002	1.7765e+003

Buildup
The material reference is : Source

Integration Parameters	
X Direction	10
Y Direction	20
Z Direction	20

Results					
Energy MeV	Activity photons/sec	Fluence Rate MeV/cm ² /sec	Fluence Rate MeV/cm ² /sec	Exposure Rate mR/hr	Exposure Rate mR/hr
		No Buildup	With Buildup	No Buildup	With Buildup
0.0318	5.453e+08	4.686e-26	9.541e-25	3.904e-28	7.947e-27
0.0322	1.006e+09	6.051e-25	2.363e-24	4.870e-27	1.902e-26
0.0364	3.661e+08	4.404e-18	5.105e-18	2.502e-20	2.900e-20
0.6616	2.370e+10	1.301e+03	3.095e+03	2.523e+00	6.000e+00
TOTALS:	2.562e+10	1.301e+03	3.095e+03	2.523e+00	6.000e+00

Appendix E

MicroShield™ Modeling Results for STS Pipeway/Shield Structure Piping and M-8 Riser to STS Piping

Component or area: STS Valve Aisle Jumper J20FV-301

Model geometry used: Cylinder surface - external dose point

Given/Facts:

1. An unshielded probe reading was taken of the jumper within the STS Valve Aisle. The reading that was measured on Jumper J20FV-301 was 1700 mR/hr.

Assumptions:

1. For calculating the curie content of the piping in the STS Pipeway the $\mu\text{Ci}/\text{cm}^2$ value of the jumper J20 FV-301 is assumed to be representative of the remaining inaccessible piping.
2. The wall thickness of the jumper was 0.145 inches of stainless steel.
3. The contamination was assumed to be uniformly distributed on the internal surfaces of the jumper and entirely of Cs-137.

Calculation:

Input into the model

Detector position: 2" from the external surface of the jumper.

Source dimensions: cylindrical source with an 18" height and a .805" radius.

Reading modeled: 1700 mR/hr

Source material: N/A

Drawings: 900D-1079 Sht.1, Rev.5

Work Documents/Surveys: Radiation Protection Survey #060042

Model prepared by: E.Y. Lauber E.Y. Lauber 6 June 04
Signature/Print name/Date

Model peer reviewed by: E.B. Lachapelle E.B. Lachapelle 1/6/04
Signature/Print name/Date

MicroShield v6.02 (6.02-0000)
Grove Engineering

Page : 1
DOS File : JumperJ20-FV301Characterization_03Dec17EYL.ms6
Run Date: January 6, 2004
Run Time: 10:39:02 AM
Duration : 00:00:00

File Ref:
Date: 1/6/04
By: W. J. Rauter
Checked: W. J. Rauter

Case Title: Jumper J20 FV-301
Description: STS Valve Aisle Jumper 1700 mR @ contact
Geometry: 10 - Cylinder Surface - External Dose Point



Source Dimensions

Height	45.72 cm	1 ft 6.0 in
Radius	2.045 cm	0.8 in

Dose Points

	<u>X</u>	<u>Y</u>	<u>Z</u>
# 1	7.493 cm 3.0 in	22.86 cm 9.0 in	0 cm 0.0 in

Shields

<u>Shield Name</u>	<u>Dimension</u>	<u>Material</u>	<u>Density</u>
Cyl. Radius	2.045 in	Air	0.00122
Transition		Air	0.00122
Air Gap		Air	0.00122
Wall Clad	.145 in	Iron	7.86

Source Input

Grouping Method : Actual Photon Energies

<u>Nuclide</u>	<u>curies</u>	<u>becquerels</u>	<u>μCi/cm²</u>	<u>Bq/cm²</u>
Ba-137m	7.6670e-002	2.8368e+009	1.3053e+002	4.8296e+006
Cs-137	8.1046e-002	2.9987e+009	1.3798e+002	5.1053e+006

Buildup

The material reference is : Wall Clad

Integration Parameters

Y Direction (axial)	20
Circumferential	20

Results

<u>Energy</u> <u>MeV</u>	<u>Activity</u> <u>photons/sec</u>	<u>Fluence Rate</u> <u>MeV/cm²/sec</u> <u>No Buildup</u>	<u>Fluence Rate</u> <u>MeV/cm²/sec</u> <u>With Buildup</u>	<u>Exposure Rate</u> <u>mR/hr</u> <u>No Buildup</u>	<u>Exposure Rate</u> <u>mR/hr</u> <u>With Buildup</u>
0.0318	5.873e+07	1.725e-07	1.884e-07	1.437e-09	1.569e-09
0.0322	1.084e+08	6.334e-07	6.928e-07	5.098e-09	5.576e-09
0.0364	3.943e+07	9.406e-05	1.054e-04	5.344e-07	5.989e-07
0.6616	2.553e+09	6.347e+05	8.767e+05	1.230e+03	1.700e+03
TOTALS:	2.759e+09	6.347e+05	8.767e+05	1.230e+03	1.700e+03

Appendix F


STS Pipeway/Shield Structure Piping Surface Area and Cs-137 Curie Inventory Calculation

**STS Pipeway/Shield Structure Cs-137 Inventory Calculation
as of Survey Date (May 1998)**

							Totals
Estimated Linear Feet of Piping ⁽¹⁾	800	330	2,390	2,040	560	330	
Schedule 40 Pipe Inches	3	2 ½	2	1 ½	1	¾	
Pipe Inside Diameter Inches	3.068	2.469	2.067	1.61	1.049	0.824	
inches ²	92,482	30,701	186,144	123,756	22,135	10,246	465,463
cm ²	596,656	198,068	1,200,927	798,425	142,804	66,103	3,002,983
Cs-137 Areal Concentration $\mu\text{Ci}/\text{cm}^{2(2)}$	138	138	138	138	138	138	
Cs-137 μCi	8.23e+07	2.73e+07	1.66e+08	1.10e+08	1.97e+07	9.12e+06	4.14e+08
Cs-137 Curies	8.23e+01	2.73e+01	1.66e+02	1.10e+02	1.97e+01	9.12e+00	4.14e+02

- (1) Estimated linear feet of STS Pipeway/Shield Structure piping provided in E-mail, Dan Meess to John Fazio, "Estimated STS HLW Piping," dated December 16, 2003.
- (2) From Appendix F MicroShield™ modeling results.

Prepared By:

 2/13/04
J. M. Fazio

Peer Reviewed By:

 2/13/04
L. M. Michalczak

Appendix G

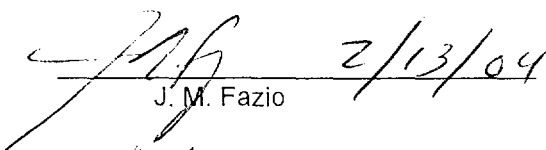
Peer Reviewed Scaling Factor Calculation for STS Valve Aisle Scaling Factor Data

Scaling Factor Calculation for
STS Valve Aisle Scaling Factor Data

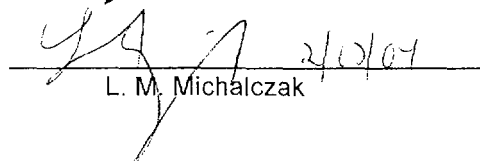
Project Isotope	STS Valve Aisle Scaling Factors May 2, 2002*	STS Valve Aisle Scaling Factors September 30, 2004
C-14	1.24e-06	1.31e-06
Tc-99	2.13e-04	2.25e-04
I-129	9.86e-10	1.04e-09
U-232	8.83e-06	9.12e-06
U-233	3.39e-06	3.58e-06
U-234	1.62e-06	1.82e-07
U-235	7.19e-07	7.60e-07
Np-237	7.87e-06	8.32e-06
U-238	5.57e-07	5.89e-07
Pu-238	1.50e-03	1.56e-03
Pu-239	4.60e-04	4.86e-04
Pu-240	8.18e-04	8.65e-04
Pu-241	1.06e-02	9.97e-03
Am-241	1.27e-02	1.34e-02
Cm-243	8.99e-05	8.96e-05
Cm-244	2.19e-03	2.11e-03
Cs-137	1.00e+00	1.00e+00
Sr-90	9.61e-01	9.58e-01

* From RIR-403-007

Prepared By:

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Peer Reviewed By:

 2/10/04
L. M. Michalczak

Appendix H

Waste Tank Farm HLW Legacy Piping Calculations (THOREX Waste Line 7P120)

Waste Tank Farm HLW Legacy Piping Calculations
THOREX Waste Line 7P120

Project Isotope	THOREX Radionuclide Distribution		
	1/01/1987		9/30/2004
	Curies*	Curies/Gallon**	
C-14	1.30e-01	1.09e-05	1.09e-05
Tc-99	1.04e+02	8.75e-03	8.75e-03
I-129	<1.80e-01	1.51e-05	1.51e-05
U-232	2.74e+00	2.30e-04	1.94e-04
U-233	2.09e+00	1.76e-04	1.76e-04
U-234	2.17e+00	1.83e-04	1.85e-04
U-235	5.17e-03	4.35e-07	4.35e-07
Np-237	3.02e-01	2.54e-05	2.54e-05
U-238	7.11e-05	5.98e-09	5.98e-09
Pu-238	4.80e+02	4.04e-02	3.51e-02
Pu-239	1.54e+01	1.30e-03	1.30e-03
Pu-240	8.09e+00	6.80e-04	6.80e-04
Pu-241	8.50e+02	7.15e-02	3.04e-02
Am-241	2.41e+02	2.03e-02	2.11e-02
Cm-243	2.34e-01	1.97e-05	1.28e-05
Cm-244	1.37e+01	1.15e-03	5.83e-04
Cs-137	4.57e+05	3.84e+01	2.56e+01
Sr-90	4.54e+05	3.82e+01	2.48e+01

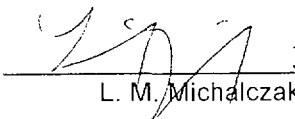
* From Table 12 of Topical Report DOE/NE/44139-14 "High-Level Waste Characterization at West Valley, " June 2, 1986⁽¹⁶⁾.

** For 11,889 gallons of THOREX waste as reported in Reference 16.

Prepared By:

 2/13/04
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Peer Reviewed By:

 2/13/04
L. M. Michalczak

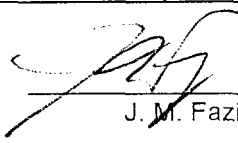
For the THOREX Waste Pipeline 7P120, a residual volume is conservatively estimated to be 7 gallons as shown below:

Reference Drawings: 8A-L-1, 8A-L-2, 8A-L-9, 8A-L-12, 15R-L-81		
	Length (Feet)	700
	Diameter (Inches)	3
	Schedule	40
Calculate	Line Volume (Gallons)	300
	Assume 2% Residual Waste Volume (Gallons) (6 gallons plus 1 gallon in dead leg)	7

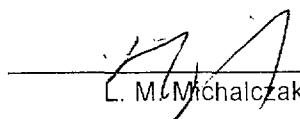
For a 7-gallon residual THOREX waste volume and using the decay corrected THOREX waste radionuclide distribution concentrations, the radionuclide inventory for Line 7P-120 is shown below:

Line 7P120 Inventory		
Radionuclide	THOREX Radionuclide Distribution Decayed to 9/30/2004 (Ci/gal)	Inventory as of September 30, 2004 2% (7 Gallons) Residual (Curies)
C-14	1.09e-05	7.63e-05
Tc-99	8.75e-03	6.13e-02
I-129	1.51e-05	1.06e-04
U-232	1.94e-04	1.36e-03
U233/234		
U-233	1.76e-04	1.23e-03
U-234	1.85e-04	1.30e-03
U-235/236		
U-235	4.35e-07	3.05e-06
Np-237	2.54e-05	1.78e-04
U-238	5.98e-09	4.19e-08
Pu-238	3.51e-02	2.46e-01
Pu-239	1.30e-03	9.10e-03
Pu-240	6.80e-04	4.76e-03
Pu-241	3.04e-02	2.13e-01
Am-241	2.11e-02	1.48e-01
Cm-243	1.28e-05	8.96e-05
Cm-244	5.83e-04	4.08e-03
Cs-137	2.56e+01	1.79e+02
Sr-90	2.48e+01	1.74e+02

Prepared By:

 2/13/04 2/13/04
J. M. Fazio

Peer Reviewed By:

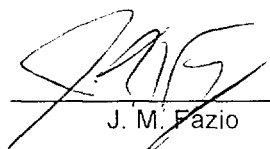
 2/13/04
L. M. Michalczak

Appendix I

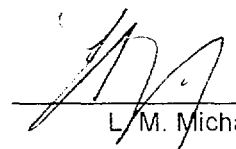
Waste Tank Farm HLW Legacy Piping Calculations
(8D-2 WasteTransfer Line 7P113)

Tank 3D-2		
Radionuclide	Sample 02-1765 December 19, 2002 ($\mu\text{Ci/ml}$)	Decay Corrected to September 30, 2004 ($\mu\text{Ci/ml}$)
C-14	9.79e-05	9.79e-05
Tc-99	1.16e-04	1.16e-04
I-129	<8.21e-05	8.21e-05
U-232	2.06e-05	2.02e-05
U-233	8.60e-06	8.60e-06
U-234	4.10e-06	4.11e-06
U-235	3.30e-08	3.30e-08
Np-237	5.17e-06	5.17e-06
U-238	4.21e-07	4.21e-07
Pu-238	1.37e-03	1.35e-03
Pu-239	9.07e-04	9.07e-04
Pu-240	6.93e-04	6.93e-04
Pu-241	1.34e-02	1.23e-02
Am-241	5.77e-03	5.79e-03
Cm-243	2.49e-05	2.38e-05
Cm-244	6.51e-04	6.08e-04
Cs-137	2.32e+00	2.23e+00
Sr-90	1.88e-01	1.80e-01

Prepared By:

 2/13/04
J. M. Fazio

Peer Reviewed By:

 2/17/04
L. M. Michalczak

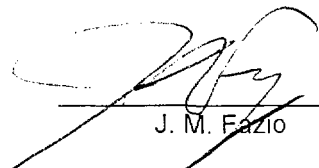
For the Tank 8D-2 Pipeline 7P113, a residual volume is conservatively estimated to be 15 gallons as shown below:

Reference Drawings: 8A-L-1, 8A-L-2, 8A-L-9, 8A-L-12, 15R-L-81		
	Length (Feet)	50
	Diameter (Inches)	3
	Schedule	40
Calculate	Line Volume (Gallons)	20
	Assume 2% Residual Waste Volume (Gallons)	4

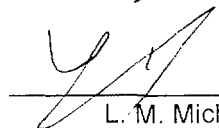
For a 15 gallon residual waste volume and using the decay corrected Tank 3D-2 waste radionuclide distribution concentrations, the radionuclide inventory for Line 7P-113 is shown below:

Radionuclide	Tank 3D-2 Sample 02-1765 Decay Corrected to September 30, 2004 ($\mu\text{Ci/ml}$)	7P113 Inventory as of September 30, 2004 2% (4 Gallons) Residual (Curies)
C-14	9.97e-05	1.48e-06
Tc-99	1.16e-04	1.76e-06
I-129	8.21e-04	1.24e-06
U-232	2.02e-05	3.06e-07
U-233	8.60e-06	1.30e-07
U-234	4.11e-06	6.22e-08
U-235	3.30e-08	5.00e-10
Np-237	5.17e-06	7.83e-08
U-238	4.21e-07	6.37e-09
Pu-238	1.35e-03	2.04e-05
Pu-239	9.07e-04	1.37e-05
Pu-240	6.93e-04	1.05e-05
Pu-241	1.23e-02	1.86e-04
Am-241	5.79e-03	8.77e-05
Cm-243	2.38e-05	3.60e-07
Cm-244	6.08e-04	9.21e-06
Cs-137	2.23e+00	3.38e-02
Sr-90	1.80e-01	2.73e-03

Prepared By:

 2/13/04
J. M. Fazio

Peer Reviewed By:

 2/12/04
L. M. Michalczak

Appendix J

MicroShield™ Modeling Results for M-8 Riser Pump Pit

Component or area: M-8 Pit

Model geometry used: Rectangular Volume

Given/Facts:

1. Unshielded probe readings were taken inside the M-8 pit. The highest reading measured was 860 mR/hr.

Assumptions:

1. The pit was modeled using a conservative approach by obtaining the highest dose reading measured in the pit and moving the dose point to the outside of the volume. The density of the source was determined by using the weight of the equipment inside the pit.
2. The amount and weight of the equipment was estimated from drawings. Each piece of equipment was identified, put into a file with its dimensions and constituents and a volume estimated. The total volume was calculated with an additional 50% of the total added as a conservative measure (see attached peer reviewed calculations)
3. All contamination was assumed to be exclusively Cs-137.
4. Material in the pit was assumed to be iron.
5. The pit is assumed to be a regular rectangular shape.

Calculation:

Input into the model

Detector position: Flush with top of pit area; centered geometrically over the pit at a distance of 2" from the surface of the volume.

Source dimensions: 6' 3" by 5' by 7' 5 1/2"

Reading modeled: 860 mR/hr

Source material: Combination of air, piping and components (3005 lbs. see attached peer reviewed calculations)

Drawings: 900D-1305 sht. 1, sht. 2 and sht. 10; 900D-1170

Work Documents/Surveys: WO 0002260

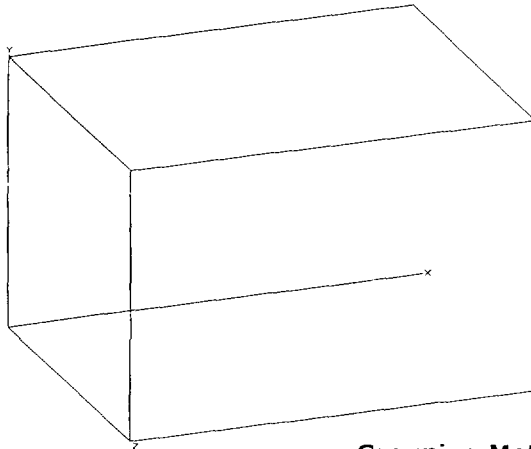
Model prepared by: Eric Y. Lauber E.Y. Lauber 27 Jan 04
Signature/Print name/Date

Model peer reviewed by: E.B. Lachapelle E.B. Lachapelle 1/27/04
Signature/Print name/Date

Page : 1
DOS File : M8PitCharacterization_04Jan12EYL.ms6
Run Date: January 27, 2004
Run Time: 11:12:56 AM
Duration : 00:00:01

File Ref: _____
Date: 27 Jan 04
By: E. J. Lander
Checked: EL

Case Title: M-8 Pit
Description: WTF Characterization of M-8 Pit based on 860 mR/hr.
Geometry: 13 - Rectangular Volume



Source Dimensions

Length	227.33 cm	7 ft 5.5 in
Width	190.5 cm	6 ft 3.0 in
Height	152.4 cm	5 ft 0.0 in

Dose Points

	<u>X</u>	<u>Y</u>	<u>Z</u>
# 1	232.41 cm 7 ft 7.5 in	76.2 cm 2 ft 6.0 in	95.25 cm 3 ft 1.5 in

Shields

<u>Shield Name</u>	<u>Dimension</u>	<u>Material</u>	<u>Density</u>
Source	6.60e+06 cm ³	Iron	0.2067
Air Gap		Air	0.00122

Source Input

Grouping Method : Actual Photon Energies

<u>Nuclide</u>	<u>curies</u>	<u>becquerels</u>	<u>μCi/cm³</u>	<u>Bq/cm³</u>
Ba-137m	3.4567e+000	1.2790e+011	5.2375e-001	1.9379e+004
Cs-137	3.6540e+000	1.3520e+011	5.5364e-001	2.0485e+004

Buildup

The material reference is : Source

Integration Parameters

X Direction	10
Y Direction	20
Z Direction	20

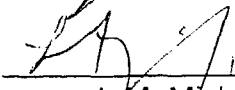
Results

<u>Energy</u> <u>MeV</u>	<u>Activity</u> <u>photons/sec</u>	<u>Fluence Rate</u> <u>MeV/cm²/sec</u> <u>No Buildup</u>	<u>Fluence Rate</u> <u>MeV/cm²/sec</u> <u>With Buildup</u>	<u>Exposure Rate</u> <u>mR/hr</u> <u>No Buildup</u>	<u>Exposure Rate</u> <u>mR/hr</u> <u>With Buildup</u>
0.0318	2.648e+09	1.582e-01	1.677e-01	1.318e-03	1.397e-03
0.0322	4.885e+09	3.487e-01	3.701e-01	2.806e-03	2.979e-03
0.0364	1.778e+09	6.282e-01	6.751e-01	3.569e-03	3.836e-03
0.6616	1.151e+11	2.782e+05	4.436e+05	5.393e+02	8.600e+02
TOTALS:	1.244e+11	2.782e+05	4.436e+05	5.393e+02	8.600e+02

Estimate of Mass of Components in the 8D-2 M-8 Pump Pit

Description	Dimensions						Ref Dwg	Volume in ³	Mass lbs
Seal Ring	46	in diameter	0.25	in thick			900D-1170	415	120
28"-150 lb weld neck flange							900D-1170	1207	350
28" riser	28	in diameter	0.75	in thick	31.2	in long	900D-1305 sh 1	2057	597
Water Spray Upper	3/4	in diameter	Schedule 40		225	in long	900D-1305 sh 1	60	17
Water Spray Lower	3/4	in diameter	Schedule 40		225	in long	900D-1305 sh 1	60	17
Culvert	18	in diameter	Schedule 40		6.5	in long	900D-1305 sh 1	206	60
Culvert Seal	19 1/8	in diameter	3/8	in thick			900D-1305 sh 2	108	31
Culvert Drain Trough top & bottom	6	in wide	62.8	in Long	1/4	in thick	900D-1305 sh 2	188	55
Culvert Drain Trough side	22	in high	31.4	in Long	1/4	in thick	900D-1305 sh 2	173	50
Gussets	27	in high	15	in Long	1/2	in thick	900D-1305 sh 2	608	176
Motor Extension	10	in diameter	Schedule 40		90	in high	900D-1305 sh10	1031	299
Pump Discharge Piping	2 1/2	in diameter	Schedule 40		15	ft long	900D-1305	287	83
Pump Discharge Piping Spare	2 1/2	in diameter	Schedule 40		5	ft long	900D-1305	96	28
Culvert Drain Piping	2	in diameter	Schedule 40		5	ft long	900D-1305	58	17
Valve Aisle Sump Drain	2 1/2	in diameter	Schedule 40		5	ft long	900D-1305	96	28
STS Return Piping	2 1/2	in diameter	Schedule 40		5	ft long	900D-1305	96	28
Casing Drain Piping	1 1/2	in diameter	Schedule 40		20	ft long	900D-1305	164	48
TOTAL								6909	2004
50% conservatism								10364	3005

Prepared By  1/22/07
J.M. Fazio

Peer Reviewed By  1/24/04
L.M. Michalczak

Appendix K

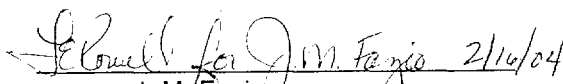
M-8 Pit to STS Piping Surface Area and Cs-137 Curie Inventory Calculation

**M-8 Pump Pit to STS Piping Cs-137 Inventory Calculation
 as of Survey Date May 1988**

Estimated Linear Feet of Piping ⁽¹⁾	900
Schedule 40 Pipe (Inches)	2 ½
Pipe Inside Diameter (Inches)	2.469
inches ²	83728.7
cm ²	540184.3
Cs-137 areal concentration μCi/cm ²⁽²⁾	138
Cs-137 μCi	74545428
Cs-137 Curies	74.5

- (1) Estimated linear feet of STS Pipeway/Shield Structure piping provided in e-mail from D. C. Meess to J. M. Fazio, "Estimated STS HLW Piping," December 16, 2003.
- (2) From Appendix E MicroShield™ Modeling results.

Prepared By:


 J. M. Fazio 2/16/04

Peer Reviewed By:


 L. M. Michalczak 2/16/04

Appendix L

Peer Reviewed Radionuclide Inventory for the Balance of the Waste Tank Farm

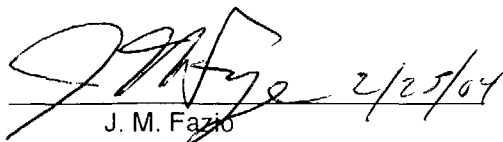
	Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5	HLW Transfer Trench Piping	HLW Legacy Piping Pipeline 7P113 to Tank 8D-2	HLW Legacy Piping Pipeline 7P120 to Tank 8D-4	STS Pipeway/ Shield Structure	M-8 Riser Pump Pit Piping	Associated Piping (M-8 Pump Pit to STS)
Cs-137 Curies from MicroShield™	2.22e+02 (See Note 1)	1.18e+02 (See Table 7)	N/A	N/A	414.1 (See Appendix F)	3.7	74.5 (See Appendix K)
Cs-137 Curies Aged to 9/30/04	(See Note 2)	(See Note 2)	N/A	N/A	392.1	3.35	64.3
Gallons of Liquid	N/A	N/A	4 (See Appendix I)	7 (See Appendix H)	N/A	N/A	N/A
Project Isotope	Aged Batch 10 Scaling Factors		Aged Tank 3D-2 Analytical Results (VAST 02-1767) (μCi/ml)	Aged THOREX Radionuclide Distribution	Aged STS Valve Aisle Scaling Factors		
C-14	2.03e-07	2.03e-07	9.79e-05	1.09e-05	1.31e-06	1.31e-06	1.31e-06
Tc-99	3.51e-05	3.51e-05	1.16e-04	8.75e-03	2.25e-04	2.25e-04	2.25e-04
I-129	1.62e-10	1.62e-10	8.21e-05	1.51e-05	1.04e-09	1.04e-09	1.04e-09
U-232	3.85e-06	3.85e-06	2.02e-05	1.94e-04	9.12e-06	9.12e-06	9.12e-06
U-233	1.49e-06	1.49e-06	8.60e-06	1.76e-04	3.58e-06	3.58e-06	3.58e-06
U-234	5.73e-07	5.73e-07	4.11e-06	1.85e-04	1.72e-06	1.72e-06	1.72e-06
U-235	1.58e-08	1.58e-08	3.30e-08	4.35e-07	7.60e-07	7.60e-07	7.60e-07
Np-237	8.30e-06	8.30e-06	5.17e-06	2.54e-05	8.32e-06	8.32e-06	8.32e-06
U-238	1.41e-07	1.41e-07	4.21e-07	5.98e-09	5.89e-07	5.89e-07	5.89e-07
Pu-238	1.55e-03	1.55e-03	1.35e-03	3.51e-02	1.56e-03	1.56e-03	1.56e-03
Pu-239	4.52e-04	4.52e-04	9.07e-04	1.30e-03	4.86e-04	4.86e-04	4.86e-04
Pu-240	3.21e-04	3.21e-04	6.93e-04	6.80e-04	8.65e-04	8.65e-04	8.65e-04
Pu-241	9.96e-03	9.96e-03	1.23e-02	3.04e-02	9.97e-03	9.97e-03	9.97e-03
Am-241	1.33e-02	1.33e-02	5.79e-03	2.11e-02	1.34e-02	1.34e-02	1.34e-02
Cm-243	8.96e-05	8.96e-05	2.38e-05	1.28e-05	8.96e-05	8.96e-05	8.96e-05
Cm-244	2.10e-03	2.10e-03	6.08e-04	5.83e-04	2.11e-03	2.11e-03	2.11e-03
Cs-137	1.00e+00	1.00e+00	2.23e+00	2.56e+01	1.00e+00	1.00e+00	1.00e+00
Sr-90	9.54e-01	9.54e-01	1.88e-01	1.80e-01	9.58e-01	9.58e-01	9.58e-01

Project Isotope	Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5	HLW Transfer Trench Piping	HLW Legacy Piping Pipeline 7P113 to Tank 8D-2	HLW Legacy Piping Pipeline 7P120 to Tank 8D-4	STS Pipeway/ Shield Structure Piping	M-8 Riser Pump Pit	Associated Piping (M-8 Pump Pit to STS)	Totals
Balance of Tank Farm Inventory Decayed/Ingrown to September 30, 2004								
C-14	4.52e-05	2.40e-05	1.48e-06	7.63e-05	5.14e-04	4.39e-06	8.42e-05	7.49e-04
Tc-99	7.79e-03	4.14e-03	1.76e-06	6.13e-02	8.82e-02	7.54e-04	1.45e-02	1.77e-01
I-129	3.59e-08	1.91e-08	1.24e-06	1.06e-04	4.08e-07	3.48e-09	6.69e-08	1.19e-04
U-232	8.56e-04	4.55e-04	3.06e-07	1.36e-03	3.58e-03	3.06e-05	5.86e-04	6.86e-03
U-233	3.32e-04	1.76e-04	1.30e-07	1.23e-03	1.40e-03	1.20e-05	2.30e-04	3.39e-03
U-234	1.27e-04	6.76e-05	6.22e-08	1.30e-03	6.74e-04	5.76e-06	1.11e-04	2.28e-03
U-235	3.50e-06	1.86e-06	5.00e-10	3.05e-06	2.98e-04	2.55e-06	4.89e-05	3.58e-03
Np-237	1.84e-03	9.79e-04	7.83e-08	1.78e-04	3.26e-03	2.79e-05	5.35e-04	6.82e-03
U-238	3.13e-05	1.66e-05	6.37e-09	4.19e-08	2.31e-04	1.97e-06	3.79e-05	3.19e-04
Pu-238	3.45e-01	1.83e-01	2.04e-05	2.46e-01	6.12e-01	5.23e-03	1.00e-01	1.49e+00
Pu-239	1.00e-01	5.34e-02	1.37e-05	9.10e-03	1.91e-01	1.63e-03	3.12e-02	3.86e-01
Pu-240	7.13e-02	3.79e-02	1.05e-05	4.76e-03	3.39e-01	2.90e-03	5.56e-02	5.12e-01
Pu-241	2.21e+00	1.18e+00	1.86e-04	2.13e-01	3.91e+00	3.34e-02	6.41e-01	8.18e+00
Am-241	2.96e+00	1.57e+00	8.77e-05	1.48e-01	5.25e+00	4.49e-02	8.62e-01	1.08e+01
Cm-243	1.99e-02	1.06e-02	3.60e-07	8.96e-05	3.51e-02	3.00e-04	5.76e-03	7.18e-02
Cm-244	4.67e-01	2.48e-01	9.21e-06	4.08e-03	8.27e-01	7.07e-03	1.36e-01	1.69e+00
Cs-137	2.22e+02	1.18e+02	3.38e-02	1.79e+02	3.92e+02	3.35e+00	6.43e+01	9.79e+02
Sr-90	2.12e+02	1.13e+02	2.73e-03	1.74e+02	3.76e+02	3.21e+00	6.16e+01	9.39e+02

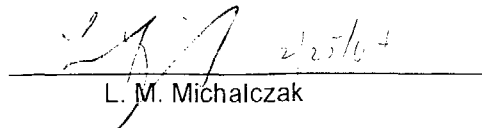
Notes:

- 1 Sum of MicroShield™ modeling results: 8Q-1 (0.31 Ci); 8Q-2 (221 Ci); 8Q-4 (0.051 Ci); 8Q-5 (0.75 Ci).
- 2 The aging of MicroShield™ results was not required since, per the CMP, the surveys were taken within one year of September 30, 2004.

Prepared By:


 J. M. Fazio

Peer Reviewed By:


 L. M. Michalczak

Appendix M

Technical Review and Approval Panel Consensus Statement

FACILITY CHARACTERIZATION PROJECT

Technical Review and Approval Panel Consensus Statement

Unit Name (s): Balance of the Waste Tank Farm

Summary of Technical Approach That Was Utilized:

From the review of the operational processes conducted in the Waste Tank Farm, the available historic information, and previously generated data, the following areas were identified as potential key curie contributors:

- HLW Transfer Trench Piping
- Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5
- STS Pipeway/Shield Structure Piping
- Waste Tank Farm HLW Legacy Piping
- M-8 Riser Pump Pit and associated piping

HLW Transfer Trench Piping

The HLW Transfer Trench piping is contained within the 500 foot long concrete waste transfer trench. The approximately 3,000 feet of two- and three-inch Schedule 40 stainless steel piping was used to convey wastes between tanks within the Waste Tank Farm and to the Vitrification Facility for solidification. The interior of the HLW Transfer Trench was last surveyed in January 2002. However, this data could not be validated due to a discrepancy in the probe and rate meter. Therefore, new dose rate measurements were needed for the Transfer Trench. Using the new dose rates and the Batch 10 vitrification run isotopic data, the Trench Transfer piping was then modeled, scaling factors developed, and a curie estimate was calculated for the residual activity in the transfer piping.

Pits 8Q-1, 8Q-2, 8Q-4, and 8Q-5

The 8Q-1, 8Q-2, 8Q-4, and 8Q-5 Pits are approximately 6 feet deep and vary in size from 6 feet by 7 feet to 13.5 feet by 12 feet. Each pit accommodates the removal pump, jumpers, and flow monitoring equipment required to process the waste out of the respective waste tank. The interior of the 8Q-1, 8Q-2, 8Q-4, and 8Q-5 Pits were last surveyed in January 2002. However, this data could not be validated due to a discrepancy in the probe and rate meter. Therefore, new dose rate measurements were needed for these pits. Using the new dose rates and the Batch 10 vitrification run isotopic data, the pits were then modeled, scaling factors developed, and a curie estimate was calculated.

STS Pipeway/Shield Structure Piping

The STS Pipeway/Shield Structure is located on top of the Tank 8D-1 vault adjacent to the first floor of the support building. This concrete and steel structure contains numerous piping runs and structural members that support the STS equipment in Tank 8D-1. These facilities were designed for the pretreatment of the HLW PUREX supernatant and sludge wash solutions. There was no historical radiological survey data located for the STS Pipeway/Shield Structure. However, jumpers in the valve aisle have been surveyed which would be radiologically similar to the pipeway/shield structure piping. Dose rate measurements of a valve aisle jumper taken in May 1998 were 1,700 mR/hr. Using the 1998 dose rate measurement and the existing STS Valve Aisle scaling factors, the pipeway/shield structure piping was then modeled and a curie estimate was calculated.

Waste Tank Farm HLW Legacy Piping

The HLW Legacy Piping originate at floor nozzles in the CPC. Each line is approximately 500 and 700 feet long and constructed of 3-inch Schedule 40 stainless steel pipe and gravity drain to HLW waste storage tanks in the Waste Tank Farm. These lines were used for the transfer of all reprocessing wastes to the Waste Tank Farm. PUREX HLW was transferred to Tank 8D-2 via Line 7P-113 and for the transfer of THOREX waste to Tank 8D-4, Line 7P-120 was used. Subsequent to reprocessing, Line 7P-113 has been flushed by the process plant decontamination solutions and other miscellaneous wastes, such as cell sumps and laboratory wastes, that were routinely collected in Tank 7D-2 and sampled in Tank 3D-2 before being transferred to Tank 8D-2. The other HLW Pipeline 7P-112, which serviced Tank 8D-1, was never used as Tank 8D-1 was the spare HLW receiver tank. Using existing data to compute the radioisotopic concentrations of the Tank 7D-2 waste stream and the THOREX waste stream, a curie estimate was calculated volumetrically for residual wastes remaining in the piping.

M-8 Riser Pump Pit and Associated Piping

The M-8 Pump Pit is 75 inches wide by 60 inches long by 90 inches deep and fabricated from 1/4-inch stainless steel. The associated supply and return transfer piping plus two spare lines are 2 1/2-inch diameter Schedule 40 304L stainless steel doubly contained in a 200 foot long 20 inch diameter culvert pipe. This system was used to transport the PUREX supernatant, sludge wash, and sodium bearing waste water to the STS for treatment.

The interior of the M-8 Riser Pump Pit was last surveyed in November and December 2000 during STS flushing operations. Surveys were taken through existing valve access ports in the pit cover located 65 inches from the top of the pit covers into the pit. Dose rates ranged from 722 mR/hr to 1,244 mR/hr. Using the 2000 dose rate measurement and the existing STS Valve Aisle scaling factors, the pipeway/shield structure piping was then modeled and a curie estimate was calculated (see Section 7.5.1).

There was no historical radiological survey data located for the associated piping of the M-8 Riser. However, jumpers in the valve aisle have been surveyed which would be radiologically similar to this piping. Dose rate measurements of a valve aisle jumper taken in May 1998 were 1,700 mR/hr. Using the 1998 dose rate measurement and the existing STS Valve Aisle scaling factors, the associated piping of the M-8 Riser was then modeled and a curie estimate was calculated.

Curie Estimate

Conservative curie estimates for the balance of the Waste Tank Farm (aged to September 30, 2004) are as follows:

Total Performance Assessment Radionuclides for Balance of the Waste Tank Farm* (Decayed and Ingrown to September 30, 2004)

Project Isotopes	Curie Estimate for Balance of the Waste Tank Farm
C-14	7.49e-04
Tc-99	1.77e-01
I-129	1.19e-04
U-232	6.86e-03
U-233	3.39e-03
U-234	2.28e-03
U-235	3.58e-03
Np-237	6.82e-03
U-238	3.19e-04
Pu-238	1.49e+00
Pu-239	3.86e-01
Pu-240	5.12e-01
Pu-241	8.18e+00
Am-241	1.08e+01
Cm-243	7.18e-02
Cm-244	1.69e+00
Cs-137*	9.79e+02
Sr-90**	9.39e+02

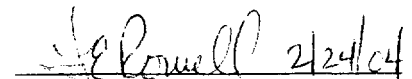
* The method for choosing the project isotopes is outlined in WVDP-403, "Characterization Management Plan for the Facility Characterization Project" (CMP).

** Cs-137 and Sr-90 are not critical radionuclides for the outcome of the performance assessment but are reported for completeness per WVDP-403.

Using best engineering judgement and available information, the following listed Technical Review and Approval Panel Members have reviewed the technical approach and resultant conservative curie estimate for the stated area/cell and have reached consensus that the approach and resultant estimate are technically sound for purposes of this project's scope as identified in the Characterization Management Plan for the Facility Characterization Project (WVDP-403).

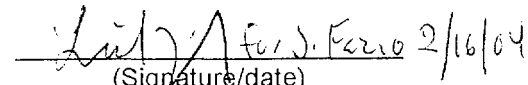
Project Manager:

L. E. Rowell


(Signature/date)

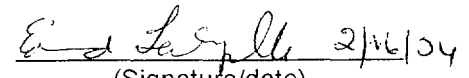
Project/Balance of Tank Farm Cell Lead:

J. M. Fazio


(Signature/date)


Project Cell Lead(s):

E. B. Lachapelle


(Signature/date)

Radiation Engineering and Dosimetry:

E. Y. Lauber


(Signature/date)

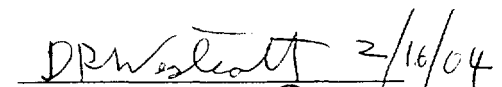
Radiation Protection:

R. L. Hazard


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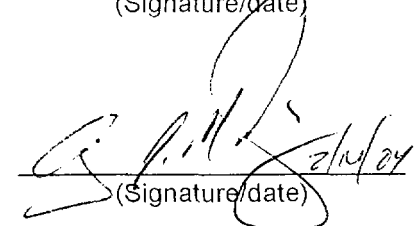
Decommissioning Planning:

D. R. Westcott


(Signature/date)

Analytical and Process Chemistry:

C. J. Maddigan


(Signature/date)

WVNSCO RECORD OF REVISION

Rev. No.	Description of Changes	Revision On Page(s)	Dated
0	Original Issue	All	02/25/04

Departments affected by this document are Facility
Characterization Project and Decommissioning Planning.